

Proposed changes to 93A.1.2.3, 93A.4, and 92.10.7.1.1:

93A.1.2.3 Two-port network for the package transmission line

The scattering parameters for ~~a 1 mm section of~~ the package transmission line model are a function of the complex propagation coefficient defined by Equation (93A-9), Equation (93A-10), and Equation (93A-11) and the reflection coefficient defined by Equation (93A-12). ~~The values of~~ the parameters ~~values that appear in these equations are defined~~ in Table 93A-3. The units of f are GHz.

~~$$s_{11} = s_{22} = \rho_0 + \rho_1(1 - \exp(-j2\pi f\tau)) \quad (93A-9)$$~~

~~$$s_{12} = s_{21} = \exp(\gamma_0 + \gamma_1\sqrt{f} + \gamma_2 f + \gamma_4 f^2) \quad (93A-10)$$~~

Table 93A-3—Transmission line model parameters

Parameter	Real	Imaginary	Units
ρ_0	0.001	0	—
ρ_1	0.100	0	—
τ	1.22×10^{-2}	0	1/GHz
γ_0	-1.067×10^{-3}	0	—
γ_1	-3.551×10^{-4}	-3.357×10^{-3}	1/GHz ^{1/2}
γ_2	-1.027×10^{-3}	-3.818×10^{-2}	1/GHz
γ_4	-1.179×10^{-5}	3.36×10^{-5}	1/GHz ²

~~$$\gamma(f) = \begin{cases} \gamma_0 & f = 0 \\ \gamma_0 + \gamma_1\sqrt{f} + \gamma_2(f)f & f > 0 \end{cases} \quad (93A-9)$$~~

~~$$\gamma_1 = a_1(1 + j) \quad (93A-10)$$~~

~~$$\gamma_2(f) = a_2(1 - j(2/\pi)\log_e(f/1 \text{ GHz})) + j2\pi\tau \quad (93A-11)$$~~

~~$$\rho = \frac{Z_c - 2R_0}{Z_c + 2R_0} \quad (93A-12)$$~~

The scattering parameters for a package transmission line ~~whose of~~ length z_p ~~is an integer multiple of 1 mm~~ are ~~derived from the scattering parameters of the 1 mm section using Equation (93A-11) defined by Equation (93A-13) and Equation (93A-12) Equation (93A-14).~~

~~$$s_{11}^{(l)} = s_{22}^{(l)} = s_{11} \sum_{i=1}^{z_p} s_{21}^{2i-2} \quad (93A-11)$$~~

Table 93A-3—Transmission line model parameters and values

Parameter	Value	Units
γ_0	0	1/mm
a_1	1.734×10^{-3}	ns ^{1/2} /mm
a_2	1.455×10^{-4}	ns/mm
τ	6.141×10^{-3}	ns/mm
Z_c	78.2	Ω

$$s_{12}^{(l)} = s_{21}^{(l)} = s_{21}^{z_p} \quad (93A-12)$$

$$s_{11}^{(l)}(f) = s_{22}^{(l)}(f) = \frac{\rho(1 - \exp(-\gamma(f)2z_p))}{1 - \rho^2 \exp(-\gamma(f)2z_p)} \quad (93A-13)$$

$$s_{21}^{(l)}(f) = s_{12}^{(l)}(f) = \frac{(1 - \rho^2) \exp(-\gamma(f)z_p)}{1 - \rho^2 \exp(-\gamma(f)2z_p)} \quad (93A-14)$$

The transmission line scattering parameter matrix is then denoted as $S^{(l)}$.

~~NOTE—Equation (93A-9) and Equation (93A-10) are based on a fit to a detailed model of a transmission line with a characteristic impedance of approximately 81 Ω and represents an extent of expected manufacturing variation. The fit is valid over the frequency range 0 to 40 GHz.~~

93A.4 Insertion loss deviation

The insertion loss deviation $ILD(f)$ is the difference between the measured insertion loss $IL(f)$ and the fitted insertion loss $IL_{fitted}(f)$ (see 93A.3) as shown in Equation (93A-53).

$$ILD(f) = IL(f) - IL_{fitted}(f) \quad (93A-53)$$

~~The RMS insertion loss deviation ILD_{RMS} is a~~ figure of merit for a channel that is ~~calculated using based on $ILD(f)$ is given by~~ Equation (93A-54). In Equation (93A-54), f_n are the frequencies considered in the computation of the fitted insertion loss and $W(f_n)$ is the weight at each frequency as defined by Equation (93A-55).

$$ILD_{RMS} = \left[\sum_n W(f_n) 10^{ILD(f_n)/10} \right]^{1/2} \quad FOM_{ILD} = \left[\frac{1}{N} \sum_n W(f_n) ILD^2(f_n) \right]^{1/2} \quad (93A-54)$$

$$W(f_n) = \text{sinc}^2(f_n/f_b) \left[\frac{1}{1 + (f_n/f_t)^4} \right] \left[\frac{1}{1 + (f_n/f_r)^8} \right] \quad (93A-55)$$

The variable f_b is the signaling rate. The 3 dB transmit filter bandwidth f_t is inversely proportional to the 20% to 80% rise and fall ~~times-time~~ T_t . The constant of proportionality is 0.2365 (e.g., $T_t f_t = 0.2365$; with f_t in Hertz and T_t in seconds). The variable f_r is the 3 dB reference receiver bandwidth.

The values assigned to f_b , T_t , and f_r are defined by the Physical Layer specification that invokes this method.

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1 **92.10.7.1.1 TP0 to TP1 and TP4 to TP5 signal paths**

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3 The additional transmitter and receiver PCB signal paths are calculated using the method defined in
4 93A.1.2.3. ~~A 1 mm section~~ The scattering parameters for a PCB of the PCB is length z_p are defined by
5 ~~Equation (93A-10)~~ Equation (93A-13), Equation (93A-11) ~~Equation (93A-14)~~, and the parameters values
6 given in Table 92-12.

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8 For the channel signal path defined in 92.10.7.1 and calculated using Equation (92-33), the transmitter and
9 receiver PCB model are each ~~consist of 141 sections~~ $z_p = 151$ mm in length representing an insertion loss of
10 6.26 dB at 12.89 GHz and ~~is~~ are each denoted as $S^{(HOSP)}$.

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12 For the channel crosstalk paths defined in 92.10.7.2 and calculated using Equation (92-34) and
13 Equation (92-35), the receiver PCB model ~~consists of 141 sections representing an insertion loss of 6.26 dB~~
14 ~~at 12.89 GHz and is denoted as $S^{(HOSP)}$~~ and the $S^{(HOSP)}$. The transmitter PCB model ~~consists of 68 sections~~
15 ~~is $z_p = 72$ mm in length~~ representing an insertion loss of 3 dB at 12.89 GHz and is denoted as $S^{(HOTxSP)}$. The
16 transmitter PCB insertion loss for the crosstalk channel is less than that for the signal channel to allow for a
17 reasonable worst case crosstalk in the COM calculation.

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20 **Table 92-12—Transmission line model parameter values**

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Parameter	Value	Units
γ_0	0	1/mm
a_1	4.114×10^{-4}	ns ^{1/2} /mm
a_2	2.547×10^{-4}	ns/mm
τ	6.191×10^{-3}	ns/mm
Z_c	109.8	Ω

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35 ~~NOTE—The host transmission line model is based on a fit to a detailed model of a transmission line with a characteristic~~
36 ~~impedance of approximately 110 Ω and represents an extent of expected manufacturing variation. The fit is valid over~~
37 ~~the frequency range 0 to 40 GHz.~~

Table 92-12—Transmission line model parameters

Parameter	Real	Imaginary	Units
ρ_0	4×10^{-4}	0	—
ρ_1	4.5×10^{-2}	0	1/GHz
τ	1.21×10^{-2}	0	1/GHz
γ_0	-1.89×10^{-4}	0	—
γ_1	-1.93×10^{-4}	-9.75×10^{-4}	1/GHz ^{1/2}
γ_2	-2.96×10^{-4}	-3.79×10^{-2}	1/GHz
γ_4	-2.47×10^{-6}	8.89×10^{-6}	1/GHz ²

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1 *Proposed changes to 93A.1.2.3 and 92.10.7.1.1 with mark-ups removed:*
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3 **93A.1.2.3 Two-port network for the package transmission line**
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5 The scattering parameters for the package transmission line model are a function of the complex propagation
 6 coefficient defined by Equation (93A-9), Equation (93A-10), and Equation (93A-11) and the reflection
 7 coefficient defined by Equation (93A-12). The values of the parameters that appear in these equations are
 8 defined in Table 93A-3. The units of f are GHz.
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$$\gamma(f) = \begin{cases} \gamma_0 & f = 0 \\ \gamma_0 + \gamma_1\sqrt{f} + \gamma_2(f)f & f > 0 \end{cases} \quad (93A-9)$$

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$$\gamma_1 = a_1(1 + j) \quad (93A-10)$$

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$$\gamma_2(f) = a_2(1 - j(2/\pi)\log_e(f/1 \text{ GHz})) + j2\pi\tau \quad (93A-11)$$

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$$\rho = \frac{Z_c - 2R_0}{Z_c + 2R_0} \quad (93A-12)$$

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 24 **Table 93A-3—Transmission line model parameters and values**
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Z_c	78.2	Ω

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 39 The scattering parameters for a package transmission line of length z_p are defined by Equation (93A-13) and
 40 Equation (93A-14).
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$$s_{11}^{(l)}(f) = s_{22}^{(l)}(f) = \frac{\rho(1 - \exp(-\gamma(f)2z_p))}{1 - \rho^2 \exp(-\gamma(f)2z_p)} \quad (93A-13)$$

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$$s_{21}^{(l)}(f) = s_{12}^{(l)}(f) = \frac{(1 - \rho^2)\exp(-\gamma(f)z_p)}{1 - \rho^2 \exp(-\gamma(f)2z_p)} \quad (93A-14)$$

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50 The transmission line scattering parameter matrix is then denoted as $S^{(l)}$.
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92.10.7.1.1 TP0 to TP1 and TP4 to TP5 signal paths

The additional transmitter and receiver PCB signal paths are calculated using the method defined in 93A.1.2.3. The scattering parameters for a PCB of length z_p are defined by Equation (93A-13), Equation (93A-14), and the parameter values given in Table 92-12.

For the channel signal path defined in 92.10.7.1 and calculated using Equation (92-33), the transmitter and receiver PCB model are each $z_p = 151$ mm in length representing an insertion loss of 6.26 dB at 12.89 GHz and are each denoted as $S^{(HOSP)}$.

For the channel crosstalk paths defined in 92.10.7.2 and calculated using Equation (92-34) and Equation (92-35), the receiver PCB model is $S^{(HOSP)}$. The transmitter PCB model is $z_p = 72$ mm in length representing an insertion loss of 3 dB at 12.89 GHz and is denoted as $S^{(HOTxSP)}$. The transmitter PCB insertion loss for the crosstalk channel is less than that for the signal channel to allow for a reasonable worst case crosstalk in the COM calculation.

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