## Adding a Simple Package Model to the Channel Response

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## Supporters

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## In support of comment 36, 129, 132 resolution

- Eliminate the problem caused by looking at the signal the package/board interface (aka bga ball).
- It causes a shelf on the SBR edge which is correct at the ball but not at the pad. It causes too much precursor equalization with reduces the available signal.
- The caveat is that the Rx package loss is added back in because exact s-parameter concatenation replaces the VTF (voltage transfer function)
- Such impairments cannot be addressed adequately with guard band.
- To help specify Tx and Rx Return loss using the test fixture
- Enable changes for and review of COM code as these values may change through the ballot process as RL speciation evolve (comment 129 132)
- Provide potential applicability to other IEEE standards (like CAUI).
- Provide direct understandable physical implementation rational
- This would suggest not how to build a package, but in the line of $T x / R x$ architecture,
- provide a package architecture to be use in COM with a clear relationship to the $T x / R x$ RL spec
- Define a model for COM that is understandable and alterable with a table


## Simplest Useful Package Modeling



## Estimate differential s-parameters for a small segment of uniform lossy transmission line

 (replaces 93A.1.2)- Segment can be either solved or measured.
- Recommend: 1mm package transmission line s4p file
- Fit RL and IL using clause 93A. 2
- Find $\mathrm{a}_{\mathrm{il}}$ and $\mathrm{a}_{\mathrm{ff}}$ from S11 and s21
- Determine $\gamma_{I L}$ and $\gamma_{R L}$
- Were $\gamma_{x}=a 0+a 1 \cdot \sqrt{f}+a 2 \cdot f+a 4 \cdot f^{2}$
- This form is from clause 93A.2, eq. (93A-31)
- For the transmission line
- $s 11$ tline $=e^{\gamma_{R L}}\left[\sum_{n=1}^{\text {Segments }} e^{\left.\gamma_{I L \cdot(2 \cdot n-2)}\right]}\right.$
- s21tline $=e^{\gamma_{i L} \text { segements }}$
- i.e. [ $\mathrm{S}_{\text {tine }}$ ]
- The package transmission line is defined by 9 parameters in a table in 93a.1.2
- $a_{i l}(0,1,2,4), a_{r \mid}(0,1,2,4)$, number of segments (Pkg_length in mm)


## Comparison for 12 mm line between math estimated and circuit model

## Example of an estimated package and tline model



## Create s parameters for pad and ball (more replacements for 93A.1.2)

- Zpad $=\frac{1}{2 * \pi * i * f * \text { Cdiepad }}$
- $s 11_{p a d}=\frac{2 * Z 0}{Z_{p a d}+2 * Z 0}, s 21_{p a d}=\frac{2 * Z p a d}{Z_{p a d}+2 * Z 0} \rightarrow\left[\mathrm{~S}_{\text {pad }}\right]$
- $Z_{\text {ball }}=\frac{1}{2 * \pi * i * f * C p k g_{-} \text {board }}$
- $s 11_{\text {ball }}=\frac{2 * Z 0}{Z_{\text {ball }}+2 * Z 0}, s 21_{\text {pad }}=\frac{2 * \text { Zball }}{Z_{\text {ball }}+2 * Z 0} \rightarrow$ [Sball]
- $\Gamma_{1}=\Gamma_{2}=\frac{\text { Z0 }- \text { Rdiepad }}{\text { Z0+Rdiepad }}$
- 3 parameters: Rdiepad, Cdiepad, Cpkg_board


## Combining 2 port S parameters

Given $\left[\mathrm{S}_{1}\right]$ and $\left[\mathrm{S}_{2}\right]$
First convert to T matrixes

$$
\left[T_{1}\right]=\left[\begin{array}{cc}
\frac{1}{s 21_{1}} & \frac{s 22_{1}}{s 21_{1}} \\
\frac{s 11_{1}}{s 21_{1}} & \frac{s 11_{1} \cdot s 22_{1}-s 12_{1} \cdot s 21_{1}}{s 21_{1}}
\end{array}\right] \quad\left[T_{2}\right]=\left[\begin{array}{cc}
\frac{1}{s 21_{2}} & \frac{s 22_{2}}{s 21_{2}} \\
\frac{s 11_{2}}{s 21_{2}} & \frac{s 11_{2} \cdot s 22_{2}-s 12_{2} \cdot s 21_{2}}{s 21_{2}}
\end{array}\right]
$$

Combine T matrixes

$$
\begin{gathered}
{\left[T_{3}\right]=\left[T_{1}\right] *\left[T_{2}\right]} \\
\text { Determine }\left[\mathrm{S}_{3}\right] \\
{\left[S_{3}\right]=\left[\begin{array}{cc}
\frac{t 21_{3}}{t 11_{3}} & \frac{t 11_{3} \cdot t 22_{3}-t 12_{3} \cdot t 21_{3}}{t 11_{3}} \\
\frac{1}{t 11_{3}} & \frac{-t 12_{3}}{t 11_{3}}
\end{array}\right]}
\end{gathered}
$$

## Combine parameters (replaces eq. 96a-5)

- $\left[\mathrm{S}_{\mathrm{pkgtx}}\right]=$ combine $\left(\left[\right.\right.$ combine $\left(\left[\mathrm{S}_{\mathrm{pad}}\right],\left(\left[\mathrm{S}_{\mathrm{tline}}\right]\right),\left[\mathrm{S}_{\text {ball }}\right]\right)$
- Create $\left[T_{p k g t x}\right] \rightarrow\left[\mathrm{S}_{\mathrm{pkgtx}}\right]$
- $\left[\mathrm{S}_{\mathrm{pkgrx}}\right]=$ combine $\left(\left[\mathrm{S}_{\text {ball }}\right.\right.$, combine $\left(\left[\mathrm{S}_{\text {tline }}\right]\right.$, $\left.\left[\mathrm{S}_{\mathrm{pad}}\right]\right)$
- Create [ $T_{\text {pkgrx }}$ ]
- Channel response:
- $[T]=\left[T_{\text {pkgtx }}\right]^{*}\left[T_{\text {channel }}\right]{ }^{*}\left[T_{\text {pkgrx }}\right] \rightarrow[S]$
- $H_{21}=\frac{S_{21}\left(1-\Gamma_{1}\right)\left(1+\Gamma_{2}\right)}{1-S_{11} \Gamma_{1}-S_{22} \Gamma_{2}-S_{21} S_{12} \Gamma_{1} \Gamma_{2}+S_{11} \Gamma_{1} S_{22} \Gamma_{2}}$


## Commercial simulation circuit used to examine response with proposed COM package at tp0a



## 25Gbps NRZ eye diagram at tpOa suggests removing transmitter filter from COM is OK because the package and die load limits transition time



## Parameters (Table 93A-2)

| a_il_0 | $-4.453 \mathrm{e}-4+4.467 \mathrm{e}-05 \mathrm{i}$ |
| :--- | :--- |
| a_il_1 | $-1.049 \mathrm{e}-08-4.568 \mathrm{e}-08 \mathrm{i}$ |
| a_il_2 | $-6.409 \mathrm{e}-13-3.914 \mathrm{e}-11 \mathrm{i}$ |
| a_il_4 | $-1.669 \mathrm{e}-23+3.134 \mathrm{e}-23 \mathrm{i}$ |
| a_rl_0 | $-6.473-1.51 \mathrm{i}$ |
| a_rl_1 | $6.451 \mathrm{e}-05+3.351 \mathrm{e}-07 \mathrm{i}$ |
| a_rl_2 | $-2.712 \mathrm{e}-10-4.903 \mathrm{e}-11 \mathrm{i}$ |
| a_rl_4 | $2.167 \mathrm{e}-21+2.765 \mathrm{e}-22 \mathrm{i}$ |
| Cdiepad | 240 |
| Rdiepad | 55 |
| Cpkg_board | 180 |
| Pkg_len | 12 |

- a_il_0, 1,2 and 4 are insertion loss fit coefficients for $a_{i l}(0,1,2,4)$ on slide 5
- a_rl_0, 1, 2 and 4 are return loss fit coefficients for $a_{r l}(0,1,2,4)$ on slide 5
- Cdiepad, Rdiepad, Cpkg_board, and Pkg_len are the package parameter on slide 4
- Remove parameter $f_{v} f_{f}$ amd $f_{n}$ and associated clauses.

