

IEEE 802.3af DTE Power via MDI

PD AC Input impedance – Sensitivity Analysis

AD HOC A.I. 2.3

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- Acknowledgments to Pavlik Rimboim and Asher Biton/PowerDsine



Objectives

- Vac_close vs. PD input ac impedance
- PD input ac impedance – design equations
- Lab tests, simulations and equations verification



Test setup – PSE side

PARAMETERS:

$C_{pse} = 0.22\mu\text{F}$

$C_{probe} = 10\mu\text{F}$

$R_{pse} = 400\text{k}$

$R_{probe} = 7.5\text{K}$

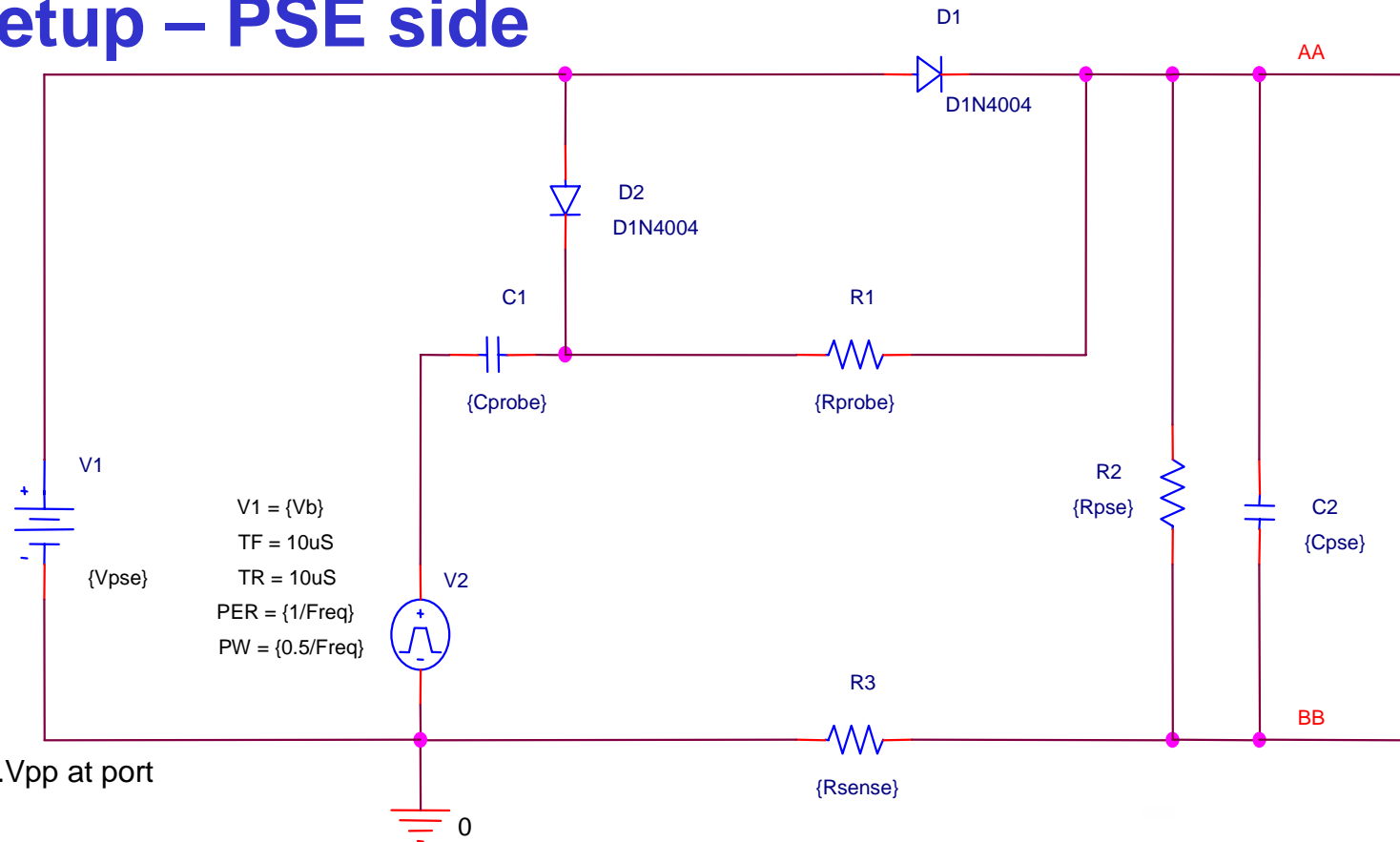
$R_{sense} = 2$

$\text{Freq} = 125$

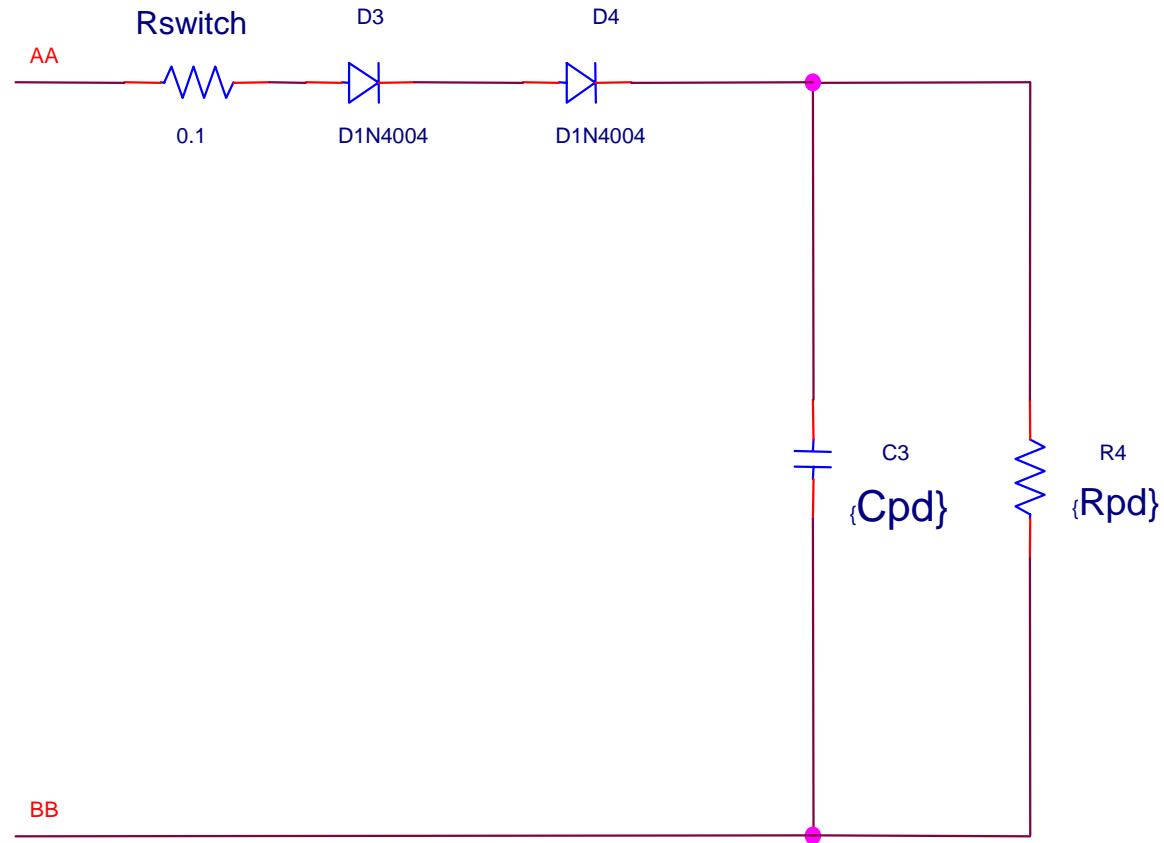
$V_{pse} = 49$

$D1, D2 = 1\text{N}4004$

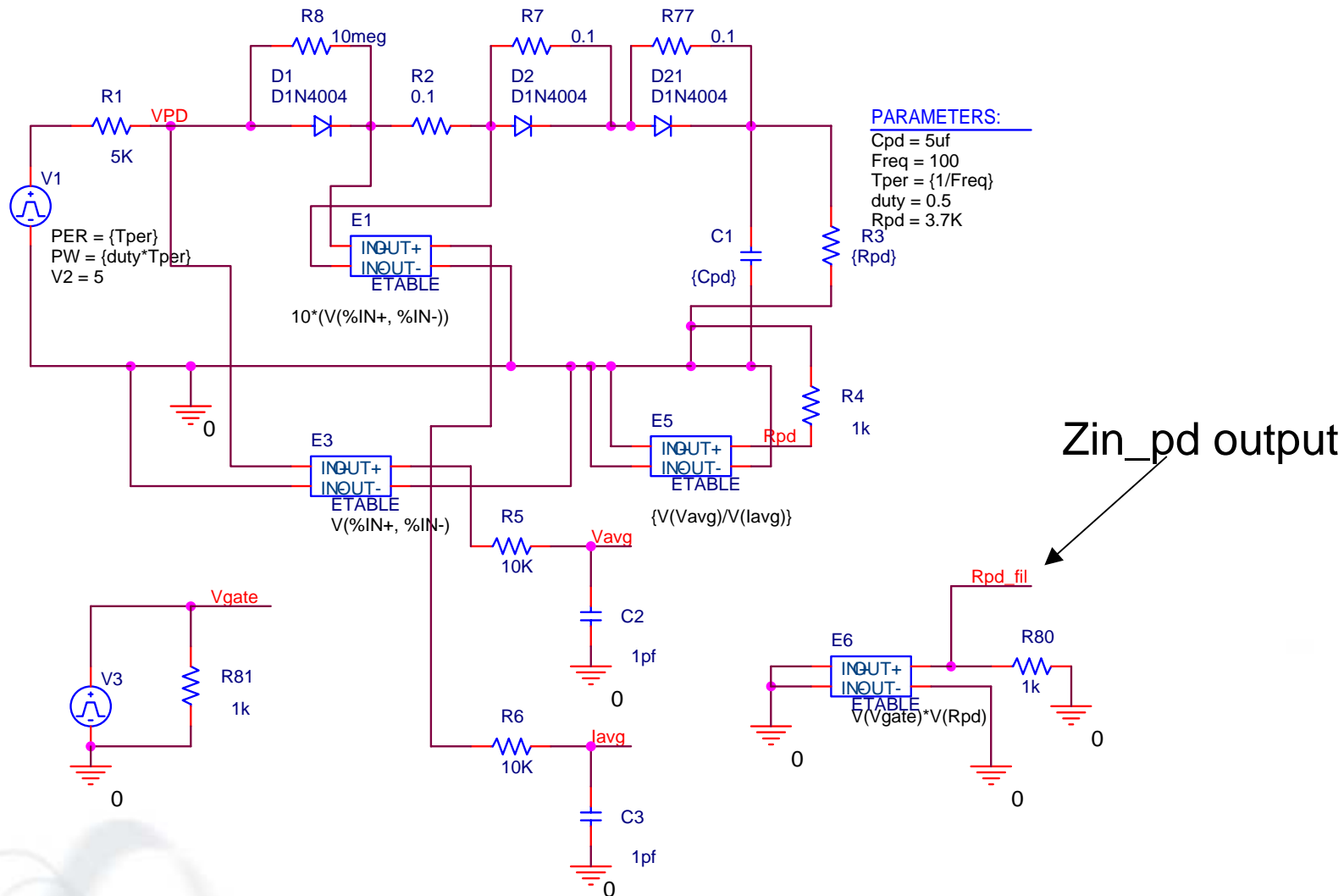
$V_b = \text{set to have } 4.4 \cdot V_{pp} \text{ at port}$



Test setup – PD side



Analysis of PD input impedance



Deriving Zin_pd- part A

$$\frac{V_{pd}}{V_s} = \frac{Z_{in_pd}}{Z_{in_pd} + R1} = \alpha \quad \text{Eq-1}$$

$$\frac{V_{pd}}{V_s} = \alpha \quad \text{Eq-2}$$

$$Z_{in_pd} = \frac{\alpha}{1-\alpha} \cdot R1 \quad \text{Eq-3}$$

$$V_{pd} = N \cdot V_d + 0.5 \cdot v1 + 0.5 \cdot v2$$

$$V_{pd} = N \cdot V_d + v1$$

$$v1 = \frac{V_{eqv} \cdot \left[1 - e^{-\frac{-D \cdot T}{\tau1}} \right]}{1 - e^{-\frac{-D \cdot T}{\tau1}} \cdot e^{-\frac{-(1-D) \cdot T}{\tau2}}}$$

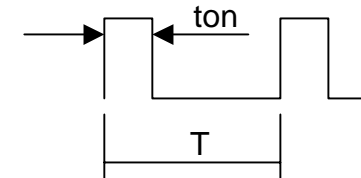
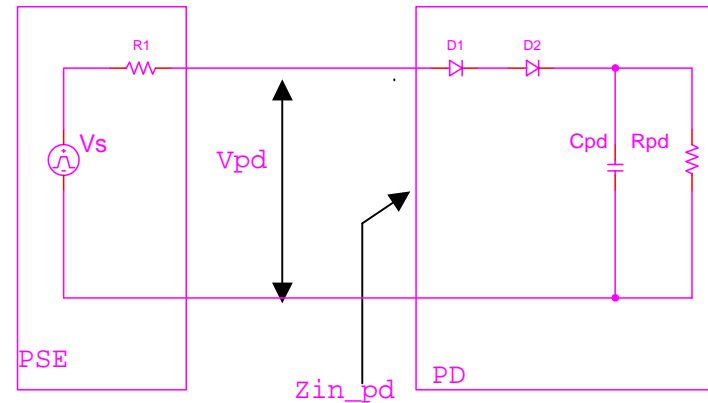
$$v2 = v1 \cdot \left[e^{-\frac{-(1-D) \cdot T}{\tau2}} \right]$$

$$V_{eqv} = \frac{(V_s - N \cdot V_d) \cdot R_{pd}}{R_{pd} + R1}$$

$$\tau1 = \frac{R1 \cdot R_{pd}}{R_{pd} + R1} \cdot C_{pd}$$

$$\tau2 = R_{pd} \cdot C_{pd} \quad \text{For } N > 0$$

$$\tau2 = \tau1 \quad \text{For } N = 0$$



For $N > 0$, $\text{toff} < \tau2$. Eq-4

For $N > 0$, $\text{toff} > \tau2$. Eq-5

V_s = pulse source

F = frequency,

$D = \text{ton}/T$

$T = 1/f$

$T_r = t_f \ll T$

N = number of series diode in the PD

V_d = diode forward voltage drop



Deriving Z_{in_pd} - part B

For $\tau_2 < t_{off}$ $\rightarrow v_1(t) = V_{eqv}$ $\rightarrow V_{pd} = N \cdot V_d + V_{eqv}$

$\rightarrow Z_{in_pd} = R_1 \cdot (N \cdot V_d + V_{eqv}) / (1 - N \cdot V_d + V_{eqv})$

\rightarrow For $N=0$ $\rightarrow Z_{in_pd} = R_{pd}$

\rightarrow For $N > 0$ $\rightarrow Z_{in} > R_{pd}$ due to the diode drop in series to R_{pd} .

\rightarrow For $\tau_2 > t_{off}$, the RC filter is integrate the voltage across C_{pd} by averaging it.

\rightarrow In this case $Z_{in_pd} < R_{pd}$ or $Z_{in_pd} > R_{pd}$ pending on all parameters

\rightarrow The highest impedance occur for $N = N_{max}$ and $\tau_2 < t_{off}$, $\rightarrow Z_{in_pd} > R_{pd}$



Worst case PD input ac impedance w/o DC bias

- R_{pd_min} at normal powering mode = $37/10\text{mA}=3.7\text{K}$
- R_{pd_max} at normal powering mode = $57/10\text{mA} = 5.7\text{K}$
- C_{pd} varies from $5\mu\text{F}$ to $500\mu\text{F}$
- $1\text{Hz} < f < 500\text{Hz}$
- Z_{in_pd} max with 3 series diode = 10.97K



Lab tests

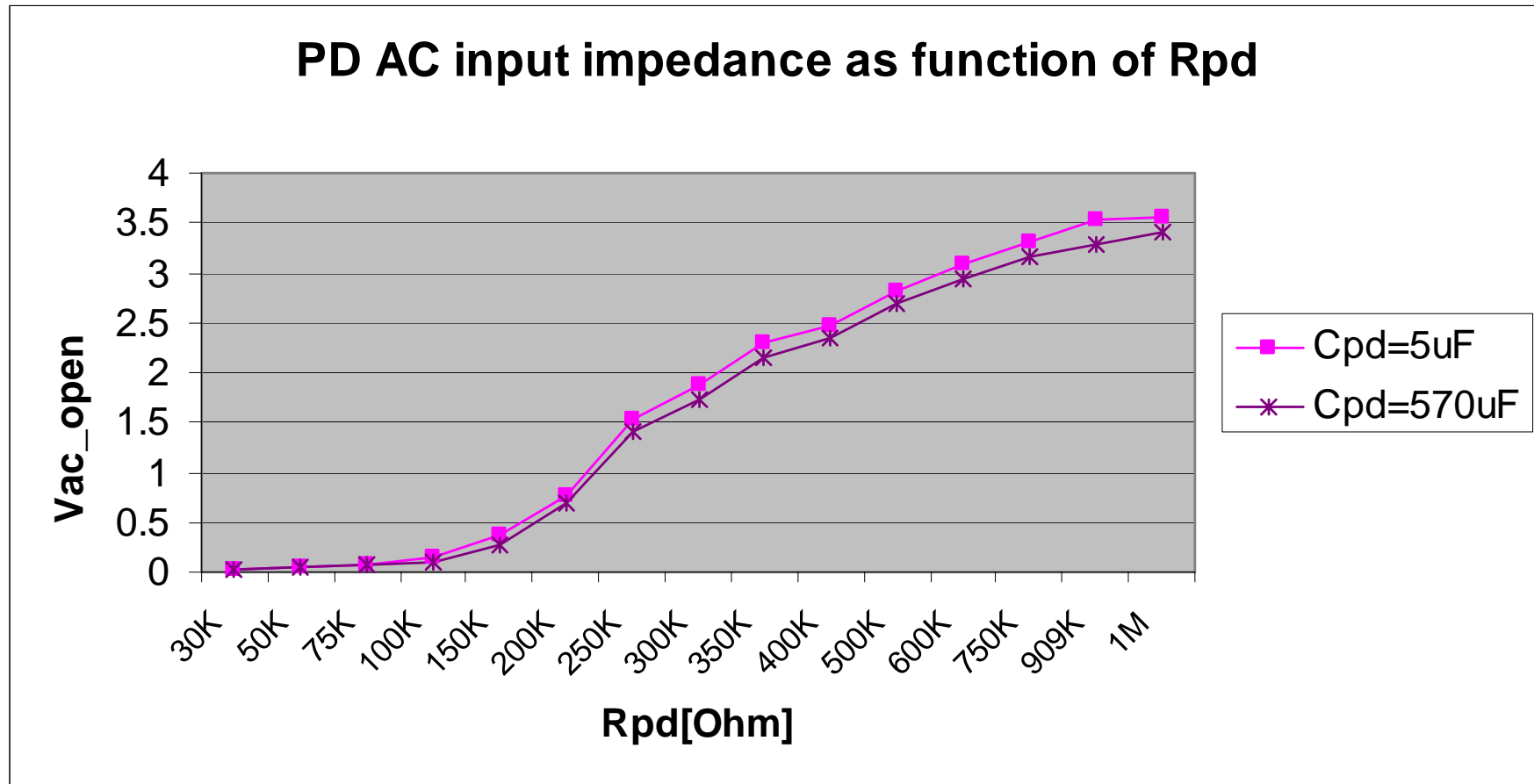
- Changing Rpd and measuring PSE port ac voltage, Vac_close.

Test Conditions

- With DC bias
- Vac_open=4.4Vpp, F=125Hz
- Changing Rpd from 30K to 1MEG.



Lab Test Results



Summary and Conclusions

- Vac_close is kept low for wide rang of PD input ac impedance
 - Not sensitive the external noise source when PD is connected
- Similar behavior for Cpd=5uF and up.
- PD input ac impedance is well defined in IEEE802.3af , table 12.



Calculations and Simulations verifications



Calculation example

Step 1, For :

* N=0 (NO DIODES IN SERIES)

* Voltage across C always > 0 (Tau2>Toff)

$$\begin{aligned}
 R1 &:= 5000 & V_s &:= 5 & N &:= 0 & D &:= 0.5 \\
 R_{pd} &:= 5000 & V_d &:= 0.55 & f &:= 100 \\
 C_{pd} &:= 0.000005 & T_s &:= \frac{1}{f} & \text{toff} &:= (1-D) \cdot T_s \\
 \tau_1 &:= R1 \cdot \frac{R_{pd} \cdot C_{pd}}{R1 + R_{pd}} & \tau_2 &:= \tau_1 & V_{eqv} &:= (V_s - N \cdot V_d) \cdot \frac{R_{pd}}{R1 + R_{pd}} \\
 \tau_1 &= 0.013 & \tau_2 &= 0.013 & V_{eqv} &= 2.5
 \end{aligned}$$

Check if Tau2>Toff if not, jump to step 3 $\tau_2 = 0.013$ $\text{toff} = 5 \cdot 10^{-3}$

$$V1 := V_{eqv} \cdot \frac{\left(1 - \exp\left(-D \cdot \frac{T_s}{\tau_1}\right)\right)}{1 - \left(\exp\left(-D \cdot \frac{T_s}{\tau_1}\right)\right) \cdot \left[\exp\left[-(1-D) \cdot \frac{T_s}{\tau_2}\right]\right]}$$

$$V2 := V1 \cdot \exp\left[-(1-D) \cdot \frac{T_s}{\tau_2}\right]$$

$$V_{avg} := (V1 + V2) \cdot 0.5 \quad \text{Ripple} := V1 - V2$$

$$V_{avg} = 1.25 \quad \text{Ripple} = 0.493 \text{ Vpp} \quad V1 = 1.497$$

$$V_{pd} := N \cdot V_d + V_{avg}$$

$$\begin{aligned}
 \text{alfa} &:= \frac{V_{pd}}{V_s} \\
 \text{alfa} &= 0.25
 \end{aligned}$$

$$Z_{in_pd} := \frac{\text{alfa} \cdot R1}{1 - \text{alfa}}$$

$$Z_{in_pd} = 1.667 \cdot 10^3 \quad \text{VERIFIED IN SIMULATIONS!!!}$$



Step 2, For :

* N>0 (DIODES IN SERIES)

* Voltage across C always > 0 (Tau2>>Toff)

$$\begin{aligned}
 R1 &:= 5000 & V_s &:= 5 & N &:= 1 & D &:= 0.5 \\
 R_{pd} &:= 5000 & V_d &:= 0.55 & f &:= 100 \\
 C_{pd} &:= 0.000005 & T_s &:= \frac{1}{f} & \text{toff} &:= (1-D) \cdot T_s \\
 \tau_1 &:= R1 \cdot \frac{R_{pd} \cdot C_{pd}}{R1 + R_{pd}} & \tau_2 &:= R_{pd} \cdot C_{pd} & V_{eqv} &:= (V_s - N \cdot V_d) \cdot \frac{R_{pd}}{R1 + R_{pd}} \\
 \tau_1 &= 0.013 & \tau_2 &= 0.025
 \end{aligned}$$

Check if Tau2>Toff if not, jump to step 3 $\tau_2 = 0.025$ $\text{toff} = 5 \cdot 10^{-3}$

$$V1 := V_{eqv} \cdot \frac{\left(1 - \exp\left(-D \cdot \frac{T_s}{\tau_1}\right)\right)}{1 - \left(\exp\left(-D \cdot \frac{T_s}{\tau_1}\right)\right) \cdot \left[\exp\left[-(1-D) \cdot \frac{T_s}{\tau_2}\right]\right]}$$

$$V2 := V1 \cdot \exp\left[-(1-D) \cdot \frac{T_s}{\tau_2}\right]$$

$$V1 = 1.626 \quad V2 = 1.331$$

$$V_{avg} := (V1 + V2) \cdot 0.5 \quad \text{Ripple} := V1 - V2$$

$$V_{avg} = 1.478 \quad \text{Ripple} = 0.295 \text{ Vpp}$$

$$V_{pd} := N \cdot V_d + V_{avg}$$

$$V_{pd} = 2.028$$

$$\text{alfa} := \frac{V_{pd}}{V_s}$$

$$Z_{in_pd} := \frac{\text{alfa} \cdot R1}{1 - \text{alfa}}$$

$$Z_{in_pd} = 3.413 \cdot 10^3 \quad \text{VERIFIED IN SIMULATIONS!!!}$$

Calculation example

Step 3, For :

* $N > 0$ (DIODES IN SERIES)

* Voltage across C approach zero before new cycle starts ($\tau_2 \ll T_{off}$)

$$R1 := 5000 \quad V_s := 5 \quad N := 1 \quad D := 0.5$$

$$R_{pd} := 5000 \quad V_d := 0.55 \quad f := 1$$

$$C_{pd} := 0.000005 \quad T_s := \frac{1}{f} \quad \text{toff} := (1 - D) \cdot T_s$$

$$\tau_1 := R1 \cdot \frac{R_{pd} \cdot C_{pd}}{R1 + R_{pd}} \quad \tau_2 := R_{pd} \cdot C_{pd} \quad V_{eqv} := (V_s - N \cdot V_d) \cdot \frac{R_{pd}}{R1 + R_{pd}}$$

$$\tau_1 = 0.013 \quad \tau_2 = 0.025 \quad V_{eqv} = 2.225$$

Check if $\tau_2 < T_{off}$ if not, jump to step 2 $\tau_2 = 0.025$ $\text{toff} = 0.5$

$$V1 := V_{eqv} \cdot \frac{\left(1 - \exp\left(-D \cdot \frac{T_s}{\tau_1}\right)\right)}{1 - \left(\exp\left(-D \cdot \frac{T_s}{\tau_1}\right)\right) \cdot \left[\exp\left[-(1 - D) \cdot \frac{T_s}{\tau_1}\right]\right]}$$

$$V2 := V1 \cdot \exp\left[-(1 - D) \cdot \frac{T_s}{\tau_2}\right]$$

$$V1 = 2.225 \quad V2 = 4.586 \cdot 10^{-9} \quad \text{Ripple} := V1 - V2 \quad V_{pd} := N \cdot V_d + V1$$

$$\text{Ripple} = 2.225 \quad V_{pp} \quad V_{pd} = 2.775$$

$$\text{alfa} := \frac{V_{pd}}{V_s}$$

$$Z_{in_pd} := \frac{\text{alfa} \cdot R1}{1 - \text{alfa}}$$

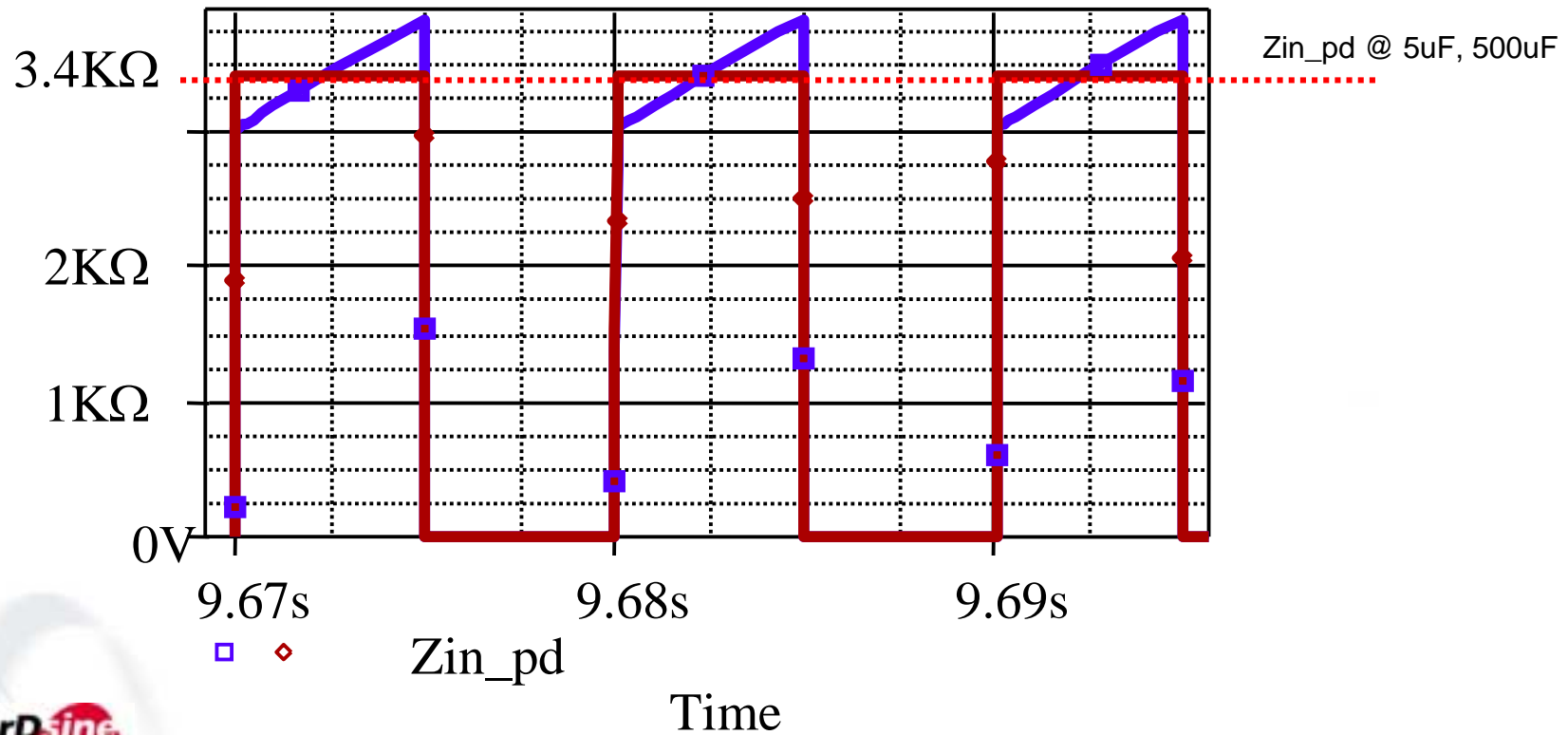
$$Z_{in_pd} = 6.236 \cdot 10^3 \quad \text{VERIFIED IN SIMULATIONS!!!}$$



Checking the equations:

Z_{in_pd} @ $T < \tau_1, \tau_2$; $N=0$, $R_{pd}=5K$, $C_{pd}=5\mu F$, $f=100Hz$, $D=50\%$

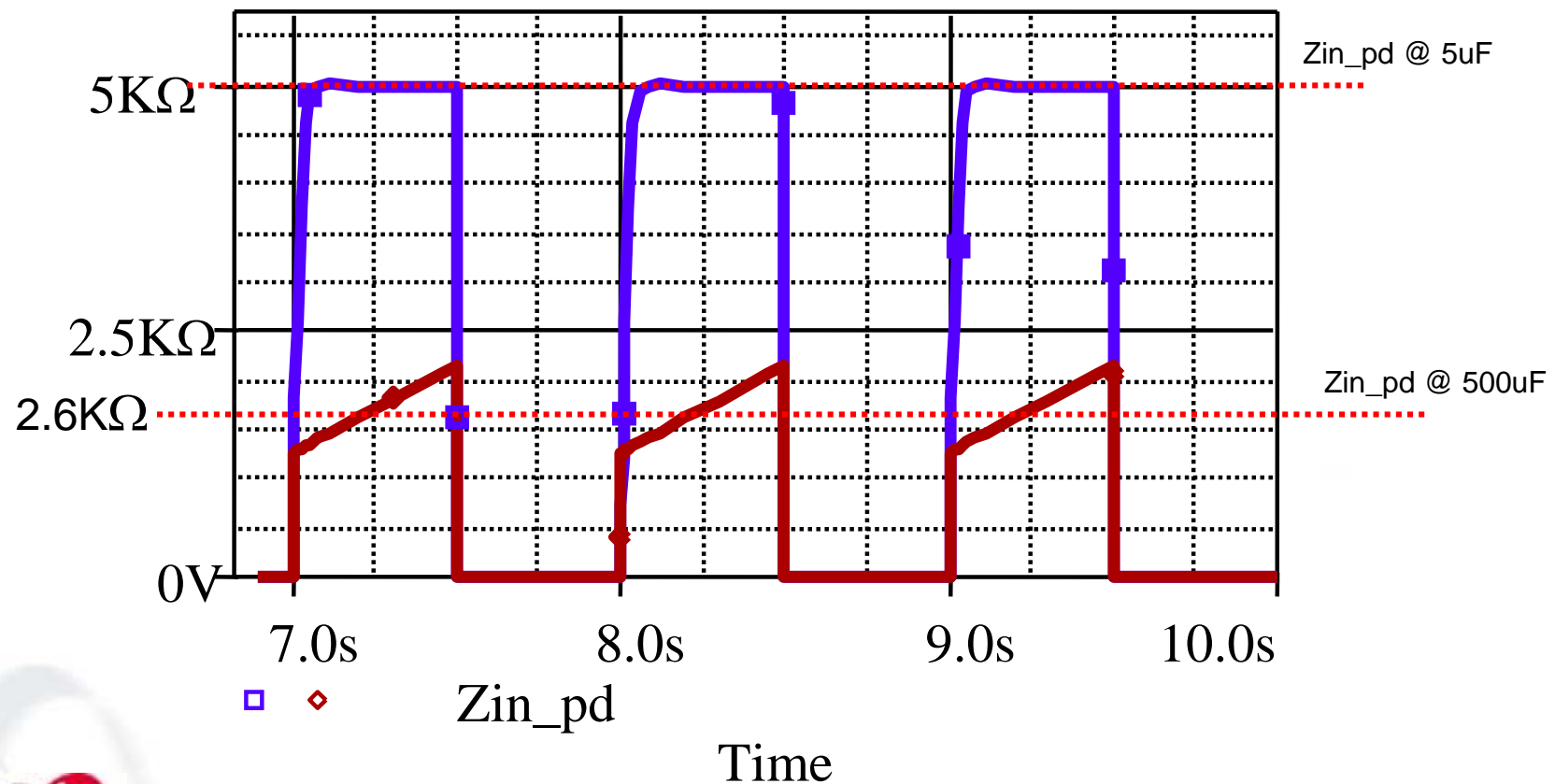
Z_{in_pd} @ $T < \tau_1, \tau_2$; $N=0$, $R_{pd}=5K$, $C_{pd}=500\mu F$, $f=100Hz$, $D=50\%$



Checking the equations:

Z_{in_pd} @ $T \gg \tau_1, \tau_2$; $N=0$, $R_{pd}=5K$, $C_{pd}=5\mu F$, $f=1Hz$, $D=50\%$

Z_{in_pd} @ $T < \tau_1, \tau_2$; $N=0$, $R_{pd}=5K$, $C_{pd}=500\mu F$, $f=1Hz$, $D=50\%$



Checking the equations:

Z_{in_pd} @ $T \gg \tau_1, \tau_2$; $N=3$, $R_{pd}=5K$, $C_{pd}=5\mu F$, $f=1Hz$, $D=50\%$

Z_{in_pd} @ $T < \tau_1, \tau_2$; $N=3$, $R_{pd}=5K$, $C_{pd}=500\mu F$, $f=1Hz$, $D=50\%$

