

# Annex 93A

(normative)

## Specification methods for electrical channels

### 93A.1 Channel Operating Margin

Insert new row into Table 93A–1 (as modified by IEEE Std 802.3bs-201x) below the row for parameter “Transmitter equalizer, minimum cursor coefficient” (unmodified rows are not shown):

**Table 93A–1—COM parameters**

Parameter	Reference	Symbol	Units
Transmitter equalizer, 2 <sup>nd</sup> pre-cursor coefficient <sup>a</sup>	93A.1.4.2	$c(-2)$	
Minimum value			—
Maximum value			—
Step size			—

<sup>a</sup>Some clauses that invoke this method do not provide a value for  $c(-2)$ . See 93A.1.4.2.

Change Table 93A–2 (as modified by IEEE Std 802.3by-2016 and IEEE Std 802.3bs-201x) as follows (some unmodified rows are not shown):

**Table 93A–2—Physical Layer specifications that employ COM**

Physical Layer	Parameter values
...	...
25GAUI C2C (Annex 109A)	Table 83D–6
50GBASE-CR (Clause 136)	Table 136–15
50GBASE-KR (Clause 137)	Table 137–5
LAUI-2 C2C (Annex 135B)	Table 83D–6
50GAUI-2 C2C (Annex 135D)	Table 83D–6
50GAUI-1 C2C (Annex 135F)	Table 120D–8
100GBASE-CR4 (Clause 92)	Table 93–8
100GBASE-CR2 (Clause 136)	Table 136–15

**Table 93A-2—Physical Layer specifications that employ COM**

Physical Layer	Parameter values
100GBASE-KR4 (Clause 93)	Table 93-8
100GBASE-KP4 (Clause 94)	Table 94-17
<u>100GBASE-KR2 (Clause 137)</u>	<u>Table 137-5</u>
CAUI-4 C2C (Annex 83D)	Table 83D-6
<u>100GAUI-4 C2C (Annex 135D)</u>	<u>Table 83D-6</u>
<u>100GAUI-2 C2C (Annex 135F)</u>	<u>Table 120D-8</u>
<u>200GBASE-CR4 (Clause 136)</u>	<u>Table 136-15</u>
<u>200GBASE-KR4 (Clause 137)</u>	<u>Table 137-5</u>
200GAUI-8 C2C (Annex 120B)	Table 83D-6 <sup>a</sup>
...	...

<sup>a</sup>With the exceptions given in 120B.4.

### 93A.1.4 Filters

#### 93A.1.4.2 Transmitter equalizer

*Change the text of 93A.1.4.2 as follows:*

$H_{ffe}(f)$  is defined by Equation (93A-21) and is intended to represent the transmitter equalizer. If  $k$  corresponds to a near-end crosstalk path, then  $c(-2)$ ,  $c(-1)$ , and  $c(1)$  are all zero regardless of the values used for the other paths. The value of the “cursor” coefficient  $c(0)$  is set to  $\frac{1 - |c(-2)| - |c(-1)| - |c(1)|}{1 - |c(-2)| - |c(-1)| - |c(1)|}$  for any value of  $c(-2)$ ,  $c(-1)$  and  $c(1)$ . If the value of  $c(0)$  is less than the specified minimum value, the corresponding combination of  $c(-2)$ ,  $c(-1)$ , and  $c(1)$  is considered invalid and is not used to calculate COM.

*Replace Equation (93A-21) with the following equation:*

$$H_{ffe}(f) = \sum_{i=-2}^1 c(i) \exp\left(-j2\pi(i+2)\frac{f}{f_b}\right) \quad (93A-21)$$

#### 93A.1.6 Determination of variable equalizer parameters

*Change the first paragraph of 93A.1.6 (as modified by IEEE Std 802.3bs-201x) and item a) as follows:*

COM is a function of the variables  $c(-2)$ ,  $c(-1)$ ,  $c(1)$ ,  $g_{DC}$ , and  $g_{DC2}$ . The following procedure is used to determine the values of these variables that are used to calculate COM.

- Compute the pulse response  $h_{(k)}(t)$  of each signal path  $k$  for a given  $c(-2)$ ,  $c(-1)$ ,  $c(1)$ ,  $g_{DC}$ , and  $g_{DC2}$  using the procedure defined in 93A.1.5.

Change the last paragraph of 93A.1.6 (as modified by IEEE Std 802.3bs-201x) as follows:

The FOM is calculated for each permitted combination of  $c(-2)$ ,  $c(-1)$ ,  $c(1)$ ,  $g_{DC}$ , and  $g_{DC2}$  values per Table 93A-1, where any parameters not provided by the clause that invokes this method are set to 0. The combination of values that maximizes the FOM, including the corresponding value of  $t_s$ , is used for the calculation of the interference and noise amplitude in 93A.1.7 and the calculation of COM in 93A.1.

Insert new subclause 93A.5 after 93A.4:

## 93A.5 Effective Return Loss

Effective Return Loss (ERL) is a figure of merit for the electromagnetic wave reflection from a device or a channel input or output. ERL shall be calculated using the method described in this annex.

The parameters used to calculate ERL are listed in Table 93A-4. The values assigned to these parameters are defined by the Physical Layer specification that invokes the ERL method.

Table 93A-4—ERL parameters (renumber)

Parameter	Reference	Symbol	Units
Signaling rate		$f_b$	GBd
Transition time associated with a pulse	93A.2	$T_r$	ns
Receiver 3 dB bandwidth	93A.1.4.1	$f_r$	GHz
Number of signal levels		$L$	—
Length of the reflection signal		$N$	UI
Number of samples per unit interval		$M$	—
Equalizer length associated with reflection signal		$N_{bx}$	UI
Incremental available signal loss factor		$\beta_x$	GHz
Permitted reflection from a transmission line external to the device under test		$\rho_x$	—
Target detector error ratio		$DER_0$	—

### 93A.5.1 Pulse time-domain reflection signal

ERL is derived from a unity pulse time-domain reflection signal, PTDR( $t$ ). PTDR( $t$ ) is defined at the test points defined in the Physical Layer specification that invokes the ERL method. PTDR( $t$ ) may be acquired directly from an appropriately filtered time domain reflectometer (TDR), or derived mathematically from measured differential scattering parameters  $S(f)$  (see 93A.1.1) and transmitter and receiver filters, according to the procedure in this subclause.

The filtered return loss,  $H_{ii}(f)$ , is defined by Equation (93A-58).

$$H_{ii}(f) = H_t(f)s_{ii}(f)H_r(f) \quad (93A-58)$$

Where

- $f$  is the frequency in GHz
- $H_r(f)$  is defined by Equation (93A-20)
- $H_t(f)$  is defined by Equation (93A-46)
- $i$  is the port index of the scattering parameters, 1 or 2.

The pulse TDR signal,  $PTDR(t)$ , is defined by Equation (93A-59).

$$PTDR(t) = \int_{-\infty}^{\infty} X(f)H_{ii}(f) \exp(j2\pi ft) df \quad (93A-59)$$

Where

- $t$  is the time in ns starting from the peak of the injected pulse
- $X(f)$  is defined by Equation (93A-23) with  $A_t$  set to 1.

### 93A.5.2 Effective reflection waveform

The effective reflection waveform,  $R_{eff}(t)$ , is computed by time gating and weighting the PTDR waveform,  $PTDR(t)$ , according to Equation (93A-60).  $R_{eff}(t)$  is a pure number.

$$R_{eff}(t) = PTDR(t) \times G_{rr}(t) \times G_{loss}(t) \quad (93A-60)$$

Where  $G_{rr}(t)$  and  $G_{loss}(t)$  are time gating weighting functions defined in Equation (93A-61) and Equation (93A-62) with  $t$  in nanoseconds.

$$G_{rr}(t) = \begin{cases} 0 & t < T_{fx} \\ \rho_x(1 + \rho_x) \exp\left(-\frac{[(t - T_{fx})f_b - (N_{bx} + 1)]^2}{(N_{bx} + 1)^2}\right) & T_{fx} \leq t < T_{fx} + \frac{N_{bx} + 1}{f_b} \\ \rho_x(1 + \rho_x) & t \geq T_{fx} + \frac{N_b + 1}{f_b} \end{cases} \quad (93A-61)$$

Where

- $t$  is the time in ns starting from the peak of the injected pulse
- $T_{fx}$  is twice the propagation delay in ns associated with the test fixture, obtained by measurement or inspection
- $\rho_x, f_b, N_{bx}$  are supplied by the clause that invokes this method.

$$G_{loss}(t) = \begin{cases} 0 & t < T_{fx} \\ 10 \frac{\frac{\beta_x}{f_b}[(t - T_{fx})f_b - (N_{bx} + 1)]}{20} & T_{fx} \leq t < T_{fx} + \frac{N_{bx} + 1}{f_b} \\ 1 & t \geq T_{fx} + \frac{N_{bx} + 1}{f_b} \end{cases} \quad (93A-62)$$

Where

- $t$  is the time in ns starting from the peak of the injected pulse
- $T_{fx}$  is twice the propagation delay in ns associated with the test fixture, obtained by measurement or inspection
- $\beta_x, f_b, N_{bx}$  are supplied by the clause that invokes this method.

### 93A.5.3 Sampled effective reflection

The sampled effective reflection for each phase  $m$  is computed per Equation (93A-63).

$$h^{(m)}(n) = R_{eff}\left(T_{fx} + \frac{n + m/M}{f_b}\right) \quad (93A-63)$$

Where  $n$  is an integer ranging from 1 to  $N$  and  $m$  is an integer ranging from 1 to  $M$ .

The standard deviation of the distribution of the reflection signal for each phase  $m$ ,  $\sigma^{(m)}_h$ , is defined by Equation (93A-64).

$$\sigma^{(m)}_h = \sqrt{\sum_{n=1}^N h^{(m)}(n)^2} \text{ dB} \quad (93A-64)$$

Where  $m$  is an integer ranging from 1 to  $M$ .

### 93A.5.4 $x$ -quantile of the reflection distribution

The reflection signal distribution  $p(y)$  is computed from the sampled effective reflection using the procedure defined in 93A.1.7.1, with  $h(n) = h^{(m)}(n)$ , where  $m$  maximizes  $\sigma^{(m)}_h$ . The value of  $L$  in Equation (93A-39) is supplied by the clause that invokes this method. The corresponding cumulative distribution function  $P(y)$  is calculated from  $p(y)$  using Equation (93A-37).

The  $x$ -quantile of the distribution,  $P^{-1}(x)$ , is the value of  $y$  that satisfies the relationship  $P(y)=x$ .

### 93A.5.5 ERL

ERL is defined as  $20 \times \log_{10} P^{-1}(DER_0)$  where  $DER_0$  is the target detector error ratio.