

Adding a Simple Package Model to the Channel Response

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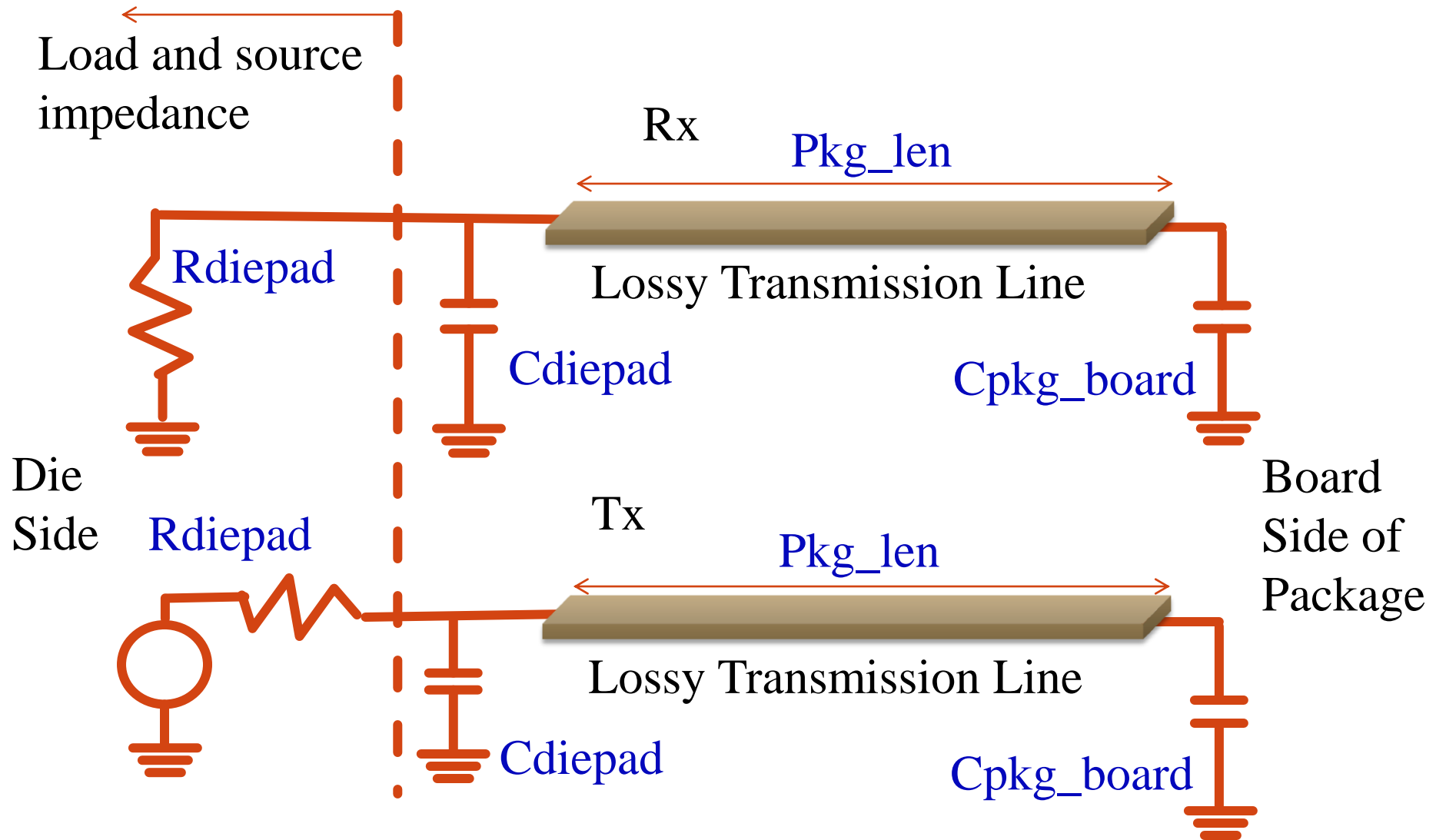
Supporters

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In support of comment 36, 129, 132 resolution

- Eliminate the problem caused by looking at the signal the package/board interface (aka bga ball).
 - It causes a shelf on the SBR edge which is correct at the ball but not at the pad. It causes too much precursor equalization with reduces the available signal.
 - The caveat is that the Rx package loss is added back in because exact s-parameter concatenation replaces the VTF (voltage transfer function)
 - Such impairments cannot be addressed adequately with guard band.
- To help specify Tx and Rx Return loss using the test fixture
 - Enable changes for and review of COM code as these values may change through the ballot process as RL speciation evolve (comment 129 132)
- Provide potential applicability to other IEEE standards (like CAUI).
- Provide direct understandable physical implementation rational
 - This would suggest not how to build a package, but in the line of Tx/Rx architecture,
 - provide a package architecture to be use in COM with a clear relationship to the Tx/Rx RL spec
- Define a model for COM that is understandable and alterable with a table

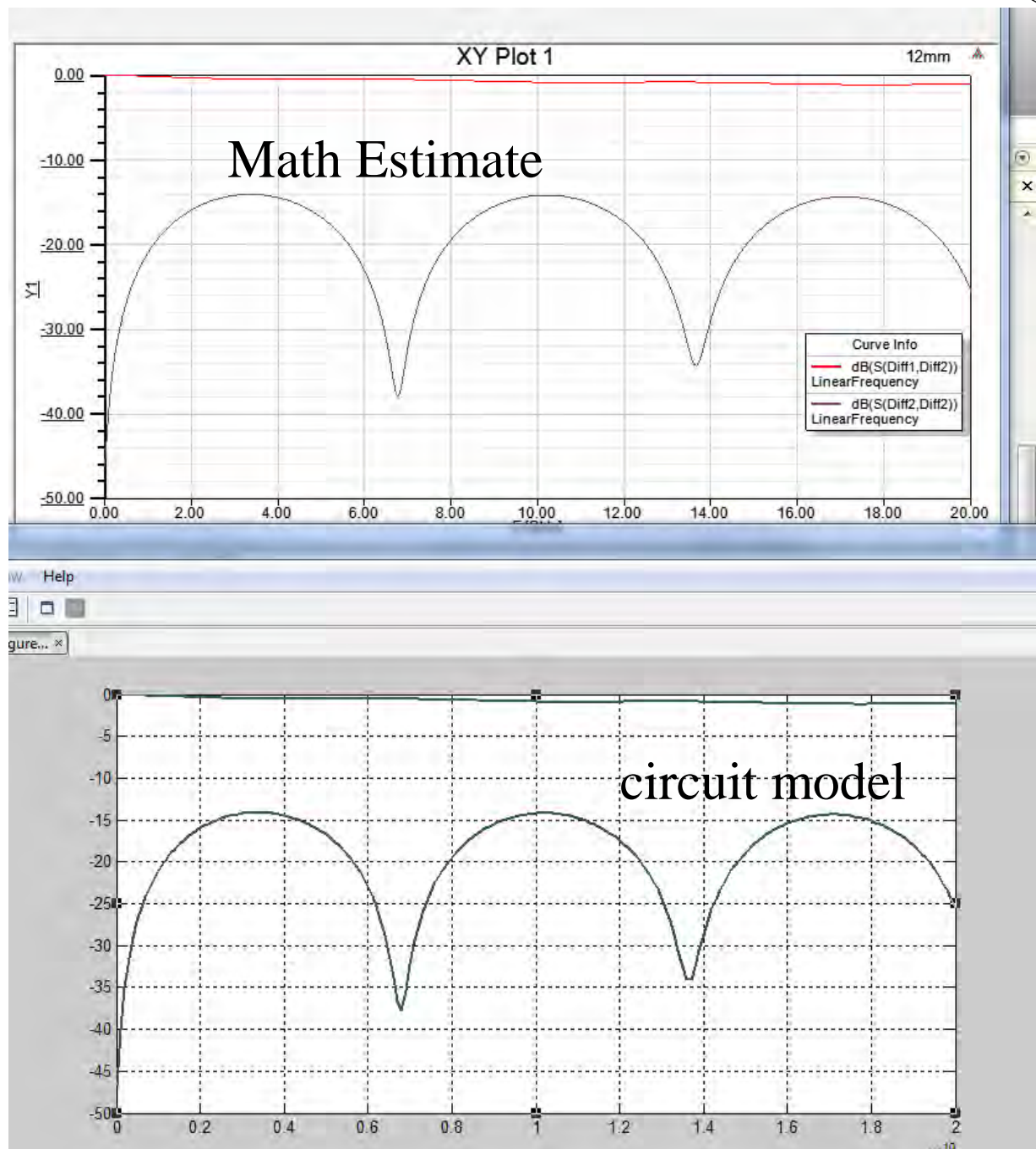
Simplest Useful Package Modeling



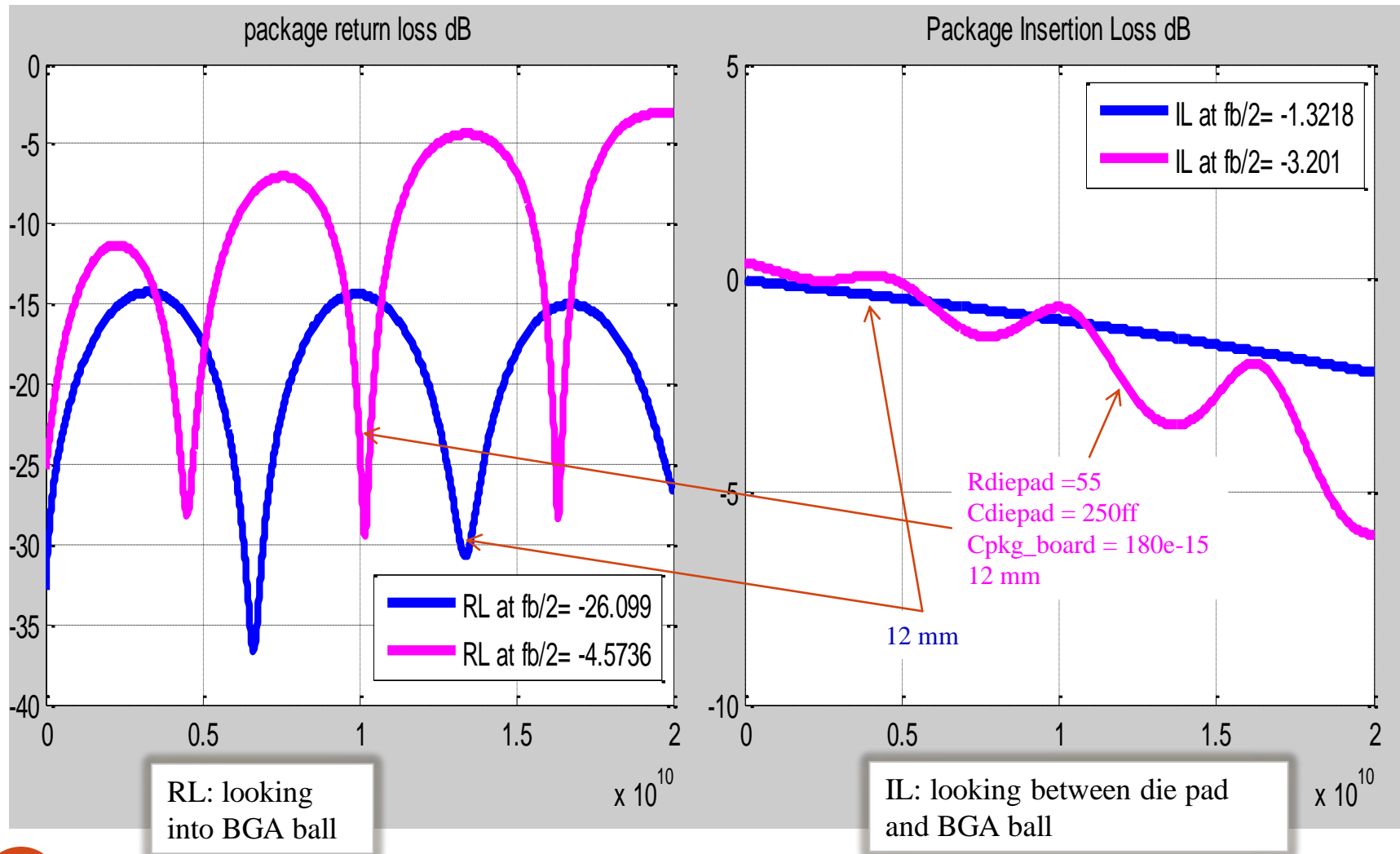
Estimate differential s-parameters for a small segment of uniform lossy transmission line (replaces 93A.1.2)

- Segment can be either solved or measured.
- Recommend: 1mm package transmission line s4p file
- Fit RL and IL using clause 93A.2
 - Find a_{il} and a_{rl} from S11 and s21
 - Determine γ_{IL} and γ_{RL}
 - Where $\gamma_x = a_0 + a_1 \cdot \sqrt{f} + a_2 \cdot f + a_4 \cdot f^2$
 - This form is from clause 93A.2, eq. (93A-31)
- For the transmission line
- $s_{11tline} = e^{\gamma_{RL}} \left[\sum_{n=1}^{segments} e^{\gamma_{IL} \cdot (2 \cdot n - 2)} \right]$
- $s_{21tline} = e^{\gamma_{IL} \cdot segments}$
- i.e. $[S_{tline}]$
- The package transmission line is defined by 9 parameters in a table in 93a.1.2
 - $a_{il}(0, 1, 2, 4)$, $a_{rl}(0, 1, 2, 4)$, number of segments (Pkg_length in mm)

Comparison for 12 mm line between math estimated and circuit model



Example of an estimated package and tline model



Create s parameters for pad and ball (more replacements for 93A.1.2)

- $Z_{pad} = \frac{1}{2 * \pi * i * f * C_{diepad}}$
- $s_{11_{pad}} = \frac{2 * Z_0}{Z_{pad} + 2 * Z_0}$, $s_{21_{pad}} = \frac{2 * Z_{pad}}{Z_{pad} + 2 * Z_0} \rightarrow [S_{pad}]$
- $Z_{ball} = \frac{1}{2 * \pi * i * f * C_{pkg_board}}$
- $s_{11_{ball}} = \frac{2 * Z_0}{Z_{ball} + 2 * Z_0}$, $s_{21_{ball}} = \frac{2 * Z_{ball}}{Z_{ball} + 2 * Z_0} \rightarrow [S_{ball}]$
- $\Gamma_1 = \Gamma_2 = \frac{Z_0 - R_{diepad}}{Z_0 + R_{diepad}}$
- 3 parameters: R_{diepad} , C_{diepad} , C_{pkg_board}

Combining 2 port S parameters

Given $[S_1]$ and $[S_2]$
First convert to T matrixes

$$[T_1] = \begin{bmatrix} \frac{1}{s21_1} & \frac{s22_1}{s21_1} \\ \frac{s11_1}{s21_1} & \frac{s11_1 \cdot s22_1 - s12_1 \cdot s21_1}{s21_1} \end{bmatrix} \quad [T_2] = \begin{bmatrix} \frac{1}{s21_2} & \frac{s22_2}{s21_2} \\ \frac{s11_2}{s21_2} & \frac{s11_2 \cdot s22_2 - s12_2 \cdot s21_2}{s21_2} \end{bmatrix}$$

Combine T matrixes

$$[T_3] = [T_1] * [T_2]$$

Determine $[S_3]$

$$[S_3] = \begin{bmatrix} \frac{t21_3}{t11_3} & \frac{t11_3 \cdot t22_3 - t12_3 \cdot t21_3}{t11_3} \\ 1 & -t12_3 \\ \frac{1}{t11_3} & \frac{t11_3}{t11_3} \end{bmatrix}$$

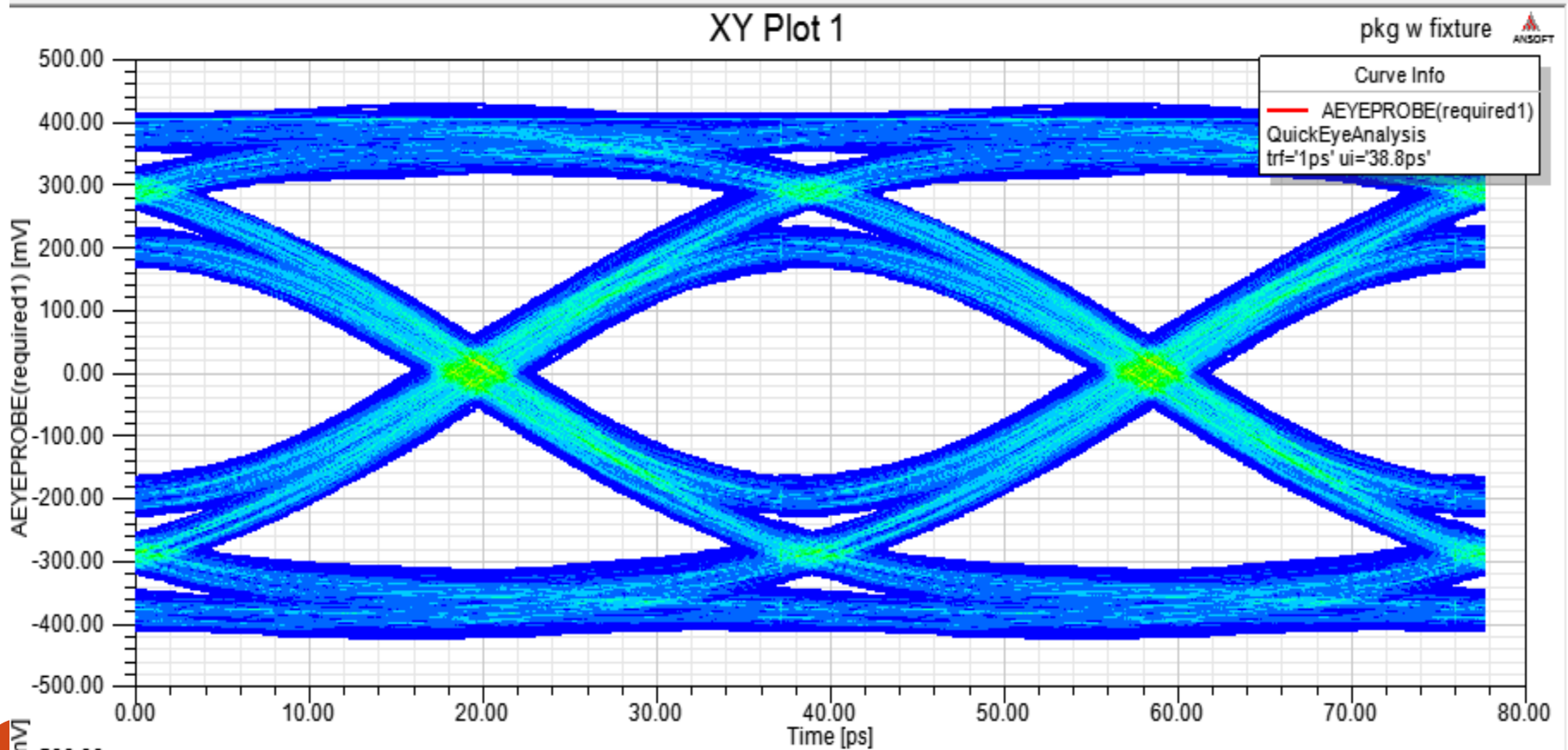
Combine parameters (replaces eq. 96a-5)

- $[S_{\text{pkgtx}}] = \text{combine}([\text{combine}([S_{\text{pad}}], ([S_{\text{tline}}])), [S_{\text{ball}}])$
 - Create $[T_{\text{pkgtx}}] \rightarrow [S_{\text{pkgtx}}]$
- $[S_{\text{pkgrx}}] = \text{combine}([S_{\text{ball}}, \text{combine}([S_{\text{tline}}], [S_{\text{pad}}])$
 - Create $[T_{\text{pkgrx}}]$
- Channel response:
 - $[T] = [T_{\text{pkgtx}}] * [T_{\text{channel}}] * [T_{\text{pkgrx}}] \rightarrow [S]$

- $$H_{21} = \frac{S_{21}(1-\Gamma_1)(1+\Gamma_2)}{1-S_{11}\Gamma_1-S_{22}\Gamma_2-S_{21}S_{12}\Gamma_1\Gamma_2+S_{11}\Gamma_1S_{22}\Gamma_2}$$

•

25Gbps NRZ eye diagram at tp0a suggests removing transmitter filter from COM is OK because the package and die load limits transition time



Parameters (Table 93A–2)

a_il_0	-4.453e-4 + 4.467e-05i
a_il_1	-1.049e-08 - 4.568e-08i
a_il_2	-6.409e-13-3.914e-11i
a_il_4	-1.669e-23 + 3.134e-23i
a_rl_0	-6.473 - 1.51i
a_rl_1	6.451e-05 + 3.351e-07i
a_rl_2	-2.712e-10 - 4.903e-11i
a_rl_4	2.167e-21 + 2.765e-22i
Cdiepad	250
Rdiepad	55
Cpkg_board	180
Pkg_len	12

- a_il_0, 1, 2 and 4 are insertion loss fit coefficients for $a_{il}(0, 1, 2, 4)$ on slide 5
- a_rl_0, 1, 2 and 4 are return loss fit coefficients for $a_{rl}(0, 1, 2, 4)$ on slide 5
- Cdiepad, Rdiepad, Cpkg_board, and Pkg_len are the package parameter on slide 4
- Remove parameter f_v , f_f and f_n and associated clauses.