

Implementation Options for 150m 100GBASE-SR4 Links

Liang Qiu, Nexans

Paul Vanderlaan, Nexans

- 150m links:
 - ◆ Eases upgrade path from 40GBASE-SR4 to 100GBASE-SR4
 - Utilize existing infrastructure
 - ◆ Minimize datacenter physical layout redesign
 - Small percentage of population, yet
 - Big impact to physical layout in large data centers
 - ◆ Maintain end user confidence in MMF technology
 - ◆ Further data center and overall SMF/MMF Ethernet growth through effective technology implementation

- Demonstrate implementation options for 150m links on OM4 with FEC
 - ◆ Impact of:
 - Spectral width
 - Rise/fall time
 - Equalization
 - Fiber bandwidth
- The benefits 150m links offer seem achievable with small changes based on the June 2012 Fiber Channel spreadsheet.

References

- David Cunningham, *Thoughts on Initial Parameters for the 32GFC MMF Link Model*
<http://www.t11.org/ftp/t11/pub/fc/pi-6/12-211v0.pdf>
- David Cunningham, *Modifications To The Mode Partition Noise Penalty Calculation For Equalised 32GFC Links*
<http://www.t11.org/ftp/t11/pub/fc/pi-6/12-042v0.pdf>
- Jonathan King, *MMF links, EQ and FEC*
http://www.ieee802.org/3/100GNGOPTX/public/nov11/king_01_1111_NG100GOPTX.pdf
- Stephen Bates et al., *Backplane NRZ FEC Baseline Proposal*
http://www.ieee802.org/3/bj/public/mar12/gustlin_01_0312.pdf

Spreadsheet Model Parameters

- Based on Fiber Channel 12-211v0 with following exceptions in red.
- FEC: $Q=4.3$, targeting BER < E-12 after FEC.
- Data rate = **25781 MBd**, Power budget = 8.0 dB
- Transmitter
 - ◆ Center wavelength $U_c = 840\text{nm}$
 - ◆ RMS spectral width and rise/fall time: variables.
 - ◆ Power OMA = -2dBm
 - ◆ RIN (OMA) = -128dB/Hz
 - ◆ DJ = 8.56ps; DCD_DJ = 2.14ps.
 - ◆ MPN $k(\text{OMA}) = 0.3$; Modal Noise Penalty = 0.3dB

Spreadsheet Model Parameters

- OM4 MMF
 - ◆ BWm = 4500 MHz.km
 - ◆ Attn. = 3.5dB/km, connector loss = 1.5dB
 - ◆ Disp. min. Uo = 1316nm; Disp. So = 0.10275 ps/(nm².km)
- Receiver
 - ◆ Nominal Sensitivity OMA = **-11.00dBm**
 - ◆ Rec_BW = 19039MHz
 - ◆ RMS Baseline Wander SD = 0.013 fraction of 1/2 eye

Tx Characteristics (150m and FEC)

| | | | | | | | | | |
|-------------------------|------|------|------|------|------|------|------|------|------|
| RMS spectral width (nm) | 0.30 | 0.35 | 0.40 | 0.45 | 0.50 | 0.55 | 0.60 | 0.65 | 0.70 |
| Ts (20-80) (ps) | 22.7 | 22.2 | 21.5 | 20.8 | 19.9 | 18.9 | 17.7 | 16.3 | 14.6 |
| Pisi (dB) <3.6 | 3.59 | 3.60 | 3.59 | 3.60 | 3.60 | 3.60 | 3.60 | 3.60 | 3.59 |
| System margin (dB) >0 | 1.2 | 1.1 | 1.1 | 1.0 | 0.9 | 0.8 | 0.6 | 0.4 | 0.2 |
| V.E.C.P. (dBo) <4.0 | 3.76 | 3.77 | 3.76 | 3.77 | 3.77 | 3.78 | 3.77 | 3.77 | 3.76 |

- VCSELs with narrow spectral width or fast rise/fall time may not be effective to implement
- Pisi limited to 3.6 dB

Tx Characteristics (150m with FEC)

- What if allowing Pisi < 3.9dB, as in 12-211v0?

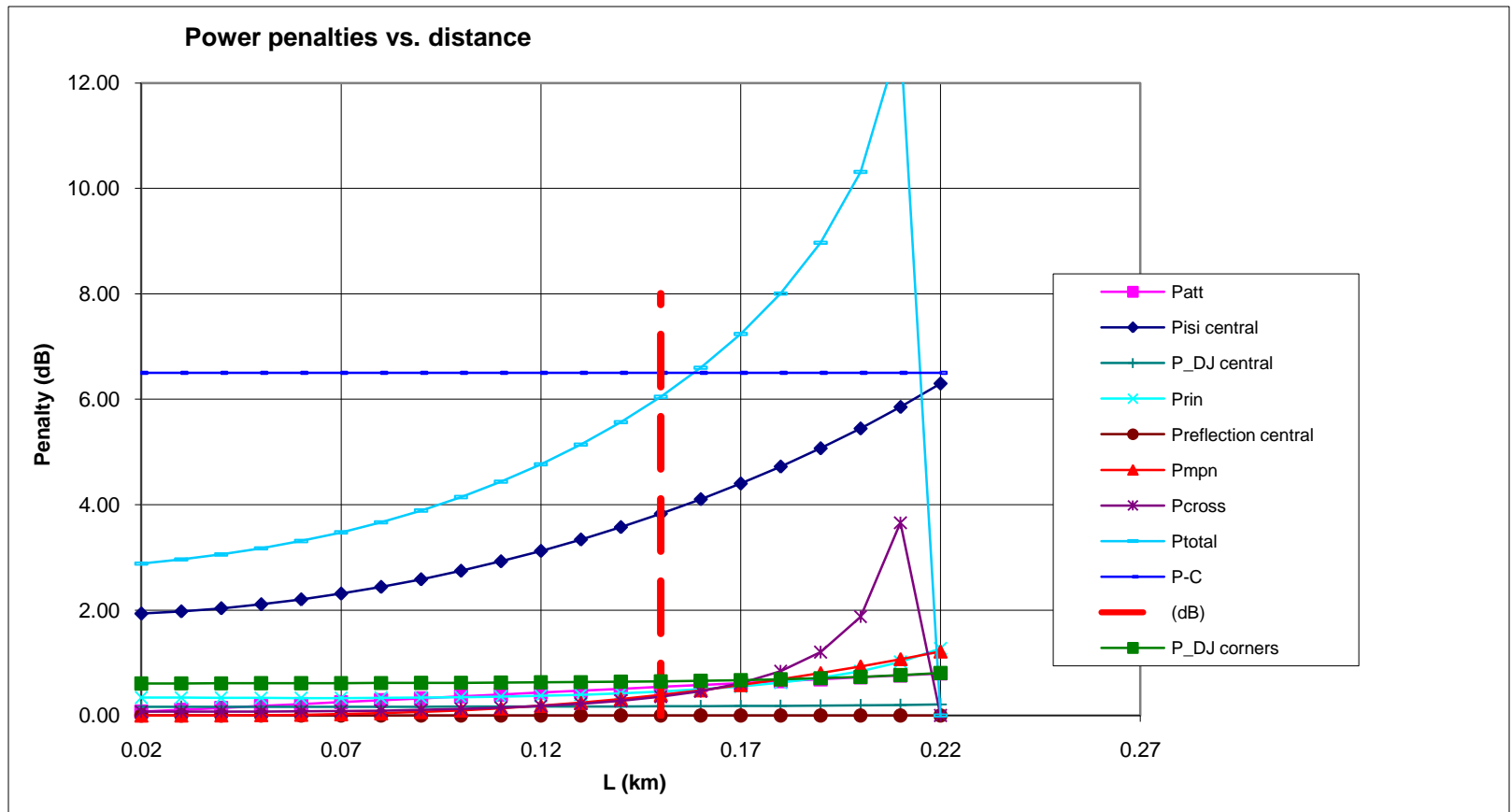
| | | | | | | | | | |
|-------------------------|------|------|------|------|------|------|------|------|------|
| RMS spectral width (nm) | 0.30 | 0.35 | 0.40 | 0.45 | 0.50 | 0.55 | 0.60 | 0.65 | 0.70 |
| Ts (20-80) (ps) | 23.6 | 23.0 | 22.4 | 21.7 | 20.8 | 19.9 | 18.7 | 17.4 | 15.3 |
| Pisi (dB) < 3.9 | 3.83 | 3.81 | 3.82 | 3.82 | 3.81 | 3.83 | 3.81 | 3.81 | 3.71 |
| System margin (dB) > 0 | 0.8 | 0.8 | 0.8 | 0.7 | 0.6 | 0.5 | 0.3 | 0.1 | 0.0 |
| V.E.C.P. (dBo) < 4.0 | 4.00 | 3.98 | 3.99 | 4.00 | 3.99 | 4.00 | 3.99 | 3.99 | 3.88 |

Power Penalties vs. Distance

150m on OM4 is Well Behaved at 180m



- RMS spectral width = 0.55nm and T_s (20-80) = 19.9ps.



Tx Characteristics (150m FEC + equalization)

| | | | | | | | | | |
|-------------------------|------|------|------|------|------|------|------|------|------|
| RMS spectral width (nm) | 0.30 | 0.35 | 0.40 | 0.45 | 0.50 | 0.55 | 0.60 | 0.65 | 0.70 |
| Ts (20-80) (ps) | 23.6 | 23.0 | 22.4 | 21.7 | 20.8 | 19.3 | 17.3 | 14.8 | 11.5 |
| System margin (dB) >0 | 0.6 | 0.5 | 0.4 | 0.2 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 |
| V.E.C.P. (dBo) <4.0 | 4.00 | 3.98 | 3.99 | 4.00 | 3.99 | 3.86 | 3.69 | 3.50 | 3.29 |

- 3-tap FFE equalization (T11/12-042V0), $\gamma = 1.0$, fixed EQ tap value = 0.14.

| | | | | | | | | | |
|-------------------------|------|------|------|------|------|------|------|------|------|
| RMS spectral width (nm) | 0.30 | 0.35 | 0.40 | 0.45 | 0.50 | 0.55 | 0.60 | 0.65 | 0.70 |
| Ts (20-80) (ps) | 23.6 | 23.0 | 22.4 | 21.7 | 20.8 | 19.9 | 18.7 | 17.4 | 15.3 |

- Equalization provides no improvement compared to FEC only (Pisi < 3.9).

Increasing Fiber Bandwidth (150m with FEC)

| Fiber Bwm (MHz.km) | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 7500 | 8000 | 8500 | 9000 |
|-------------------------|------|------|------|------|------|------|------|------|------|------|
| RMS spectral width (nm) | 0.54 | 0.57 | 0.59 | 0.60 | 0.61 | 0.62 | 0.62 | 0.63 | 0.63 | 0.64 |
| Pisi (dB) <3.9 | 3.80 | 3.83 | 3.84 | 3.82 | 3.82 | 3.83 | 3.80 | 3.83 | 3.80 | 3.84 |
| System margin (dB) >0 | 0.5 | 0.4 | 0.3 | 0.2 | 0.2 | 0.1 | 0.2 | 0.1 | 0.1 | 0.0 |
| V.E.C.P. (dBo) <4.0 | 3.98 | 4.00 | 4.01 | 4.00 | 4.00 | 4.01 | 3.97 | 4.00 | 3.98 | 4.01 |

- Model parameters from slides 5-6 (except fiber BWm)
- $T_s(20-80) = 20ps$
- Increased Fiber BWm to maximize RMS spectral width
- For this scenario, increasing Fiber BW yields limited gains

Summary

- Retaining 150m reach will:
 - ◆ best service existing infrastructure
 - ◆ maintain positive technology perception
 - ◆ increase industry adoption
- 150m drops may be a smaller percentage of deployment, but tend to have a bigger impact upon overall layout
- 150m appears reasonable from most recent FC spreadsheet
 - ◆ Increasing Pisi to 3.9dB relaxes rise/fall time (as in FC 12-211v0)
 - ◆ Equalization does not appear to be required

Suggest further group investigation of the effects of spectral width, rise/fall time, Pisi, and equalization to enable 150m reach

Backup, Snapshot of 25.8Gb/s, FEC



| Spreadsheet by David Cunningham, Avago Technologies | | | | | | | | | | Rev. | #REF! | This file | #REF! | of | #REF! | | | | | | | |
|--|-----------|------------|------------|------------|------------|--------------|---------|---------|-------------------------------|---|-------------------|--------------------------|--------|-------|-----------|-----------|---------------------|---------------------|----------------------|---------------------|--------------------------|-------------------|
| Basics Input= Bold Ts(20-80) 19.9 ps Case: 850nm serial newMMF Q= 4.30 Ts(10-90) 30 ps Target Target reach 0.15 km Base Rate= 25781 MBd RIN(OMA) -128 dB/Hz and L_start= 0.02 km RIN at MinER -136.0 dB/Hz graph L_inc= 0.01 km Wavelength Uc 840 nm RIN_Coeff= 0.70 Power Budget P= 8.00 dB Uv (see notes) 0.55 nm Det.Jitter 8.56 ps inc. DCD Connections C 1.50 dB Tx pwr OMA= -2.00 dBm DCD_DJ= 2.14 ps TP3 Pwr.Bud.-Conn.Loss 6.50 dB Min. Ext Ratio= 3.65 dB Effect. DJ= 0.18 (UI) ex DCD C1= 480 ns.MHz *Worst*ave.TxPwr -1.0 dBm MPN k(OMA) 0.3 Reflection Noise factor 0 no units Ext. ratio penalty 4.01 dBo Tx eye height 39.1% Effective Rate 27286 MBd Tx mask X1= 0.3 UI Refl Tx -12 dB Tb_eff= 37 ps X2= 0.4 UI ModalNoisePen 0.3 dB Effective Rec Eye 0.21 UI Y1= 0.25 Tx mask top 0.2 UI | | | | | | | | | | Fiber Attenuation= 3.5 dB/km Model/format rev #### of #REF! at 850 nm NomSens OMA -11.00 dBm Margin 0.45 dB at C_att= 1.00 Receive Refl Rx -12 dB Answer! 0.15 km Attenuation= 3.62 dB/km Rec_BW= 19,039 MHz Test Rx BW 19,039 MHz at 840 nm c_rx 329 ns.MHz Disp. min. Uo= 1316 nm T_rx(10-90) 17.3 ps Test Source ER= Disp. So= 0.10275 ps/nm^2*km TP4 Eye 8 ps Test Tx 6.5 dB Disp. D1= -108.41 ps/(nm.km) Opening (=Tx eye) TestERper 1.98 dBo γ = 1.0 RMS Baseline wander SD 0.013 fraction of 1/2 eye (not in use) 10 V.E.C.P. 4.00 dBo BWm= 4500 MHz*km P_BLW(no ISI) 0.01 dB Stressed Eff. BWm= 4.5E+03 MHz*km P_BLW 0.01 dB Rx sens | | | | | | | | | | | | |
| L (km) | Patt (dB) | Ch IL (dB) | D1.L ps/nm | D2.L ps/nm | BWcd (MHz) | effBWm (MHz) | Te (ps) | Tc (ps) | P Eye central corners J=0, dB | P_DJ central (dB) | P_DJ corners (dB) | Preflection central (dB) | Beta | SDmpn | Pmpn (dB) | Prin (dB) | Pcross central (dB) | Ptotal central (dB) | <Ptotal corners (dB) | LP Pen central (dB) | 10GbE Method Margin (dB) | OMA central (dBm) |
| 0.002 | 0.01 | 1.51 | -0.22 | 0.00 | 2E+06 | 2.3E+06 | 30 | 35 | 1.90 | 0.24 | 0.17 | 0.61 | -1E-02 | 0.00 | 0.00 | 0.34 | -0.17 | 2.20 | 2.88 | 2.2 | 4.3 | -4.5 |
| 0.02 | 0.07 | 1.57 | -2.2 | 0.00 | 156,810 | 225,000 | 30 | 35 | 1.93 | 0.24 | 0.17 | 0.61 | 0 | 0.00 | 0.00 | 0.34 | 0.07 | 2.9 | 3.6 | 2.8 | 3.6 | -4.7 |
| 0.03 | 0.11 | 1.61 | -3.3 | 0.00 | 104,540 | 150,000 | 31 | 35 | 1.98 | 0.24 | 0.17 | 0.61 | 0 | 0.00 | 0.00 | 0.34 | 0.07 | 3.0 | 3.6 | 2.9 | 3.5 | -4.7 |
| 0.04 | 0.14 | 1.64 | -4.3 | 0.00 | 78,405 | 112,500 | 31 | 36 | 2.03 | 0.24 | 0.17 | 0.61 | 0 | 0.01 | 0.00 | 0.34 | 0.07 | 3.1 | 3.7 | 2.9 | 3.4 | -4.8 |
| 0.05 | 0.18 | 1.68 | -5.4 | 0.00 | 62,724 | 90,000 | 32 | 36 | 2.11 | 0.24 | 0.17 | 0.61 | 0 | 0.01 | 0.01 | 0.33 | 0.07 | 3.2 | 3.9 | 3.0 | 3.3 | -4.8 |
| 0.06 | 0.22 | 1.72 | -6.5 | 0.00 | 52,270 | 75,000 | 32 | 37 | 2.20 | 0.24 | 0.17 | 0.61 | 0 | 0.02 | 0.01 | 0.33 | 0.08 | 3.3 | 4.0 | 3.1 | 3.2 | -4.9 |
| 0.07 | 0.25 | 1.75 | -7.6 | 0.00 | 44,803 | 64,286 | 33 | 37 | 2.31 | 0.24 | 0.17 | 0.61 | 0 | 0.03 | 0.03 | 0.33 | 0.08 | 3.5 | 4.2 | 3.22 | 3.0 | -4.9 |
| 0.08 | 0.29 | 1.79 | -8.7 | 0.00 | 39,202 | 56,250 | 34 | 38 | 2.44 | 0.25 | 0.17 | 0.62 | 0 | 0.03 | 0.04 | 0.33 | 0.09 | 3.7 | 4.4 | 3.4 | 2.8 | -5.0 |
| 0.09 | 0.33 | 1.83 | -9.8 | 0.00 | 34,847 | 50,000 | 35 | 39 | 2.58 | 0.25 | 0.17 | 0.62 | 0 | 0.04 | 0.07 | 0.34 | 0.11 | 3.9 | 4.6 | 3.6 | 2.6 | -5.0 |
| 0.10 | 0.36 | 1.86 | -10.8 | 0.00 | 31,362 | 45,000 | 36 | 39 | 2.75 | 0.25 | 0.17 | 0.62 | 0 | 0.05 | 0.10 | 0.35 | 0.12 | 4.1 | 4.8 | 3.8 | 2.4 | -5.1 |
| 0.11 | 0.40 | 1.90 | -11.9 | 0.00 | 28,511 | 40,909 | 37 | 40 | 2.93 | 0.25 | 0.17 | 0.62 | 0 | 0.06 | 0.14 | 0.36 | 0.15 | 4.4 | 5.1 | 4.0 | 2.1 | -5.2 |
| 0.12 | 0.43 | 1.93 | -13.0 | 0.00 | 26,135 | 37,500 | 38 | 41 | 3.12 | 0.25 | 0.17 | 0.63 | 0 | 0.07 | 0.18 | 0.37 | 0.18 | 4.8 | 5.5 | 4.3 | 1.7 | -5.3 |
| 0.13 | 0.47 | 1.97 | -14.1 | 0.01 | 24,125 | 34,615 | 39 | 42 | 3.34 | 0.25 | 0.17 | 0.63 | 0 | 0.08 | 0.24 | 0.39 | 0.22 | 5.1 | 5.9 | 4.7 | 1.4 | -5.5 |
| 0.14 | 0.51 | 2.01 | -15.2 | 0.01 | 22,401 | 32,143 | 40 | 44 | 3.57 | 0.25 | 0.17 | 0.64 | 0 | 0.08 | 0.31 | 0.42 | 0.28 | 5.6 | 6.3 | 5.1 | 0.9 | -5.6 |
| 0.15 | 0.54 | 2.04 | -16.3 | 0.01 | 20,908 | 30,000 | 41 | 45 | 3.83 | 0.26 | 0.17 | 0.65 | 0 | 0.09 | 0.39 | 0.45 | 0.36 | 6.0 | 6.8 | 5.5 | 0.5 | -5.8 |
| 0.16 | 0.58 | 2.08 | -17.3 | 0.01 | 19,601 | 28,125 | 42 | 46 | 4.10 | 0.26 | 0.18 | 0.66 | 0 | 0.10 | 0.48 | 0.50 | 0.46 | 6.6 | 7.3 | 6.0 | -0.1 | -6.0 |