

Time-Domain Channel Specification: Proposal for Backplane Channel Characteristic Sections

IEEE802.3bj

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Agenda

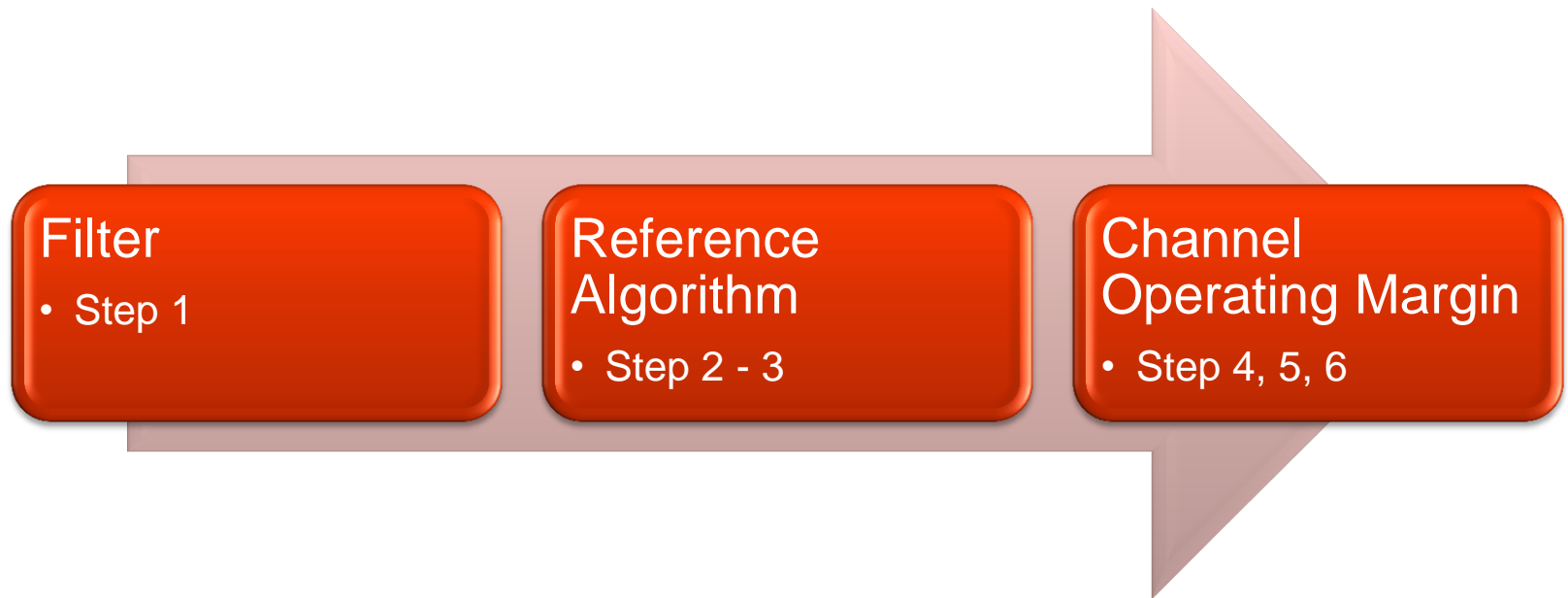
- Channel Specification Steps
- Flow Diagram
- Technical Description
- Tables
- Proposal

Channel Operating Margin (COM)

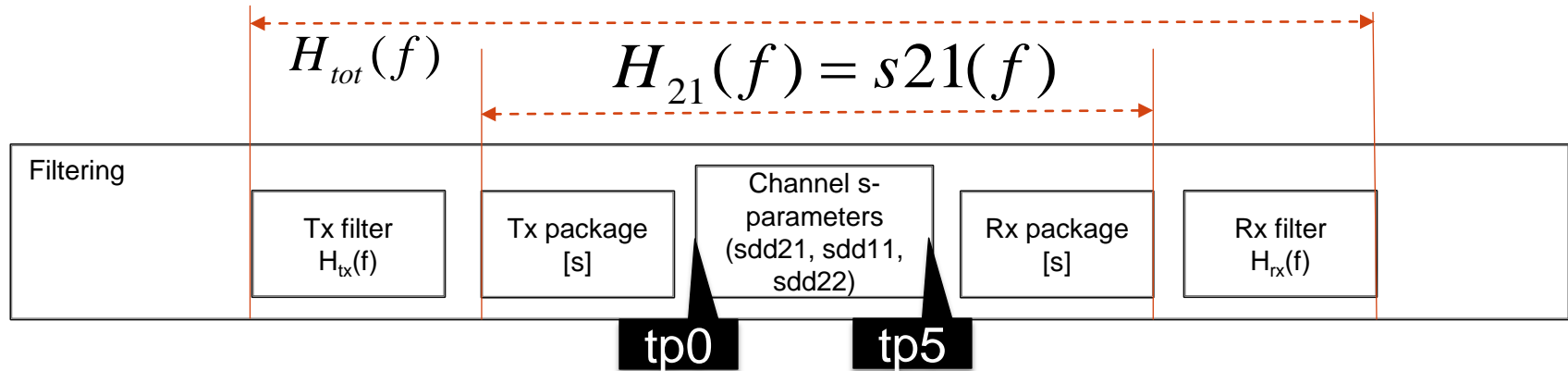
- The channel operating margin (COM) is a figure of merit for a channel utilizing reference transmitter/receiver performance characteristics. The reference transmitter/receiver block represents a minimum expected capability.
- This method shall be complemented by appropriate TX and RX compliance tests.
 - It is expected that compliant receivers will cope with ISI in the first 16 UI or so in some way and that COM may have computational differences between PAM4, NRZ/FEC, and NRZ.
- A channel with positive COM is expected to operate with a minimally compliant transmitter and receiver.
- COM effectiveness is presented in *adee_01_0712.pdf*

Top Level Flow:

Starting with channel s-parameters

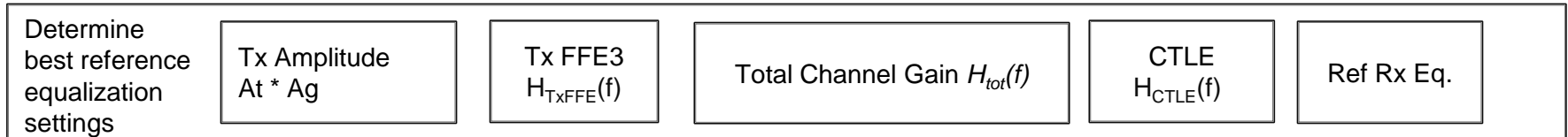


Process consisting of: Step 1



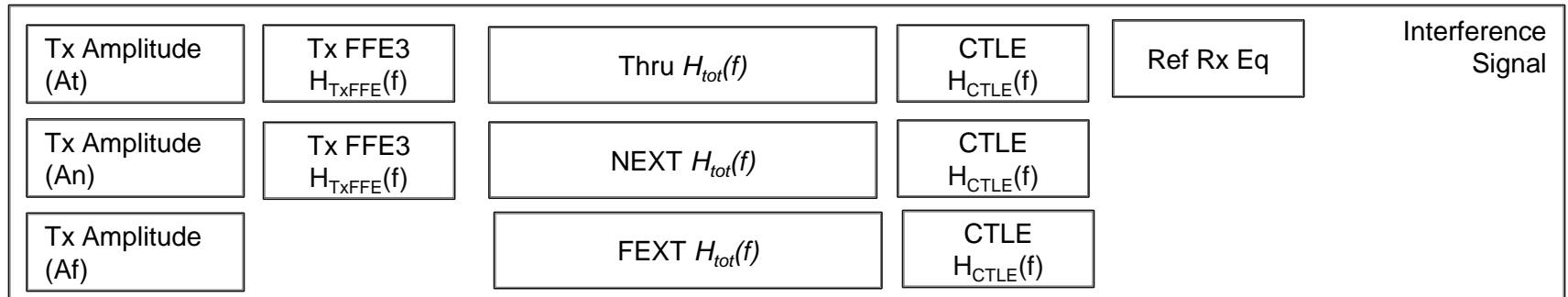
1. Computation of total channel gain $H_{tot}(f)$ from linear filters and channels s-parameters
 - Combine channel S-parameters (sdd21...) with reference Tx and Rx package S-parameters to get S-parameters of complete channel, $H_{21}(f)$.
 - Tx/Rx low pass filters

Process cont'd: Steps 2-3



2. Compute SBRs (single bit responses) from convolution of a
 - 1 UI wide source of appropriate amplitude
 - the 3 tap Tx FFE filter $H_{TxFFE}(f)$
 - the pole/zero CTLE filter $H_{CTLE}(f)$
 - and the through channel $H_{tot}(f)$
3. Compute available single amplitude(S_x), Tx FFE setting, and CTLE setting (NRZ/wo FEC example)
 - For each SBR of every Tx FFE and CTLE setting: (exhaustive search)
 - Determine the signal amplitude using a main cursor sample point 1 UI after the first positive zero crossing
 - Determine the RMS of the residual ISI (interference signal) after accounting for reference UI Gating
 - Combine the RMS with a fixed white noise source before the CTLE
 - Determine the Tx FFE taps setting and CTLE setting that produces the largest signal amplitude (S_x) to adjusted ISI RMS ratio.
 - The settings are used in following steps.
 - Also the main cursor sample point is also recorded for following steps.

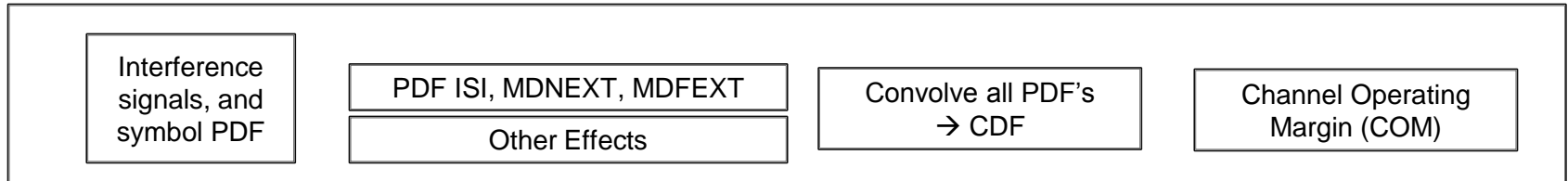
Process cont'd: Steps 4



4. Determine interference signals (without symbol gain)

- Create SBRs for Thru, NEXT, FEXT
 - For all channels, perform a linear transformation on H_{tot} (step 1) with $H_{CTLE}(f)$ CTLE setting found in step 3.
 - For Thru and FEXT, additionally perform a linear transformation with $H_{TxFFE}(f)$
- FEXT, and NEXT interference signals are the above SBRs
- The Thru interference signal is the Thru SBR accounting for “Ref Rx Equalizer”

Process cont'd: Steps 5 and 6



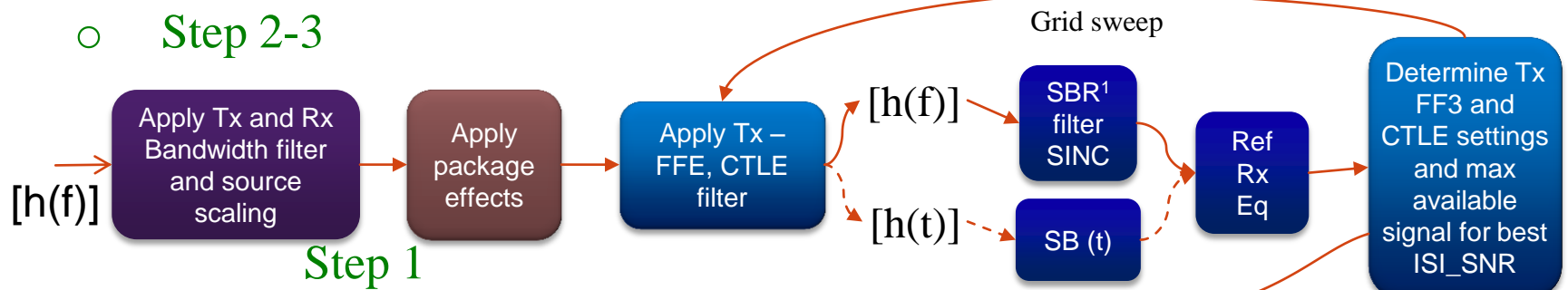
5. Compute interference PDFs for some number of sampling phases (32) and select the PDF for the worst variance and then compute a CDF.
 - PDFs for the Thru, all NEXT, and all FEXT channels are created using convolution with the PDF of a symbol for the port type and sampled interference signals.
 - Allowance for other effects are also joined with the joint PDF created from all channel PDFs
 - A CDF (cumulative distribution function) is computed using the cumulative sum of the joint PDF.
6. Computation of channel operating margin (COM) is dB ratio of the available signal amplitude (S_x) to the CDF voltage at the specified raw BER probability.

Twofold Flow

SBR¹ – single bit response aka pulse response
 PDF² – Probability Density Function
 CDF³ – Cumulative Distribution Function
 CTLE – Continuous Time Linear Equalizer

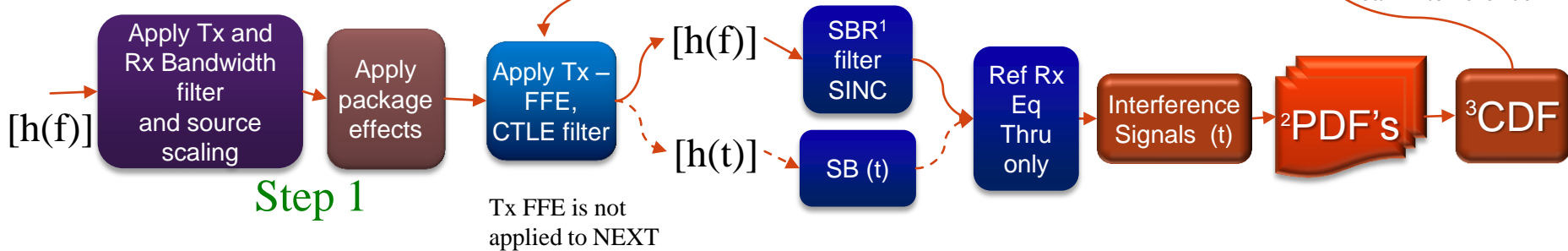
1. Determine Tx FFE and CTLE settings and available signal using Thru channel

○ Step 2-3



2. Determine peak interference for Thru, FEXT, NEXT channels

○ Steps 4-6



Total Channel Gain, H_{tot} w/o equalization (from step 1)

$$H_{tot}(f) = H_{tx}(f) * H_{21}(f) * H_{rx}(f)$$

Tx/Rx Filter

● Tx Filter

- $$H_{tx}(f) = \frac{1}{1 + \sqrt{2} \cdot \left(\frac{j \cdot f}{f_t}\right) + \left(\frac{j \cdot f}{f_t}\right)^2}$$

● Rx Filter

- $$H_{rx}(f) = \frac{1}{1 + bw1 \cdot \left(\frac{j \cdot f}{f_r}\right) + bw2 \cdot \left(\frac{j \cdot f}{f_r}\right)^2 + bw1 \cdot \left(\frac{j \cdot f}{f_r}\right)^3 + \left(\frac{j \cdot f}{f_r}\right)^4}$$

$bw1=2.613126, bw2=3.4142136$

Tx/Rx Package Modeling

return loss and channel s-parameters , H_{21}

$$\text{Tx, } \Gamma_1(f) = \frac{\Gamma_{01} - j\frac{f}{f_1}}{1 + j\frac{f}{f_1}}$$

$$\text{Rx, } \Gamma_2(f) = \frac{\Gamma_{02} - j\frac{f}{f_2}}{1 + j\frac{f}{f_2}}$$

TBD

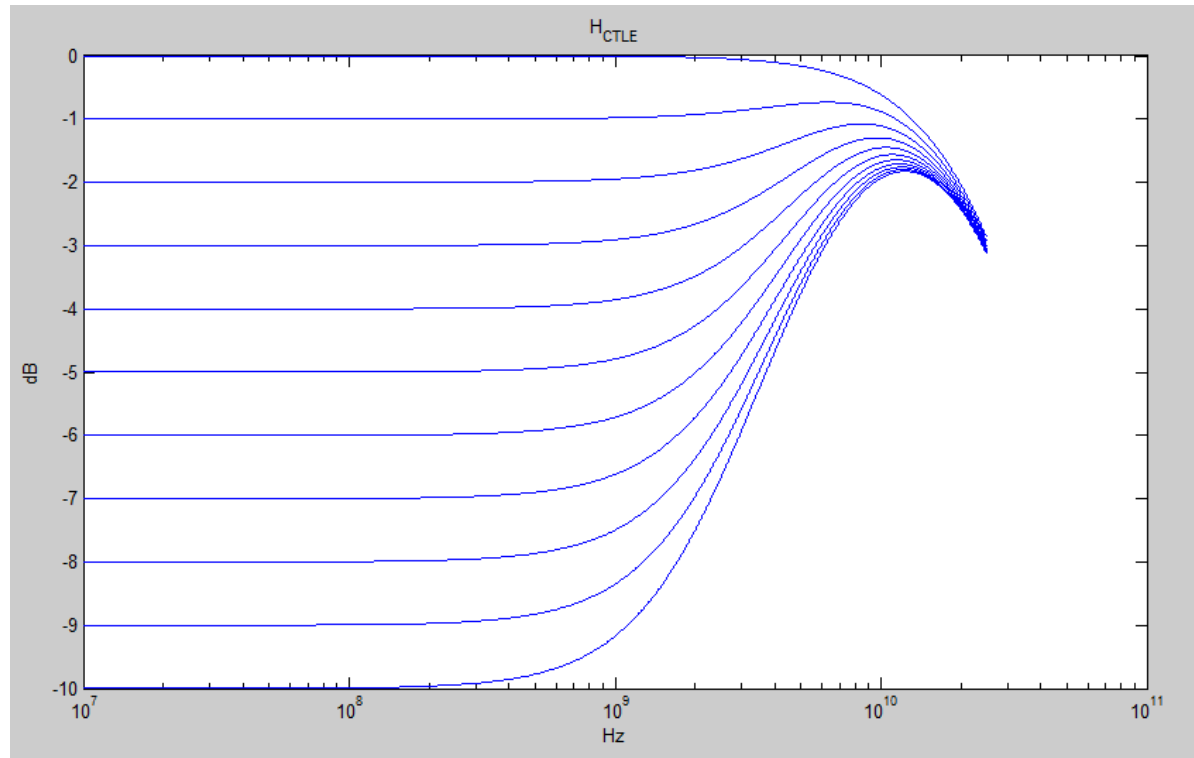
$$H_{21} = \frac{S_{21}}{1 - S_{11}\Gamma_{TX} - S_{22}\Gamma_{RX} - S_{21}S_{12}\Gamma_{TX}\Gamma_{RX} + S_{11}\Gamma_{TX}S_{22}\Gamma_{RX}}$$

H, S and, Γ are all function of f

CTLE

One degree of freedom: G_{DC}

$$H_{CTLE}(f) = f_b \frac{j \cdot f + 0.25 \cdot f_b 10^{\frac{G_{DC}}{20}}}{(j \cdot f + 0.25 \cdot f_b) \cdot (j \cdot f + f_b)}$$



G_{DC} is DC gain
in dB

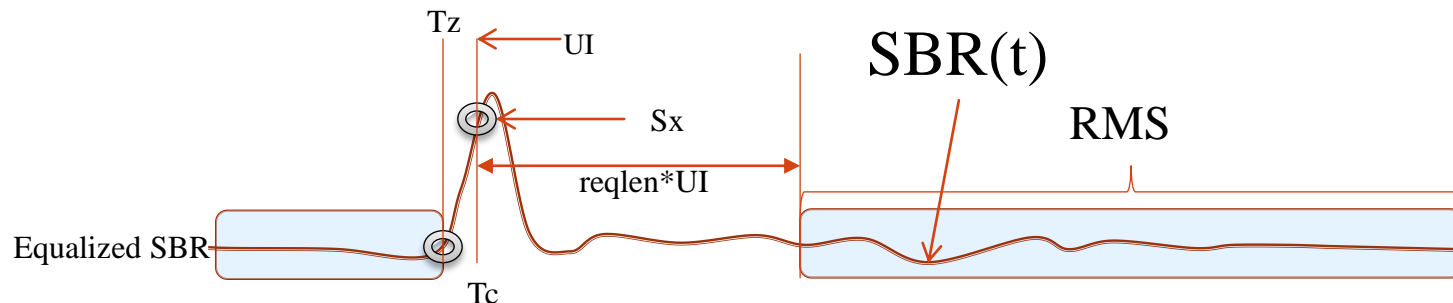
SBR(t) from $H_{tot}(f)$ example

(as in step 2ff)

- Peak Amplitude (per port type) for a 1 UI wide 100Ω differential ideal data source whose voltage swings between +/- peak amplitude
 - Amplitude, A , is assign per channel type
 - Thru channel and FEXT channels will have the same amplitude but NEXT will be larger
 - A_t , A_{ft} , and A_{nt}
 - Symbol gain scale is applied during PDF generation for NRZ and PAM4 and during the algorithm to determine S_x .
- Reference termination is 100Ω differential.
- Example:
 - $SBR(t) = \text{inverseDFT}(A \cdot H_{tot}(t) \cdot H_{CTLE}(f) \cdot (c(-1) \cdot e^{j \cdot 2 \cdot \pi \cdot f \cdot UI} + c(0) + c(1) \cdot e^{j \cdot 2 \cdot \pi \cdot f \cdot UI}))$
 - SBR extraction using convolution in the time domain is also acceptable.
- Inverse DFT must be applied prior to UI gating if a Thru channel. Time domain data is sampled OVERSAMPLING times per UI. Data should be available from 50MHz to 40GHz at 10MHz intervals:
 - LMS linear fit "unwrapped" phase and log amplitude from 10MHz to 100MHz. Modify phase fit by changing y intercept to give integer multiple of pi at DC and slope to give best LMS fit from 50MHz to 100MHz. Use these linear fits to extrapolate down to DC
 - May use other methods known by the implementer to give a better fit.
 - Zero pad data from 40GHz to $0.5 \cdot \text{OVERSAMPLING}/\text{UI}$

Finding available signal (S_x) and equalization settings from SBR(t) is an exhaustive search: NRZ /wo FEC example (as in step 3)

- For each CTLE G_{DC} gain setting, $c(-1)$ setting, and $c(1)$ setting
 - $c(0) = 1 - |c(-1)| - |c(1)|$
 - Determine SBR(t) as in previous slide
 - Determine first zero positive crossing, T_z (precursor sample point)
 - Main cursor $T_c = T_z + UI$
 - Determine voltage S_x one UI after first zero positive crossing ($T_z + UI$)
 - Determine RMS for region out side equalizers' reach, *residual_ISI*
 - $Noise = \sqrt{residual_ISI^2 + (G_{\sigma_noise} \cdot S_x)^2}$
 - Determine $ISI_SNR = 20 * \log_{10}(\frac{S_x}{Noise})$
 - If $ISI_SNR > best\ ISI_SNR$, $best\ ISI_SNR = ISI_SNR$, record, S_x , $c(-1)$, $c(1)$, G_{dc} and SBR(t), and main cursor sample point, $T_z + 1UI$



PDF generation

(as in step 5)

- Interference consists of residual ISI, several NEXT, and several FEXT signals.
 - Interference signal for ISI, aka Thru channel, is the Thru SBR after gating by “reqlen” Uis. (NRZ example)
 - Interference signal for XTALK is all of SBR for each NEXT or FEXT.
- Each interference signal is sampled at UI intervals into OVERSAMPLING vectors, representing sampling phases that are UI/OVERSAMPLING apart.
- For each interference pattern
 - Using the specified “binsize”, Convolve the PDF of a single cursor specified per port type with cursor values for all UI for each OVERSAMPLING vector
 - Select the PDF of the OVERSAMPLING vector that has maximum variance for each Thru, NEXT, and FEXT
- Convolve PDFs of all selected FEXT and NEXT together with the PDF for the ISI to create an interference PDF.

Allowances:

- Some sources considered
 - Jitter
 - Non-ideal performance of real circuits due to non-linearity, bandwidth limitations, etc.
 - Manufacturing tolerance of PHY
 - Manufacturing tolerance of channel
- Binary (Dual Dirac) noise = $\pm G_{dd_noise} * S_x$
- Gaussian Noise: $RMS = G_{\sigma_noise} * S_x$
- These allowances convolve with the interference PDF creating a total interference PDF.

COM Computation

- A CDF is created from the total interference PDF. A total peak interference is created when the CDF probability achieves the raw BER for the specified port type
 - $CDF(i) = \sum_{k=1}^i Total_PDF.y(k)$
 - The peak total interference, $Total_PDF.x(spec_i)$, is when the when $CDF(spec_i) = \text{“raw BER”}$
 - Where $Total_PDF.y$ are probabilities and $Total_PDF.x$ are respective voltage values in the bins of “binsize”.
- COM is the dB ratio of the available signal to total peak interference.
 - $COM = 20\log_{10}\left(\frac{S_x}{Total_PDF.x(spec_i)}\right)$

Table: Channel Electrical Characteristics

Parameters	Type	Description
COM	Figure of merit	Channel Operating Margin
ILfit at $f_b/2$	dB loss	Insertion loss fit at the Port Nyquist frequency
IL at $f_b/2$	dB loss	Insertion fit at the Port Nyquist frequency
Amax/IL	Mask/graph	Maximum Attenuation
RL	Mask/graph	Maximum Common Mode and Differential Return Loss
PTI	Interim Peak V	Peak ¹ Total Interference at raw BER including ISI, crosstalk, and system “allowance”
PJI	Interim Peak V	Peak ¹ joint ISI and crosstalk interference voltage at raw BER
PISI	Interim Peak V	Peak ¹ ISI interference voltage at raw BER
Sx	Interim V	Available signal amplitude
PMXI	Interim Peak V	Peak ¹ Multi-aggressor crosstalk interference voltage at raw BER
PMFEXTI	Interim Peak V	Peak ¹ Multi-aggressor FEXT interference voltage at raw BER
PMNEXTI	Interim Peak V	Peak ¹ Multi-aggressor NEXT interference voltage at raw BER

Table: Channel Parameters

Moore_01_0311

Parameter	Symbol	100GBASE-KP4	100GBASE-KR4	
Symbol rate, GH	fb	13.5938	25.7813	GHz
Victim differential output amplitude, mV peak	A_t	400	400	mV
Victim transmitter 3 dB bandwidth, GHz	f_t	0.55 x fb	0.55 x fb	GHz
Far-end disturber differential output amplitude, mV peak	A_{ft}	400	400	mV
Far-end disturber 3 dB bandwidth, GHz	f_{ft}	0.55 x fb	0.55 x fb	GHz
Near-end disturber differential output amplitude, mV peak	Ant	600	600	mV
Near-end disturber 3 dB bandwidth, GHz	f_{nt}	1.00 x fb	1.00 x fb	GHz
Receiver 3 dB bandwidth GH	f_r	0.75x fb	0.75x fb	GHz
Maximum frequency for transfer function fit, GHz	fmax	0.75 x fb	0.75 x fb	GHz
Symbol gain	Ag	1/3	1	
Interference Symbol Gain (X values of a PDF)	ISG	PDF.x = [-1 -1/3 1/3 1]	[-1 1]	-
Interference Symbol probability. (Y probabilities of a PDF)	ISP	PDF.y= [.25 .25 .25 .25]	[.5 .5]	-
Probability bin size for probability density	binsize	100	100	μ V
Oversampling	OVERSAMPLING	32	32	

Table: Channel Parameters

Parameters	symbol	100GBASE-KP4	100GBASE-KR4	
Transmitter DC reflection coefficient, V/V	Γ_{01}	.161	.161	
Transmitter return loss reference frequency, GHz	f_1	1.25*f _b TBD	1.25*f _b	Hz
Receiver DC reflection coefficient, V/V	Γ_{02}	.161	.161	
Receiver return loss reference frequency, GHz	f_2	1.25*f _b	1.25*f _b	Hz
Tx FFE3 pre cursor tap	c(-1)	[0.0, -.02, ... -0.1]	[0.0, -0.02, ... -0.1]	
TX FFE3, post cursor tap	c(1)	[0.0, -.02, ... -0.4]	[0.0, -0.02, ... -0.4]	
CTLE ac gain	Gdc	0, 1, ... 10	0, 1, ... 10	dB
Reference Rx equalizer length	reqlen	TBD	TBD	
Raw Probability Target	rawBER	1e-5	1e-5(FEC)/1e-12	
Reference equalizer Gaussian noise scale	G_{σ_noise}	0.01	0.01	
Reference equalizer Dual Dirac noise scale	G_{dd_noise}	0.1	0.1	

Proposal

Add sub clause after 93.9.2 and 94.4.2 entitled “Channel Operating Margin” based on this presentation.

Channel operating margin shall be normative for clause 93 and 94

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