

# **Analytical Model for 100 Gb/s Discrete Multi-Tone Modulation**

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40Gb/s and 100Gb/s Fiber Optic Task Force  
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# Outline

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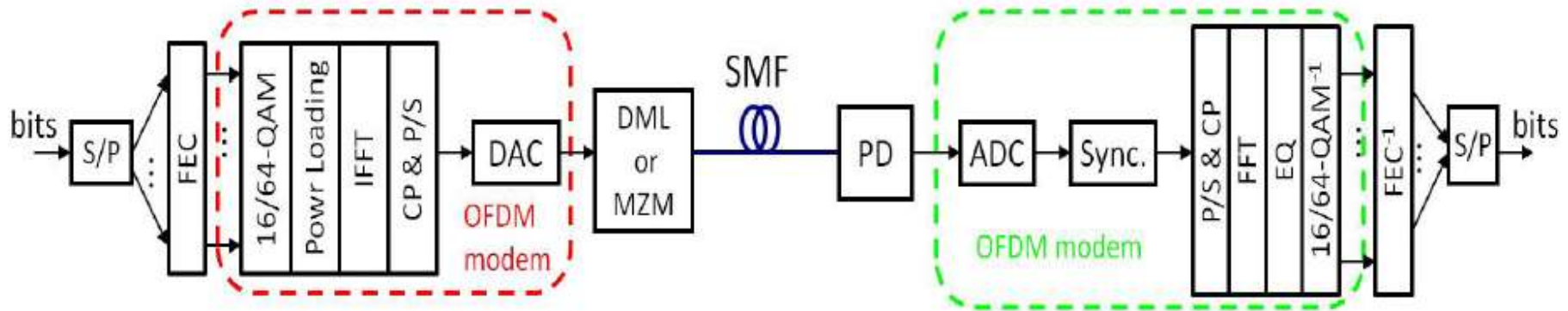
- Objectives
- DMT Analytical Model
- Impact of Thermal and Shot Noise
- Impact of Clipping Nonlinearity
- Impact of RIN
- Comparison of 100Gb/s DMT with PAM-M
- Conclusion

# Objectives

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- Continue higher order modulation analysis development in [nicholl\\_01b\\_0312](#), [ghiasi\\_01a\\_0912](#), and [lyubomirsky\\_01a\\_1112\\_optx](#)
- Gain physical insights from analytical models
- Compare performance of 802.3bm SMF PMD alternatives

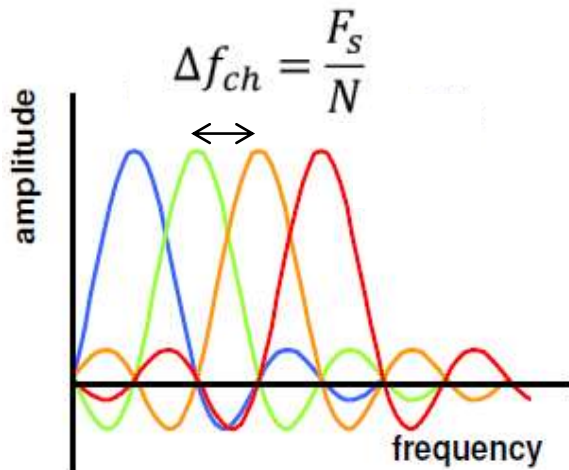
# 100 Gb/s DMT System Architecture



**FEC:** forward error correction   **P/S:** parallel to serial conversion   **CP:** cyclic prefix   **Sync.:** Synchronization   **PD:** photo-detector  
**(I)FFT:** (inverse) fast Fourier transform   **DAC/ADC:** digital to analog/analog to digital conversion

Source: J. Wei, et. al., "Performance Studies of 100 Gigabit Ethernet Enabled by Advanced Modulation Formats," IEEE 802.3, Next Gen. 40Gb/s and 100Gb/s Opt. Ethernet Study Group, ingham\_01\_0512\_optx, May, 2012

# DMT Effective SNR Model



$$SNR_{eff} = \frac{P_{ch}}{N_0 \Delta f_{ch}} = \frac{N_{sc} P_{ch}}{N_0 N_{sc} \Delta f_{ch}} = \frac{P_{sig}}{N_0 \Delta f}$$

$P_{sig} = N_{sc} P_{ch}$  = total DMT signal power at Rx

$N_0$  = one-sided noise power spectral density

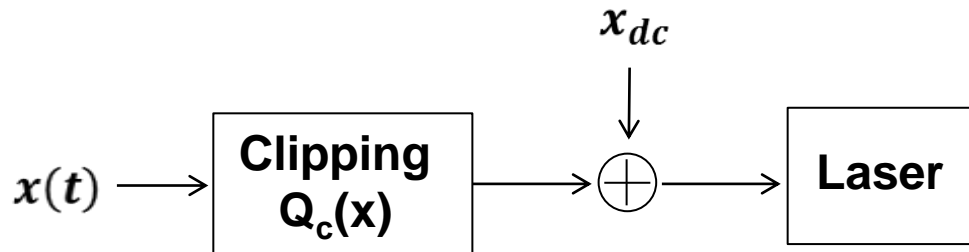
$\Delta f = \frac{N_{sc}}{N} F_s$  = effective noise bandwidth

$N$  = FFT size

$N_{sc}$  = number nonzero DMT subcarriers  $< N/2$

$F_s$  = DAC sampling rate

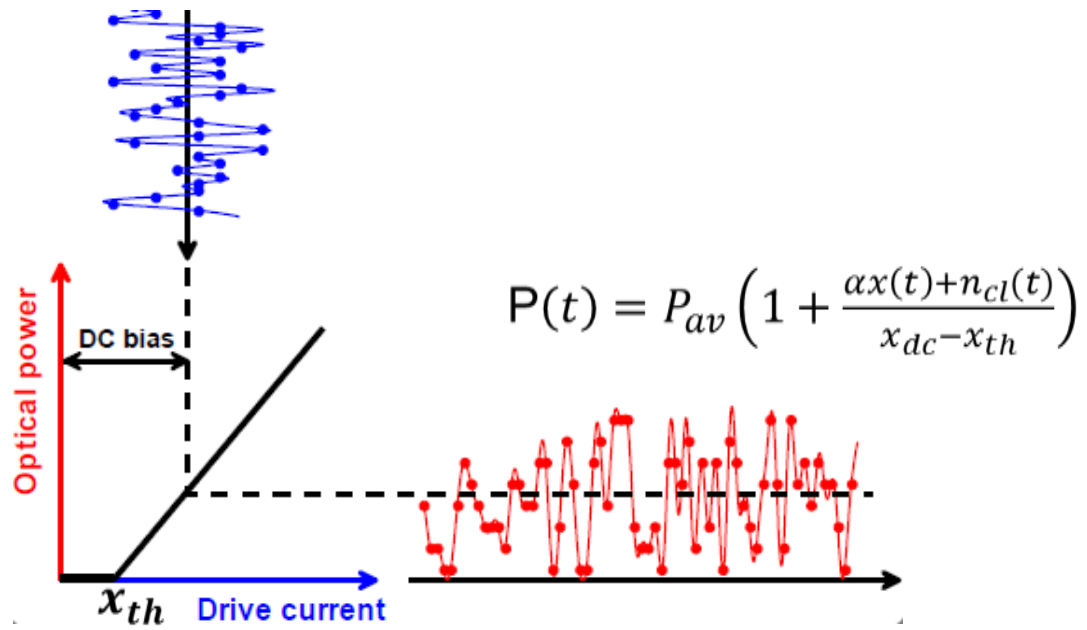
# DMT Effective SNR Model (continued)



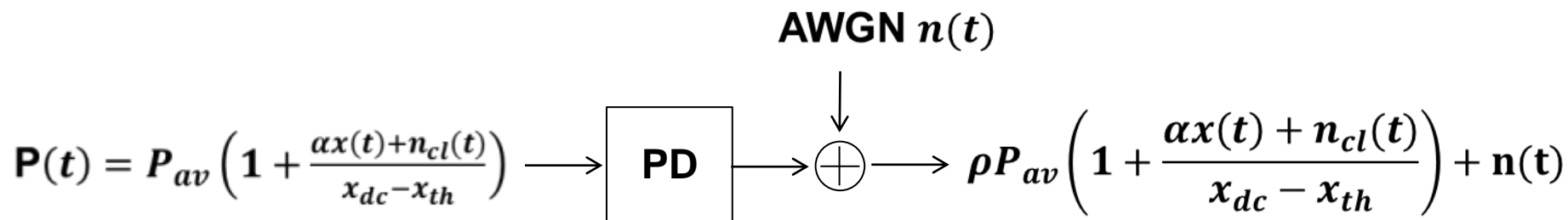
$$Q_c(x) = \begin{cases} x, & \text{if } |x| < x_0 \\ x_0 \cdot \text{sign}(x), & \text{if } |x| \geq x_0 \end{cases}$$

$$\text{Clipping Ratio} = R_{cl} = \frac{x_0^2}{\langle x^2 \rangle}$$

$$x_{drive}(t) = \alpha x(t) + n_{cl}(t) + x_{dc}$$



# DMT Effective SNR Model (continued)



$$P_{sig} = \left( \frac{\rho P_{av}}{x_{dc} - x_{th}} \right)^2 \alpha^2 \langle x^2 \rangle = (\rho P_{av})^2 \left( \frac{x_0}{x_{dc} - x_{th}} \right)^2 \frac{\alpha^2}{R_{cl}}$$

$$SNR_{eff} = \frac{P_{sig}}{P_{th} + P_{sh} + P_{rin} + P_{clip}}$$

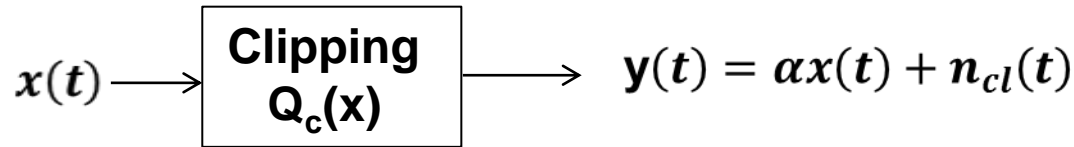
$$P_{th} = S_{th}^2 \Delta f = \text{Thermal Noise}$$

$$P_{sh} = 2q\rho P_{av} \Delta f = \text{Shot Noise}$$

$$P_{rin} = 10^{RIN/10} (\rho P_{av})^2 \Delta f = \text{RIN Noise}$$

$$P_{clip} = \text{Clipping Noise (see next slide)}$$

# DMT Effective SNR Model (continued)



$$Q_c(x) = \begin{cases} x, & \text{if } |x| < x_0 \\ x_0 \cdot \text{sign}(x), & \text{if } |x| \geq x_0 \end{cases}$$

$$R_{cl} = \frac{x_0^2}{\langle x^2 \rangle}$$

$$\langle x^2 \rangle = \sigma_x^2$$

Bussgang Theorem: Clipping noise  $n_{cl}(t)$  uncorrelated with  $x(t)$

$$\alpha = \frac{\langle x \cdot y \rangle}{\langle x^2 \rangle} = \frac{1}{\sqrt{2\pi}\sigma_x^3} \int_{-\infty}^{+\infty} x \cdot Q(x) \cdot \exp\left\{-\frac{x^2}{2\sigma_x^2}\right\} dx = 1 - \text{erfc}\left(\sqrt{R_{cl}/2}\right)$$

$$\langle y^2 \rangle = \frac{1}{\sqrt{2\pi}\sigma_x} \int_{-\infty}^{+\infty} Q^2(x) \cdot \exp\left\{-\frac{x^2}{2\sigma_x^2}\right\} dx$$

$$\langle y^2 \rangle = \sigma_x^2 \left(1 - \text{erfc}\left(\sqrt{R_{cl}/2}\right) + R_{cl} \text{erfc}\left(\sqrt{R_{cl}/2}\right) - \sqrt{2R_{cl}/\pi} \exp\{-R_{cl}/2\}\right)$$

$$P_{clip} = \left(\frac{\rho P_{av}}{x_{dc} - x_{th}}\right)^2 (\langle y^2 \rangle - \alpha^2 \sigma_x^2)$$

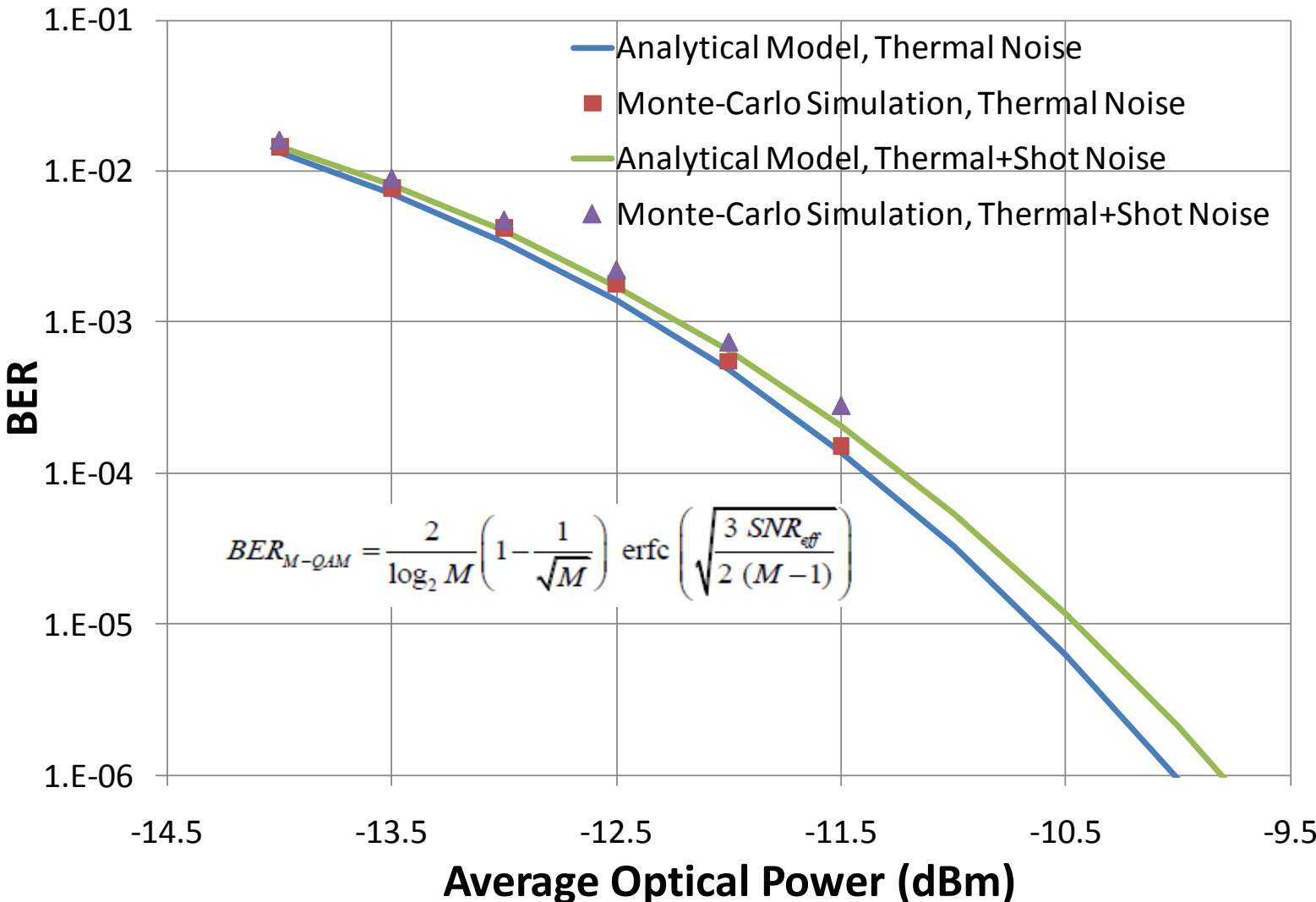
Closed form formulas derived in E. Vanin, "Performance evaluation of intensity modulated optical OFDM system with digital baseband distortion," Opt. Exp., Vol. 19, No. 5, pp. 4280-4293, 2011



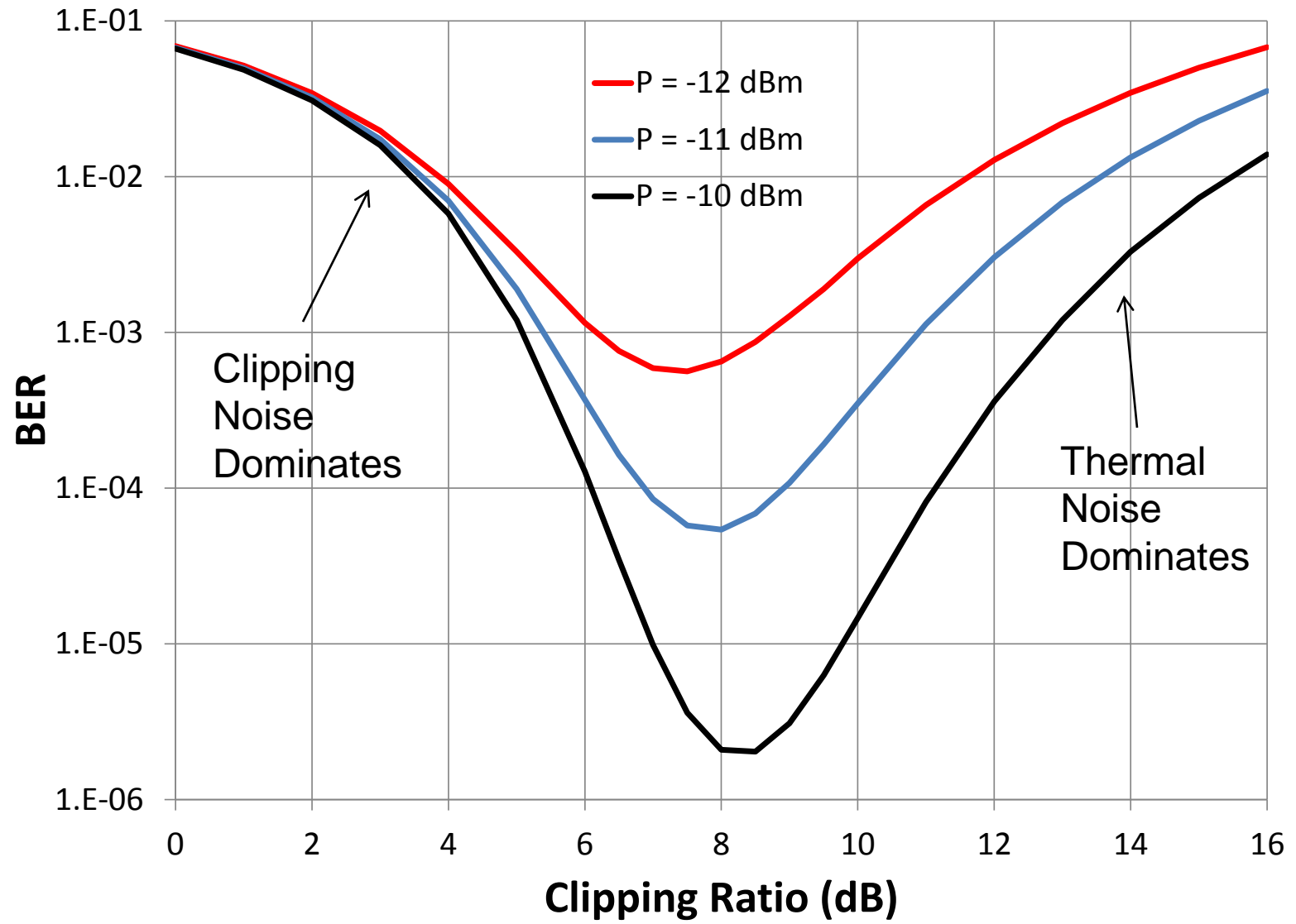
# Monte-Carlo Simulation Parameters

Parameter	Value
Sampling rate, $F_s$	60 Gs/s
FFT size, N	128
Number of nonzero subcarriers, $N_{sc}$	55
High freq. subcarriers padded to zero	8
DC subcarriers padded to zero	1
Cyclic prefix, CP	4
Clipping ratio, $R_{cl}$	8 dB
QAM modulation order, M	16
Noise bandwidth, $\Delta f$	25.8 GHz
Thermal noise density, $S_{th}$	16 pA/sqrt(Hz)
Photodiode responsivity, $\rho$	0.8 A/W

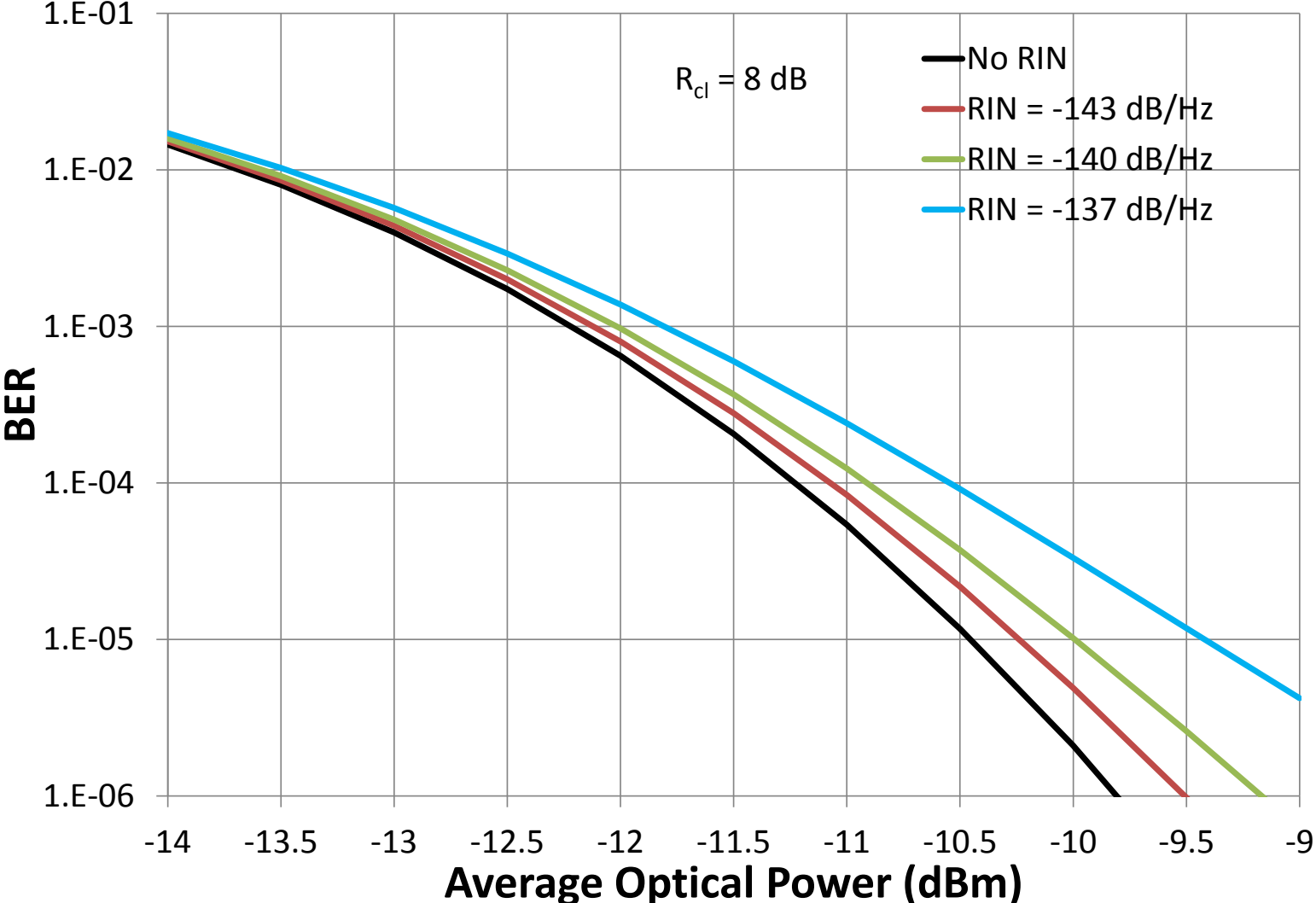
# 100 Gb/s DMT Analytical Model Results



# Optimization of Clipping Ratio



# Impact of RIN



# Analytical Model for PAM-M

For optimum receiver thresholds, the symbol error probability is determined by an average over all the PAM eye Q-factors

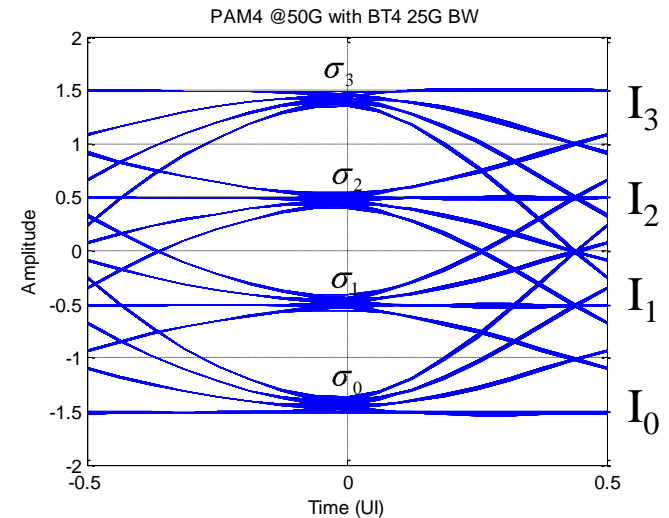
$$Q(k) = \frac{I_{k+1} - I_k}{\sigma_{k+1} + \sigma_k}, \quad k = 0, \dots, M-2$$

$$I_{k+1} - I_k = \frac{2RP_{av}}{M-1} \frac{ER-1}{ER+1}$$

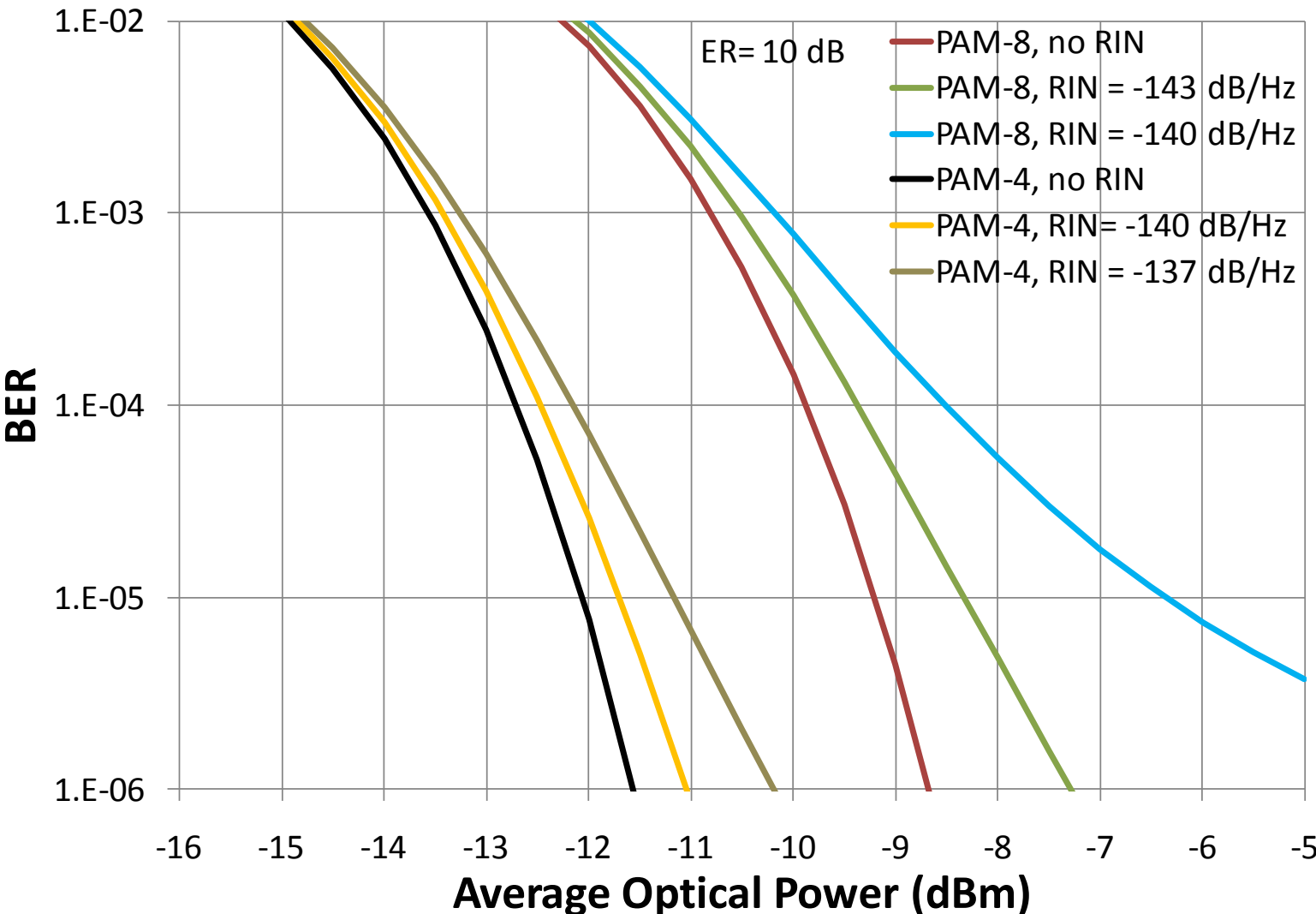
$$\sigma_k^2 = (S_{th}^2 + 2qI_k + 10^{\frac{RIN}{10}} I_k^2) \Delta f$$

$$P(k) = \text{erfc}\left(\frac{Q(k)}{\sqrt{2}}\right)$$

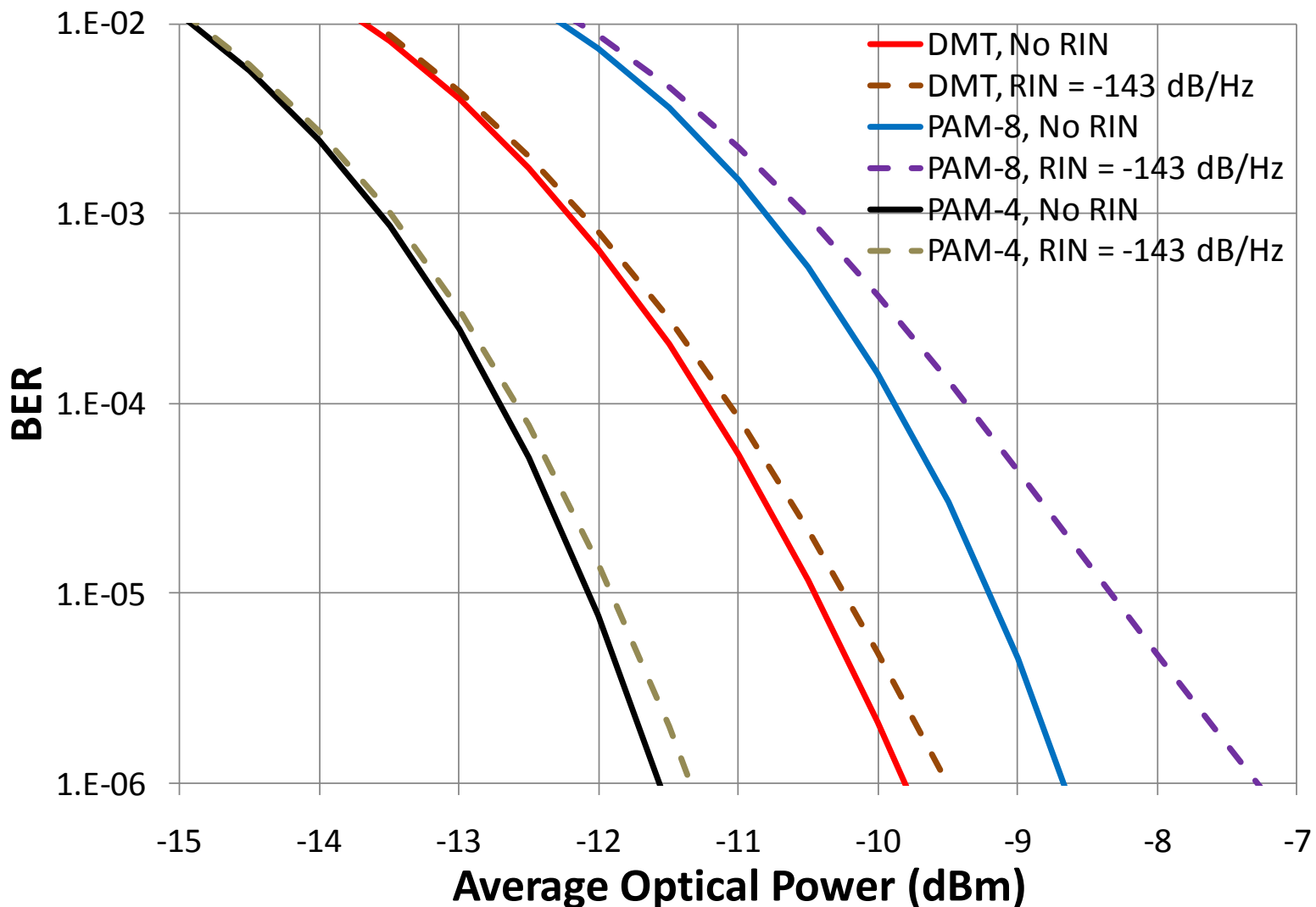
$$P_s = \frac{1}{M} \sum_{k=0}^{M-2} P(k)$$



# 100 Gb/s PAM-M Analytical Model Results



# 100 Gb/s DMT versus PAM-4 and PAM-8



# Conclusions

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- We presented an analytical model for DMT modulation based on an effective SNR approach
- The model provides a useful baseline for performance, as well as physical insight on the interplay of DMT system parameters