



# Relative Intensity Noise measurements

IEEE802.3bv Gigabit Ethernet over POF Task Force  
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Volker Goetzfried

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# Purpose

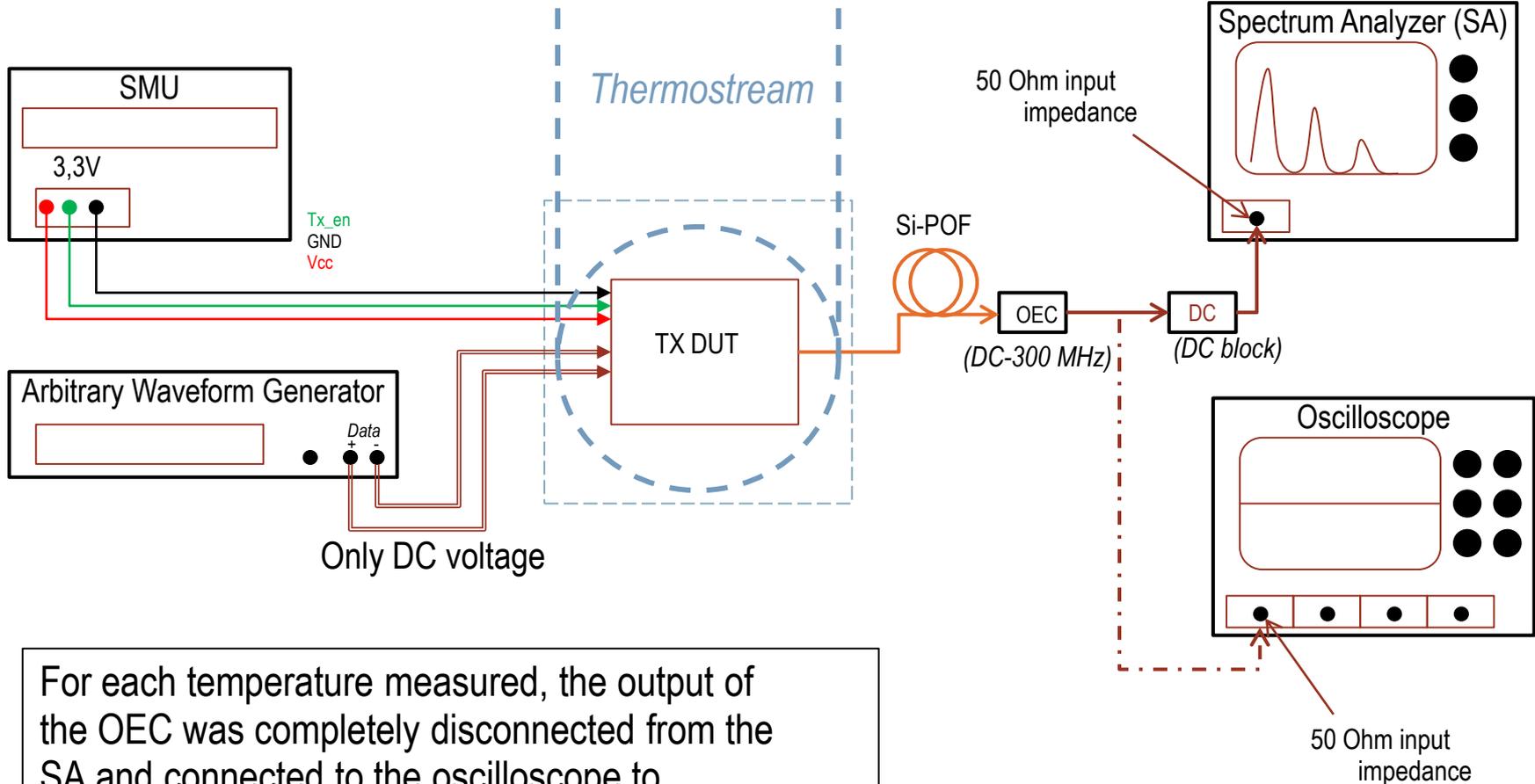
- Present the 802.3bv TF members a measurement methodology and results of relative intensity noise for a PMD transmitter

## Measurement conditions

- Temperature: -40 to 85 deg
- Sweeping frequency from 10 – 170 MHz
- The used optical-to-electrical converter (OEC) was a Femto DC...300MHz



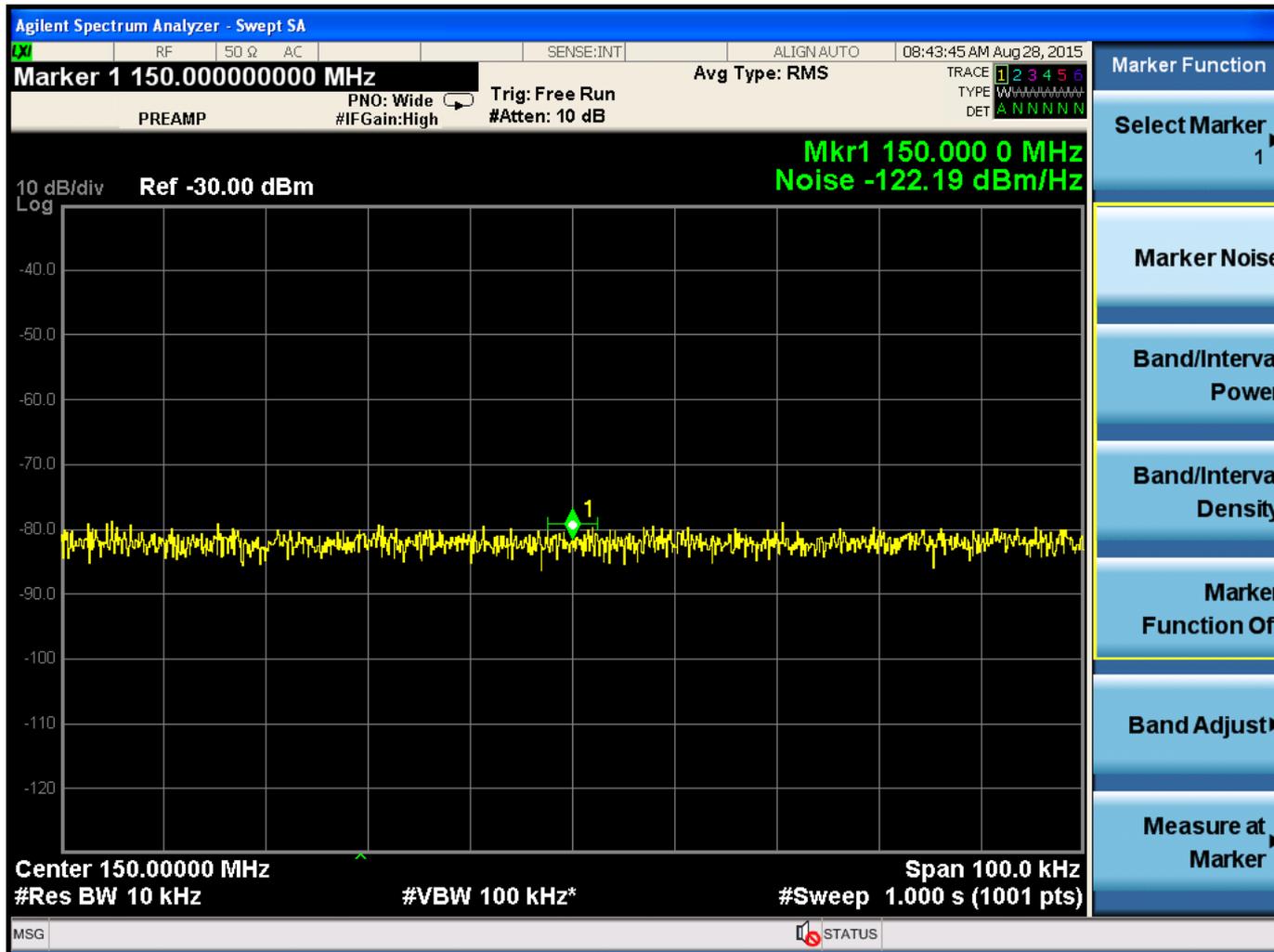
# Setup



For each temperature measured, the output of the OEC was completely disconnected from the SA and connected to the oscilloscope to measure the DC output voltage



# Spectrum Analyzer settings

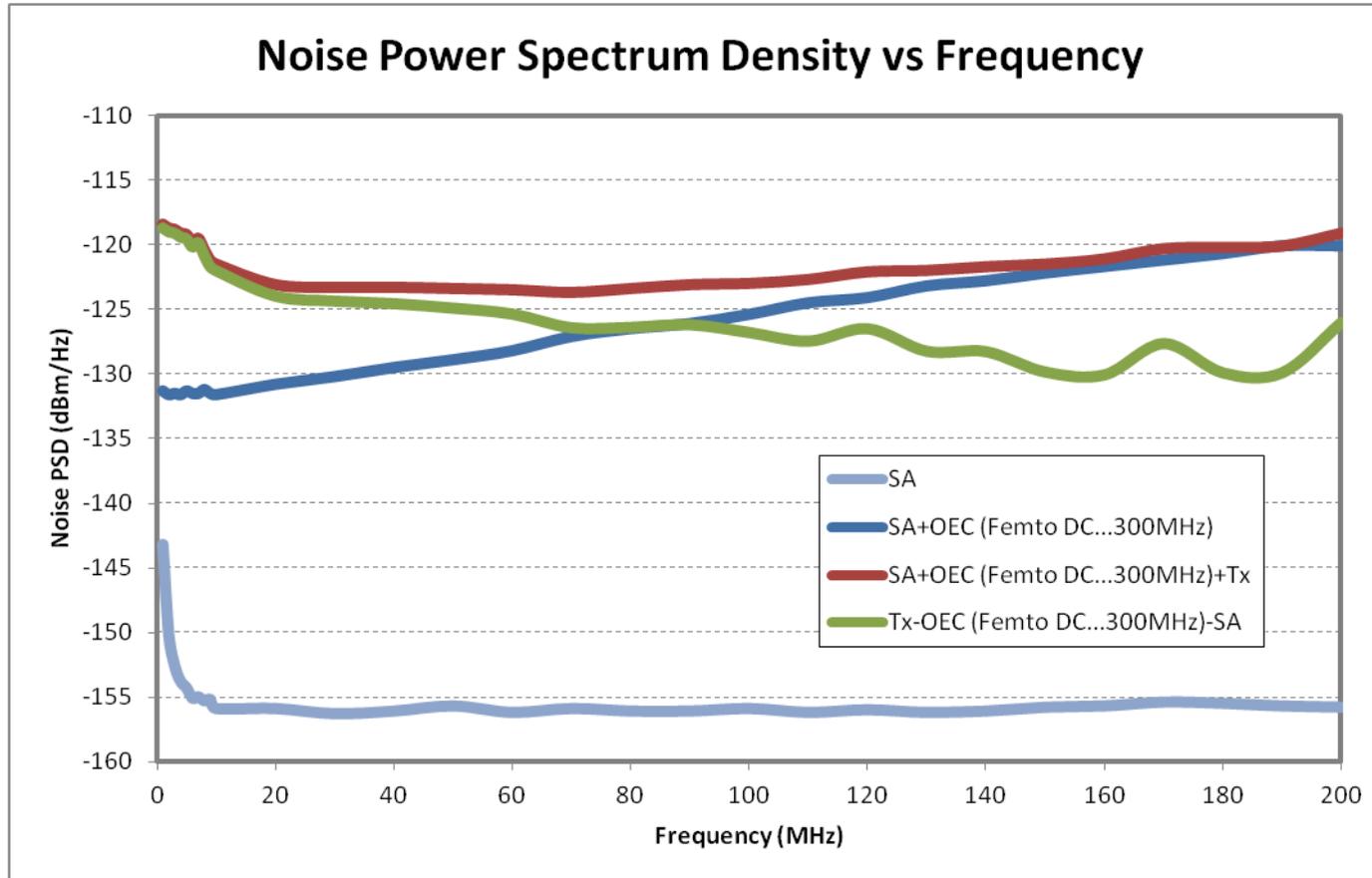


## SA settings at a glance:

- Internal pre-amplifier enabled (noise level ~10 dB improved)
- ADC Dither function off (decreased linearity but also improved noise floor)
- High Swept IF Gain and FFT IF Gain for best noise level
- Low Resolution BW (10kHz) and low Video BW (100kHz)
- Long sweep time (1 second)
- Enabled noise marker



# Measurement procedure



To get the noise PSD of a transmitter sample (green chart), the noise spectra of SA and OEC (blue chart) need to be subtracted from the acquired measurement data (red chart)



# Relative Intensity Noise calculation

$$\text{RIN} = 10 \log_{10} \frac{P_N}{BW \times I_{oe}^2 \times R} - G \text{ (dB/Hz)}$$

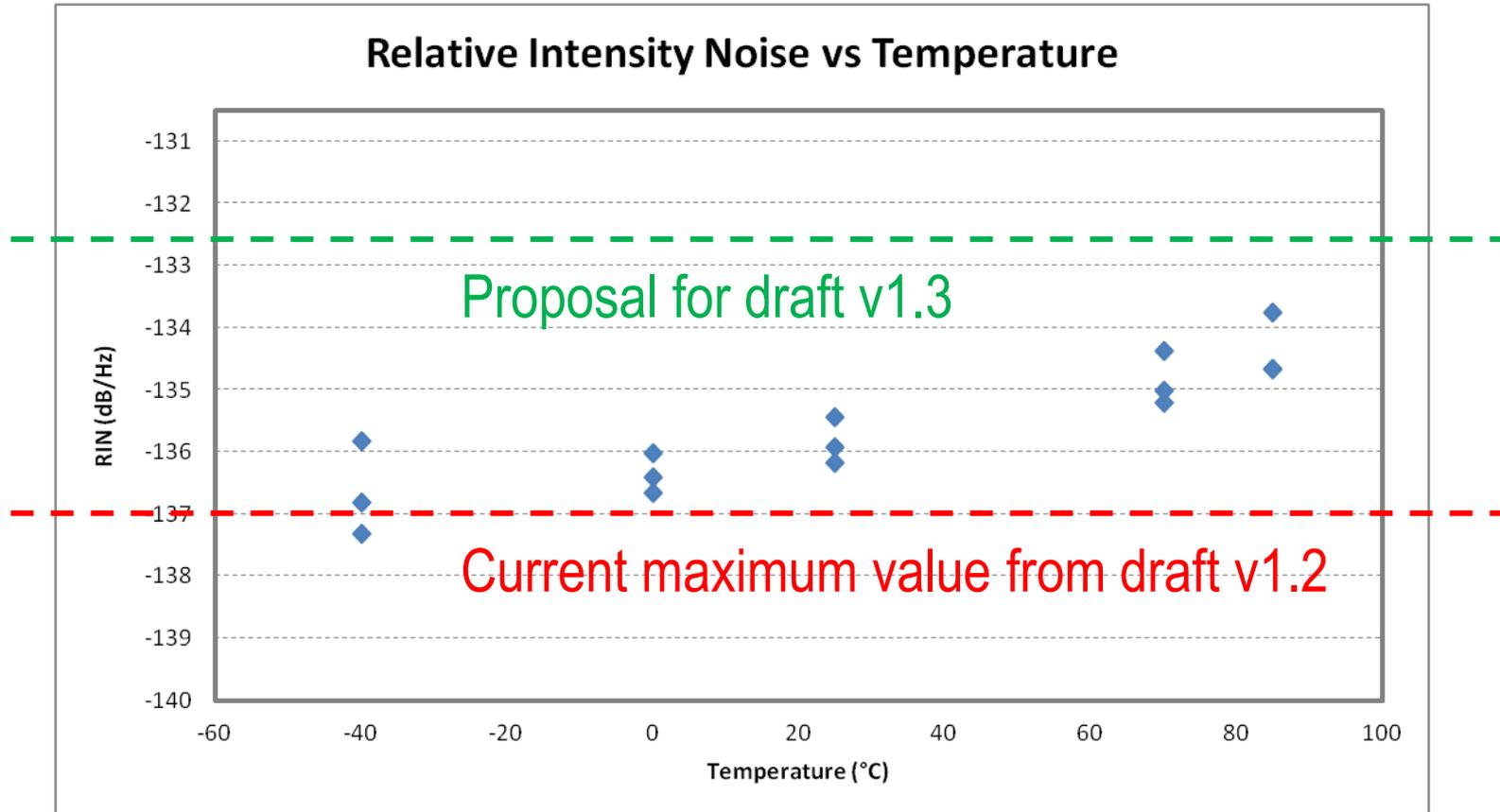
where:

- |             |  |
|-------------|--|
| RIN         | is the relative intensity noise,   |
| 1. $P_N$    | is the electrical noise power in Watts with modulation off,  |
| 2. $BW$     | is the low-pass bandwidth of apparatus – high-pass bandwidth of apparatus due to DC blocking capacitor,  |
| 3. $I_{oe}$ | is the photocurrent of the optical to electrical converter,  |
| 4. $R$      | is the effective load impedance of the optical to electrical converter (for example, a 50 ohm detector load in parallel with a 50 ohm power meter would give R equal to 25), |
| 5. $G$      | is the Gain in dB of any amplifier in the noise measurement path.  |

1. PSD measured w/ SA, calculated in Watts
2. Signal bandwidth -> 162,5 MHz -> 170 MHz were taken for ease of use
3. Conversion gain of OECs output voltage need to be considered -> instead of  $I_{oe}^2 \times R$   
 $U_{oe}^2 / R$  was taken
3. Load impedance of OEC = 50 Ohm
4. Internal amplifier of SA (~ +10 dB) was neglected



# RIN measurement results





# Conclusions

- **Considering the application case up to 85°C, the limit for RIN need to be increased to -132,5 dB/Hz**
- **For a differentiation between several use/application cases with other temperatures, more RIN limits can be taken into account**



**Thank you**