## 1. Update table 33-11 item 7 as follows:

| Item | Parameter | Symbol | Unit | Min | Max | PSE <br> Type | Additional Information |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7 | Overload current per pair set, detection range | I CUT-2P | A | Pclass/Vport_PSE-2P | $\mathrm{I}_{\text {LIM }}$ | 1,2 | Optional LIMIT; See 33.2.7.6, Table 33-7. K_icut3Kicut=: 0.596 for class 5 . 0.5560 .557 for class 6 . 0.539 for class 7. K_icut4 $=0.5380 .535$ for class 8 . |
|  |  |  |  | Kicut3 Kicut X <br> Pclass/Vport_PSE-2P |  | 3,4 |  |
|  |  |  |  | Kicut4X <br> Pelass/Vport_PSE 2P |  | 4 |  |

## End of Baseline Text

## Notes:

The value for class 6 was updated from D1.1 due to round down error.
The value for class 8 was updated from D1.1 due to the changes made for Type 4 power from 71.3 W to 71 W .
The values for Class 5 and 7 are new. See Annex A and B for details.

## Annex A: Derivation of Icut-2P

1. Icut_min- $2 \mathrm{P}=$ Icont- 2 P _unb by definition.
2. Worst case $\mathrm{P} 2 \mathrm{P}_{-}$Iunb conditions in Type 3 is at short cable ( $0.1 \Omega$ ) and in Type 4 is at long cable ( $12.5 \Omega$ ) therefore the ratio
Optimized_E2EP2P_Iunb_effect $=\frac{\text { Icont }-2 P_{-} \text {unb_max }}{\text { Icont }-2 \mathrm{P}_{-} \max }$ Can be used to set Pclass/Vport_PSE-2P at
E2EP2P_Iunb conditions, therefore:
Icont-2P_max $=0.5^{*}$ (Pclass/Vport_PSE_min)
Icont-2P_unb_max=Simulation results, the pair with maximum current from Rch=0.1 $\Omega$ to $12.5 \Omega$

## For Type 3 class 5:

Icut_min-2P = Icont-2P_unb= (Icont-2P_unb_max/Icont-2P_max)*0.5*Pclass/Vport_PSE-2P= $=(0.536 / 0.45))^{*} 0.5 *$ Pclass $/$ Vport_PSE-2P $=0.596 *$ Pclass $/$ Vport_PSE-2P.
For Type 3 class 6:
Icut_min- $2 \mathrm{P}=$ Icont-2P_unb $=(\text { Icont-2P_unb_max/Icont-2P_max })^{*} 0.5 *$ Pclass/Vport_PSE-2P $=$ $=(0.668 / 0.6) * 0.5 *$ Pclass $/$ Vport_PSE-2P $=\mathbf{0 . 5 5 6 0 . 5 5 7} *$ Pclass/Vport_PSE-2P.

## For Type 4 class 7:

Icut_min- $2 \mathrm{P}=$ Icont-2P_unb $=($ Icont-2P_unb_max/Icont-2P_max $) * 0.5 *$ Pclass/Vport_PSE-2P $=$ $=(0.778 / 0.721) * 0.5 *$ Pclass $/$ Vport_PSE- $2 \mathrm{P}=\mathbf{0 . 5 3 9} *$ Pclass/Vport_PSE-2P.
For Type 4 class 8:
Icont-2P_unb $=(0.9310 .926 / 0.865) * 0.5 *$ Pclass/Vport_PSE-2P $=\mathbf{0 . 5 3 8 0 . 5 3 5 * P c l a s s / V p o r t \_ P S E - 2 P ~}$ Notes:

1. All Kicut values are worst case ratio and not depend on Vport_PSE-2P. Generating Kicut as function of Vport_PSE-2P to reduce unnecessary margins in Icut_min is possible but not necessary and adds complexity.
2. As long as total system Vdiff stays 60 mV and we require the same Icon-2P_unb per class to be met with extended power mode, the Kicut ratio per class will remain the same for extended power

## Annex B: Why changing D1.1 from Kicut3 and Kicut4 to Kicut per class.

The reason was to fix accuracy problems that were resulted with differences between Icut_min to Icont-2P_unb that must be the same value. The differences were occurred due to the usage of a constant that was calculated for Type 3 class 6 , to calculate Icut_2P min for class 5 which is incorrect. The same was for the constant that was calculated for Type 4 class 8 and was used to calculate Class 7 Icut-2P.

| $\#$ | Parameter | Class 5 | Class 6 | Class 7 | Class 8 |
| :---: | :--- | :---: | :---: | :---: | :---: |
| 1 | Icont-2P_unb | 0.536 | 0.668 | 0.778 | 0.926 |
| 2 | K_icut3 and K_icut4 | 0.557 | 0.557 | 0.535 | 0.535 |
| 3 | Icut_min per the current constants K_icut3 and K_icut4 in <br> D1.2 [A] | 0.501 | 0.668 | 0.772 | 0.926 |
| 4 | There is an error due to using constants of Type power for all <br> classes instead of per class [A] | -0.035 | 0.000 | -0.006 | 0.000 |
| 5 | Changing to constants per class | 0.596 | 0.557 | 0.539 | 0.535 |
| 6 | New Icut_min=Kicut*Pclas/Vport_min [A] | 0.536 | 0.668 | 0.778 | 0.925 |

We can see now that Icut_min=Icont-2P_unb as required (lines 1 and 6).

