

# In Response to TDECQ/SECQ Questions for Threshold Adjustments and Proposed Changes

(Comments r01-98, r01-104, r01-99, r01-103, r01-102, r01-97)\*

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David Leyba, Keysight; Hai-Feng Liu, Intel  
Marco Mazzini, Cisco; Kohichi Tamura, Oclaro  
Mingshan Li, AOI; Mark Heimbuch, Source  
Winston Way, NeoPhotonics; Mark Kimber, Semtech  
Phil Sun, Credo Semiconductors

Special thanks to Ali Ghiasi for fruitful discussion on making the point that TDECQ value without threshold adjust may require guard band during implementation, but adjustable threshold receiver would require adjustable threshold SRS stressor.

\*: With data to support comment resolutions for adding Adaptive Threshold Adjustments in computing TDECQ values (floating slicing)

IEEE P802.3cd March Plenary; 5 March 2018; Rosemont, IL

# Update supporter list from Liu\_3cd\_01b\_0118

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- Stephen Didde (Keysight)

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- David Lewis (Lumentum)
- David Li (Hisense)
- Mike Wang (Hisense)
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- Samuel Liu (Nokia)
- Chongjin Xie (Alibaba)
- Earl Parsons (CommScope)
- Pirooz Toyserkani (Cisco)
- Jane Lim (Cisco)
- Matt Traverso (Cisco)
- Tomoo, Takahara (Fujitsu Lab)
- Tongqing Wang (Luxar Tech)

## ❑ Problem Statements

- ❑ To follow up discussion/questions from Jan interim

## ❑ Why threshold adjustment is necessary

- ❑ Make the reference receiver close to real receiver by adding threshold adjustments

## ❑ Show improved correlation with threshold adjustment

- ❑ Current correlation with D3.1 is considered arguably “poor”.

## ❑ Minimum impact on Rx side under SRS

- ❑ Using real ASICs under low power DSP mode mimic reference 5T equalizers.

# Problem Statements

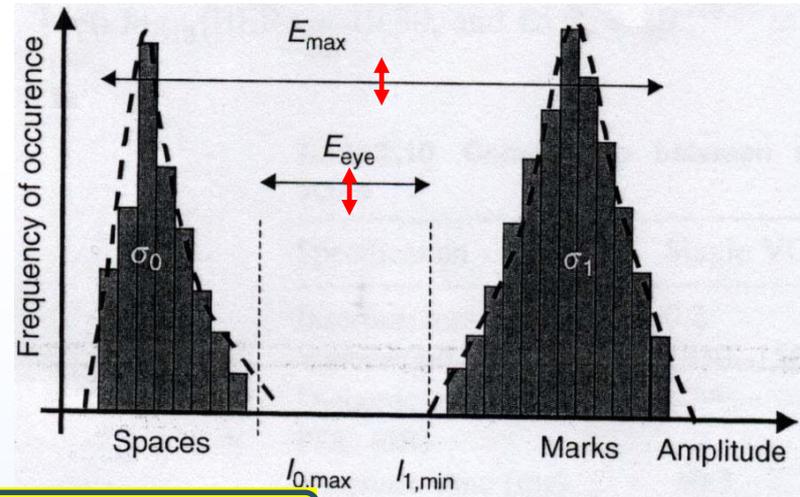
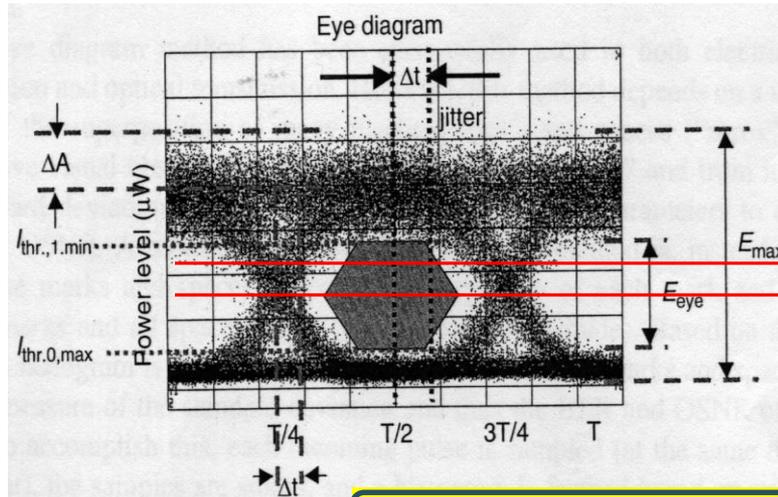
- ❑ Strong support to add Adaptive Slicing in Ref. equalizers to resolve TDECQ specs dilemma ([mazzini\\_120617\\_3cd\\_adhoc-v2](#))
  - ❑ Supported by 27+ companies including majority module and IC vendors as well as systems vendors/users.
  - ❑ Extensive data demonstrated some improvements (~0.3-0.4dB) across all transmitter types: DML, VCSEL, EML, and MZM.
  - ❑ Keysight and Tektronix have just released in mid Feb new beta FW with floating thresholds as defined in recent proposal. It includes setting an adjustable limit.
- ❑ Some questions asked “why threshold adj. is needed?” in real RX IC implementation – a tutorial.
- ❑ No analog equalizers available with 5T for link BER measurements.
- ❑ Follow up questions from the editorial team (cite Jonathank)
  - ❑ Show improves correlation between TDECQ vs measured receiver sensitivity.
  - ❑ Show not too high a stress for the receiver in SRS tests

# Why Threshold Adjustment is Necessary (1)

- Threshold adjustment has been well deployed for CDRs & SerDes IC for NRZ systems (2.5, 10G, 25G) with direct detection
  - Either manual or adaptive for optimized BER, refs. e.g.
    - 1) Matsumoto et al. “*An adaptive decision threshold control of the optical receiver for multi-gigabit terrestrial DWDM transmission systems*”; OFC 2001, Paper TuR2, March 2001. (2.5G NRZ)
    - 2) Park et al. “*Performance Analysis for Optimizing Threshold Level Control of a Receiver in Asynchronous 2.5 Gbps/1.2 Gbps Optical Subscriber Network with Inverse Return to Zero(RZ) Coded Downstream and NRZ Upstream Re-modulation*”; J. OSK V.13, No.3. pp361-366, Sept 2009. (2.5G/1.25G NRZ)
    - 3) Yan et al. “*Performance enhancement in 10-Gb/s long-haul fiber links with adaptive eye mapping in an integrated Si-CMOS 16-bit transceiver IC*”; IEEE Photonics Tech. Letters, Vol.17, No.8, pp1752-4, Aug. 2005. (10G NRZ)
    - 4) Chang et al; “*Accurate in-situ monitoring of Q-factor and BER using adaptive sampling in a 10Gb/s CMOS optical receiver IC*”; IMS05, Paper WEPL-3, June 2005. (10G NRZ)
- Similar practice in QAM systems like QPSK & 16QAM for 100+G coherent DSP, refs. e.g.
  - 1) Chiba et al. “*Adaptive threshold adjustment for signal distortion-free digital-coherent optical demodulation system*”; Vol.16, No.26, Opt. Express, pp21647-55, Dec. 2008.

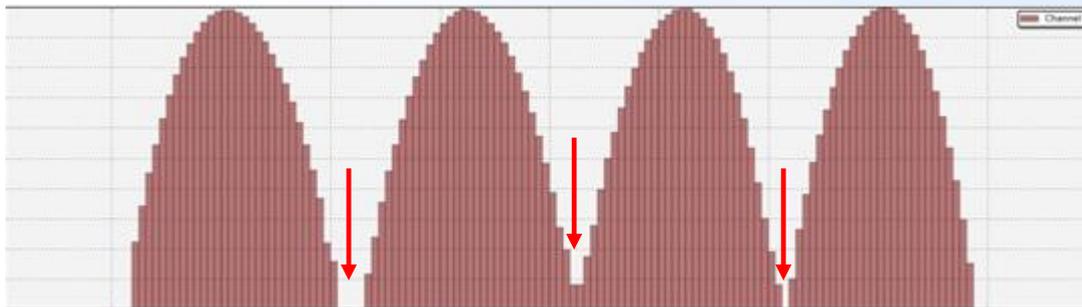
# Why Threshold Adjustment is Necessary (2)

- Results from unevenly distributed noise on 0/1 levels



Average threshold  $\neq$  Optimum point

- Actually measured PAM4 histograms show similar

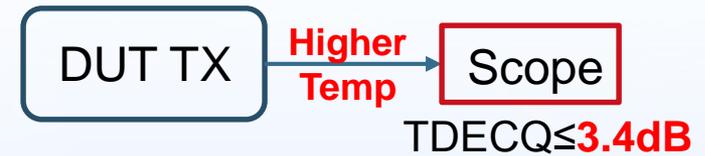
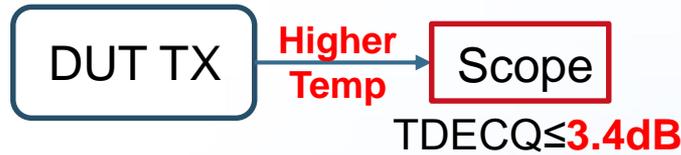
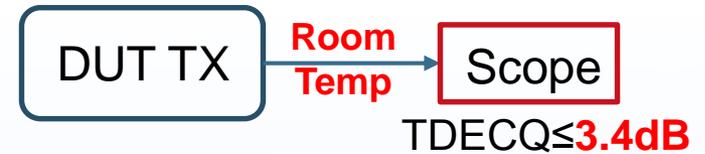
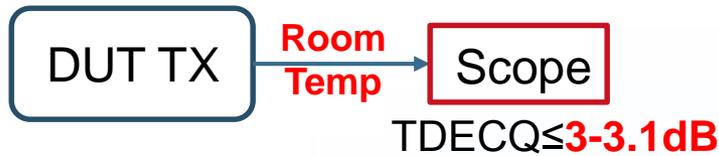


In real ASIC implementations, decision threshold level and phase of received data in the decision circuit are automatically adjusted to the optimum position

# Why Threshold Adjustment is Necessary (3)

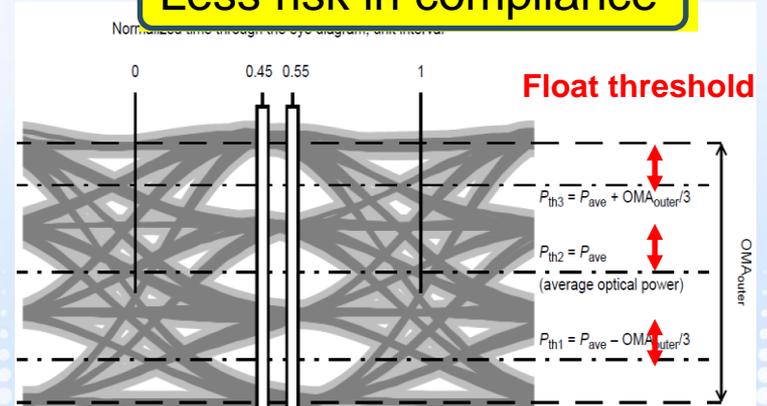
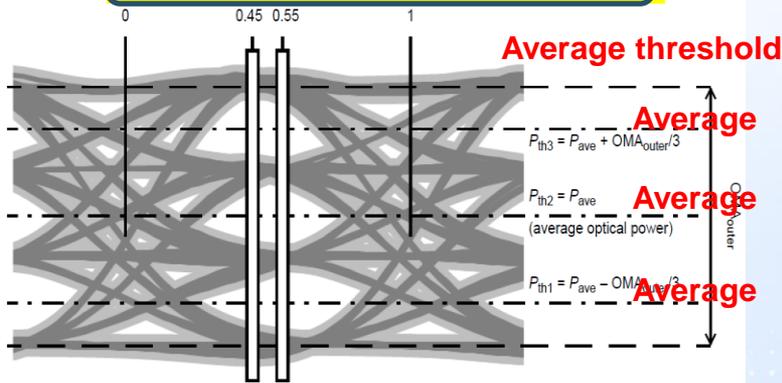
## ■ Threshold adjustment help improve implementing TDECQ

- NO **Guard Band** needed to compensate for threshold variations with Temp.
- D3.1 case: 0.3-0.4dB guardband needed - With threshold Adjustments



More risk in compliance

Less risk in compliance



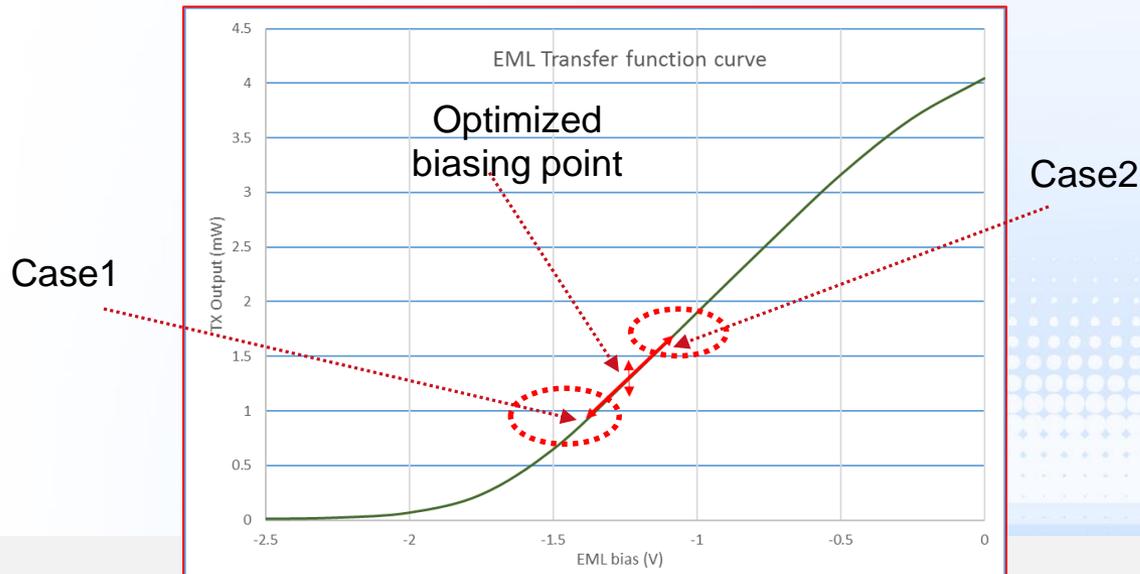
Threshold Adjustment help reduce the risk in product test compliance

# Correlate TDECQ with Rx Sensitivity

Under well controlled lab environments with golden EML TOSA, following 3 scenarios are considered for threshold adjustment within the limit of <2%

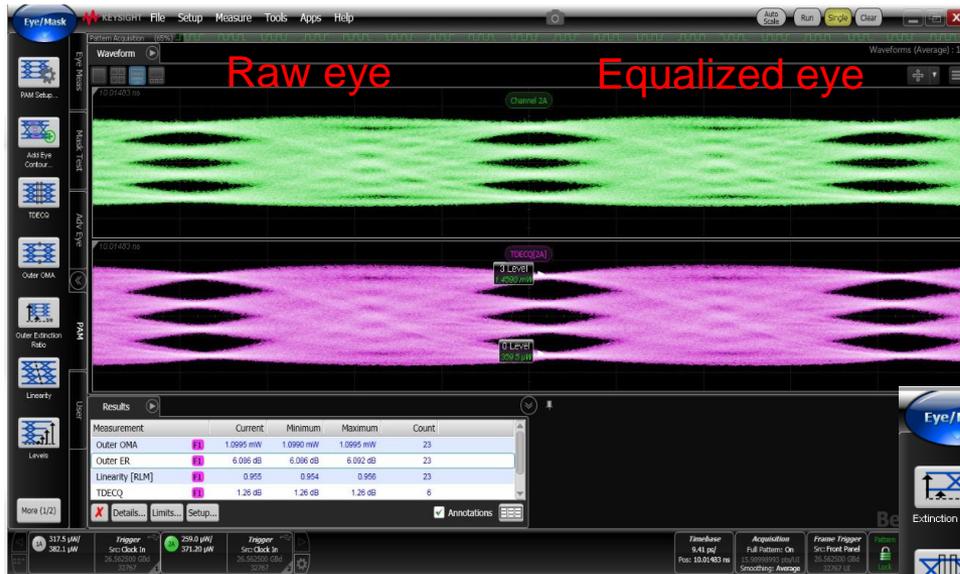
- (Setup refer to [chang\\_011018\\_3cd\\_02\\_adhoc-v2](#) & [chang\\_3cd\\_01a\\_0917](#))

- Full optimized EML condition, full link optimized with best BER condition.
  - Optimized EML Bias voltage, and Linear driver nonlinearity
- Off-optimized conditions,
  - Keep default EML bias voltage (VEML), vary Linear driver nonlinearity
- Unoptimized Case 1: Move two TX setting downwards;
  - Vary VEML bias down by ~ 150mV, and vary driver gain accordingly (all the rest no change)
- Unoptimized Case 2: move TX setting upwards;
  - Vary VEML bias up by ~ 150mV and vary driver gain accordingly (all the rest no change)

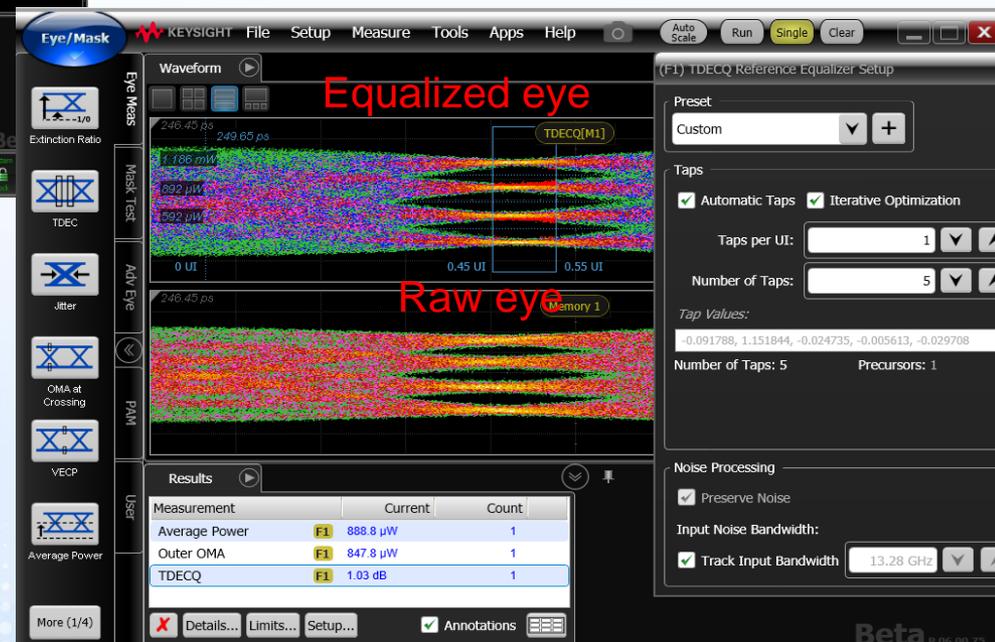


# TX eye diagrams: optimized condition (D3.1)

Full optimized case (D3.1) ER=6.1dB  
TDECQ/SECQ=1.26dB, RLM=0.955



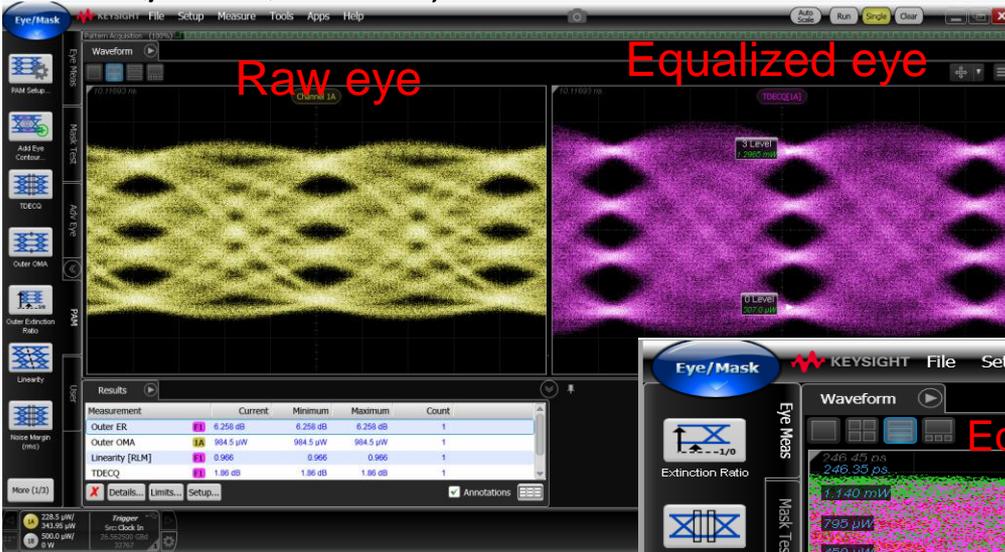
Optimized case D3.1 with threshold Adj  
TDECQ/SECQ=1.03dB



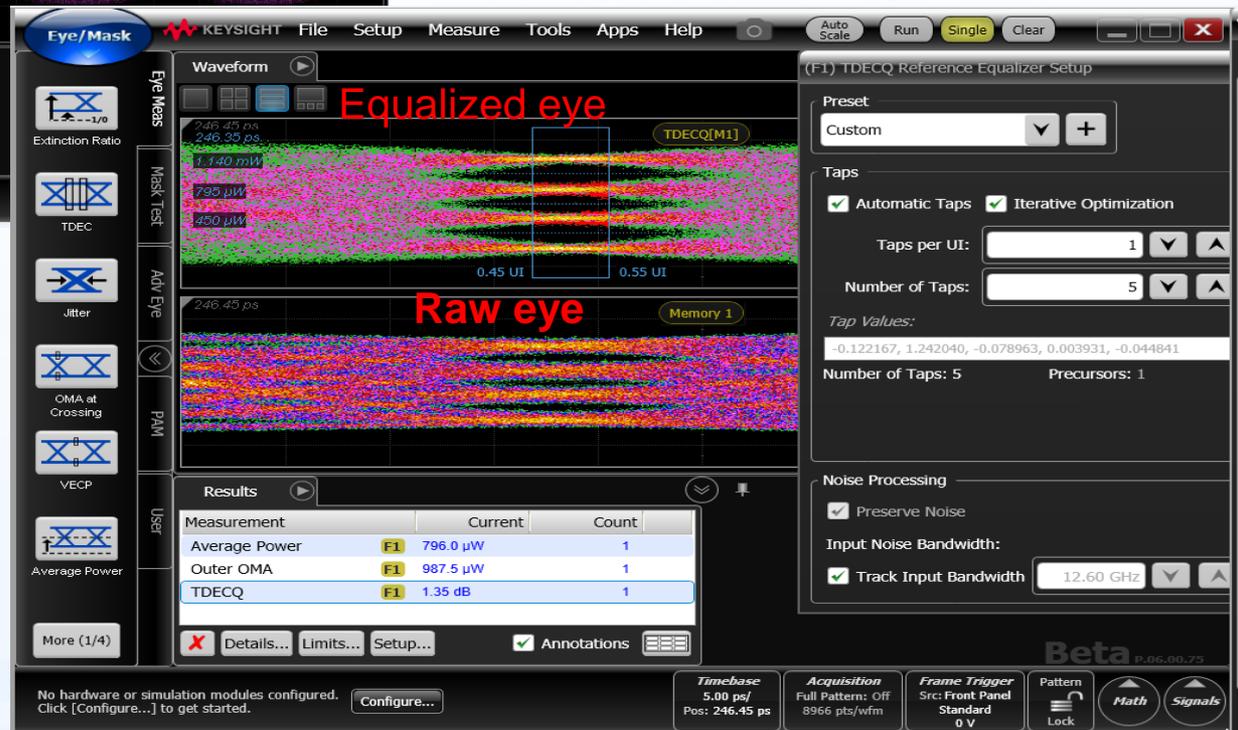
Note: TDECQ/SECQ tests for slides#9-12 are actually SECQ (without test fiber) and based on PRBS15 pattern.

# TX eye diagrams: off-optimized condition (D3.1)

Off-optimized case (D3.1) ER=6.2dB  
 TDECQ/SECQ=1.86dB, RLM=0.966



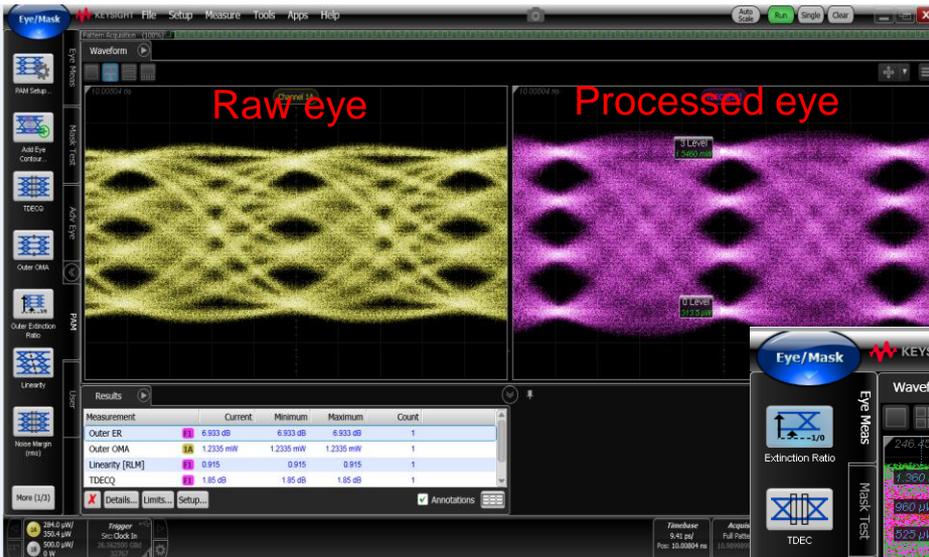
Off-optimized case D3.1 with threshold Adj  
 TDECQ/SECQ=1.35dB, Adj~1.% of OMAouter



		Adj	%
Pth3	1130.167	-9.83333	-0.99%
Pavg	796	-1	-0.13%
Pth1	466.8333	-6.83333	-0.69%

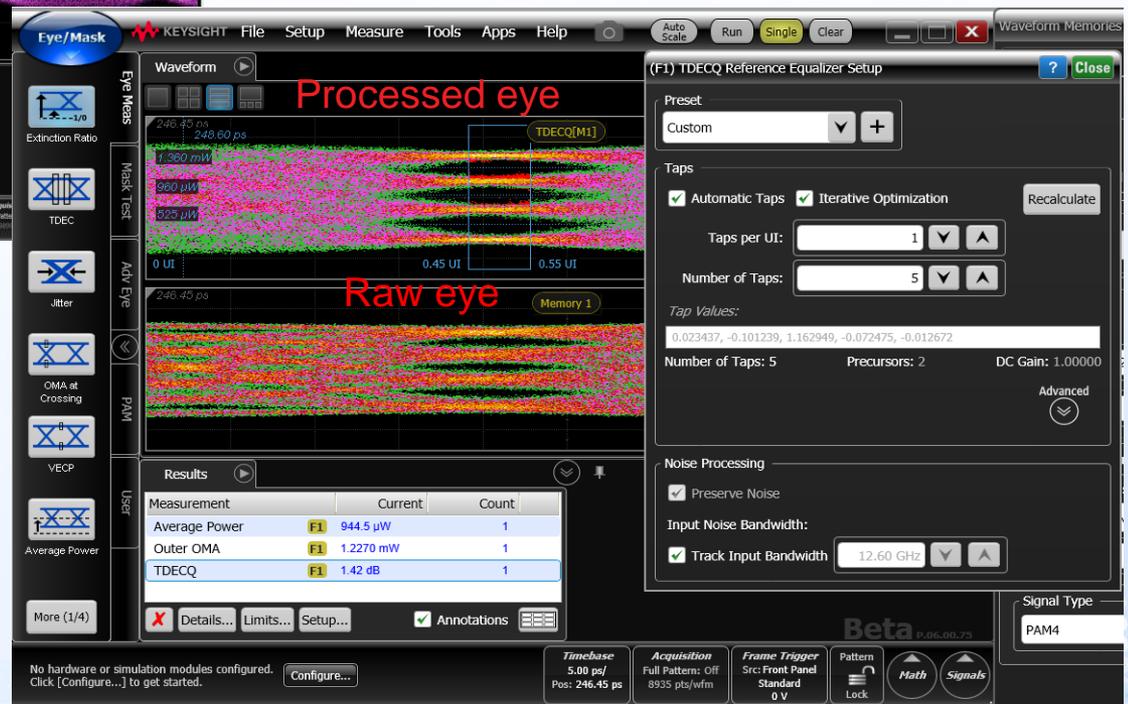
# TX eye diagrams: Case1 (D3.1)

Unoptimized Case1: ER=6.9dB  
TDECQ/SECQ=1.85dB, RLM =0.915



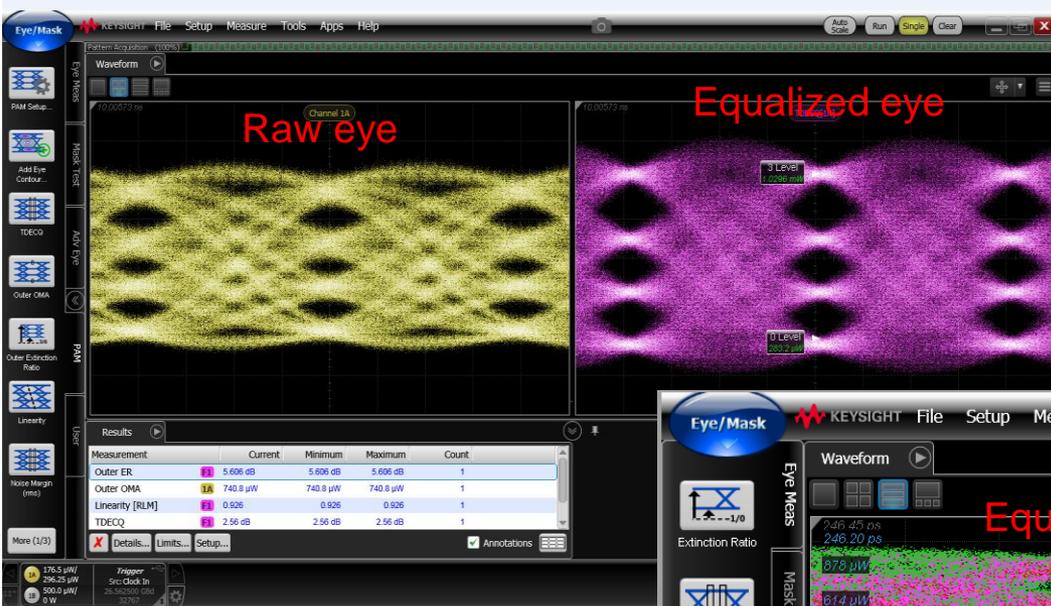
Case1(D3.1 with threshold Adj)  
TDECQ/SECQ=1.42dB Adj within +1.95%

	Adj	%
Pth3	1353.5	6.5 0.53%
Pavg	944.5	15.5 1.95%
Pth1	535.5	-10.5 -0.86%



# TX eye diagrams: Case2 (D3.1)

Unoptimized case2 ER=5.6dB,  
TDECQ/SECQ=2.56dB, RLM =0.926



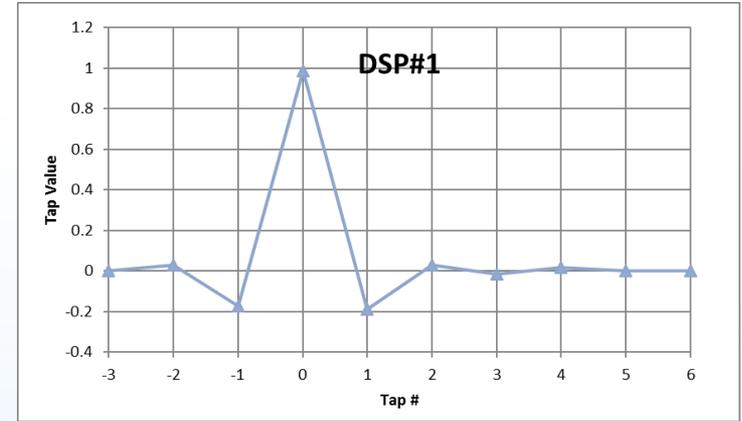
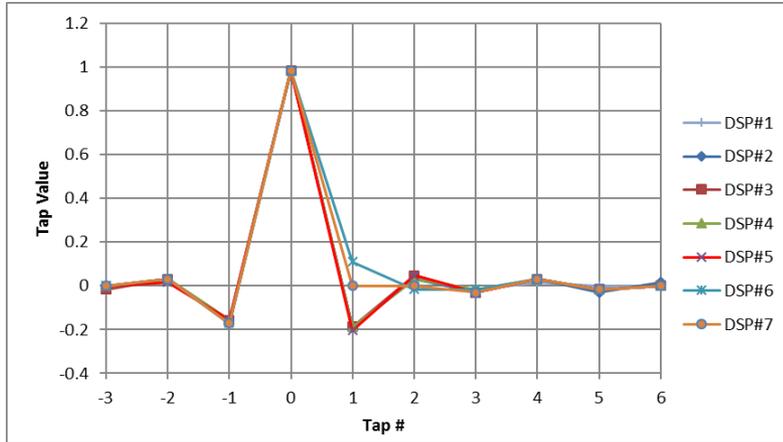
Case2 (D3.1 with threshold Adj)  
TDECQ/SECQ=1.68dB, Adj within -1.93%



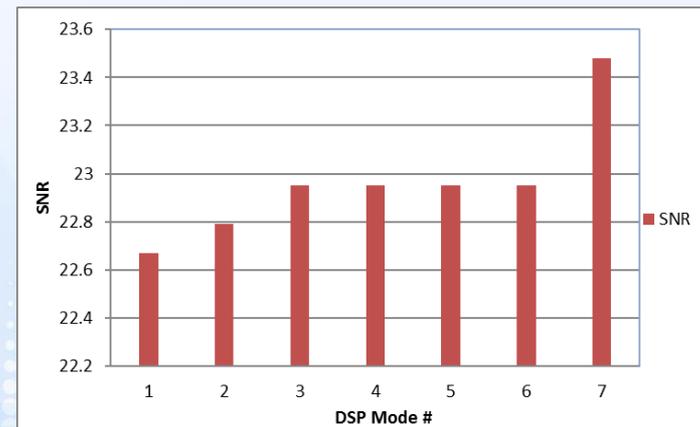
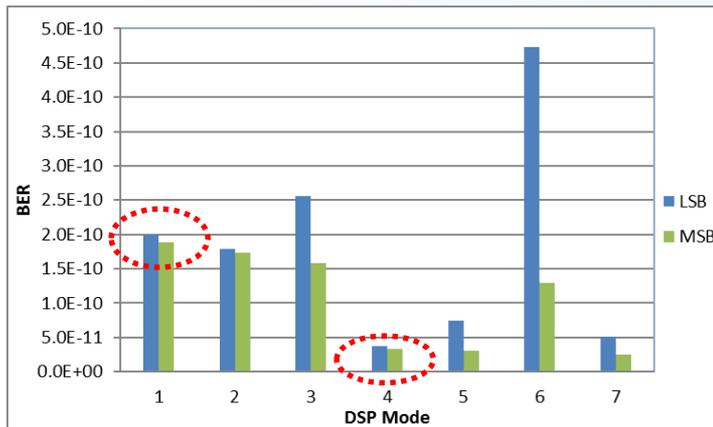
		Adj	%
Pth3	877.3333	0.666667	0.09%
Pavg	629.4	-15.4	-1.93%
Pth1	381.4667	0.533333	0.07%

# Correlate TDECQ with Rx Sens: how to tackle the analog equalizer non-availability issue

- Emulated low power DSP Mode with closer to Ref 5T equalizers for link BER measurements.

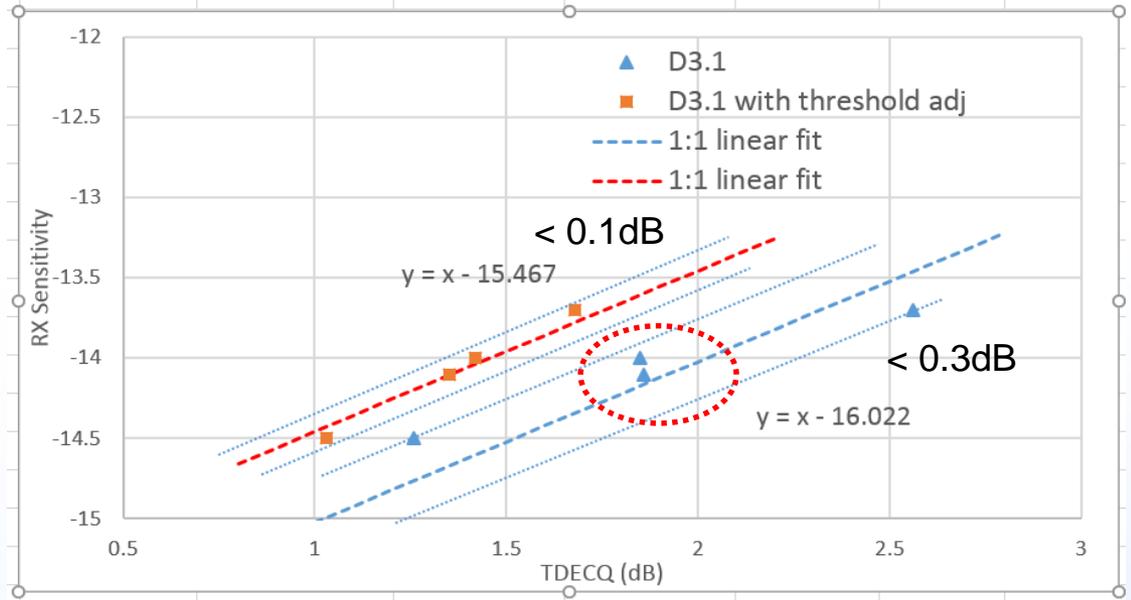
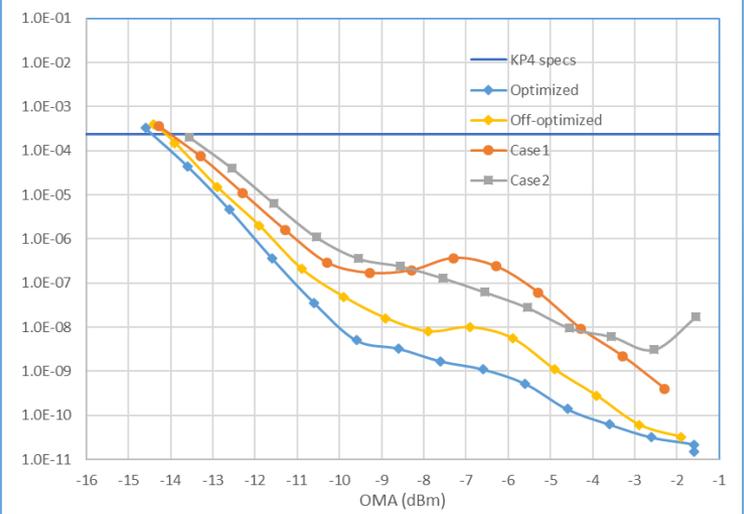


- Comparing performance of various DSP modes (for BER flooring)



# Correlate TDECQ with Rx Sensitivity

## Link BER performance



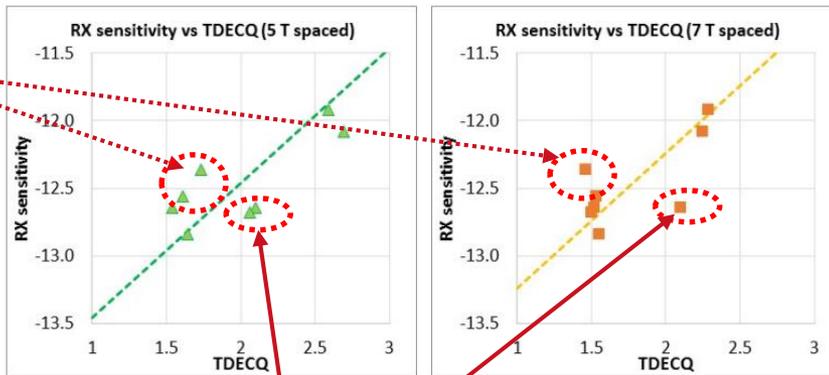
	Full optimized	off-optimized	Case1 <-2%	Case2 <+2%
EML bias	-1.28	-1.26	-1.41	-1.12
ER	6.1	6.2	6.9	5.6
TDECQ (D3.0)	1.26	1.86	1.85	2.56
TDECQ (TH adj)	1.03	1.35	1.42	1.68
OMA Sens.	-14.5	-14.1	-14	-13.7

Show better correlation with TDECQ and predict well how RX sens. will vary when threshold adjustment is implemented with limits

# Correlating TDECQ with Rx Sensitivity (D3.1)

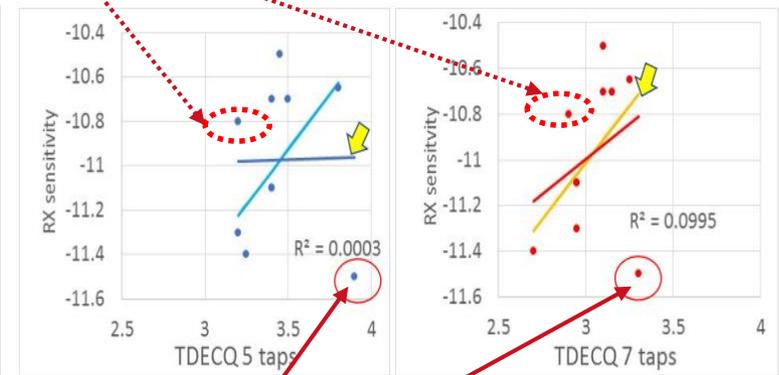
- Some thoughts: All of us who took the data feel this correlation is “poor”. Where is the “disconnection” with data analysis by [king\\_3cd\\_01\\_0118](#)?
  - The data analysis were good but based on statistics in macro scale with large fitting error of 0.3-0.4dB. If looking into individual TOSAs, there are many exceptions for the situation that good TDECQ values delivers worse RX Sens and vice versa, so simply tough to predict RX sensitivity from TDECQ values with D3.1, for examples:

Analysis of way\_3bs\_01a\_0517



RMS error vs best fit to 1:1 slope: 0.26 dB      0.25 dB

Analysis of baveja\_3cd\_01\_1117, slide 1



RMS error vs best fit 1:1 slope: 0.40 dB      0.32 dB

Good TDECQ, but worse sens.

Good TDECQ, but worse sens.

Worse TDECQ, but good sens.

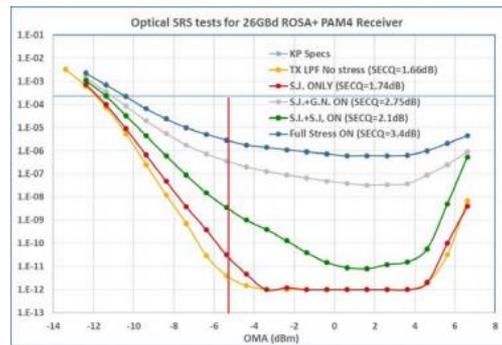
Golden part with best sens. but TDECQ bad

# The Impact to RX SECQ (D3.1)

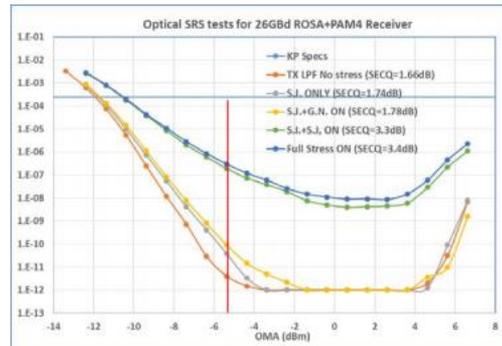
- Recap current analysis with D3.1 by ([king\\_3cd\\_01\\_0118](#))
  - LN MZM TX for instrument testers are well behaved linear devices, and expect to show better correlation.

Analysis of chang\_cd\_01\_1117: BER plots vs SECQ (5 tap T-spaced)

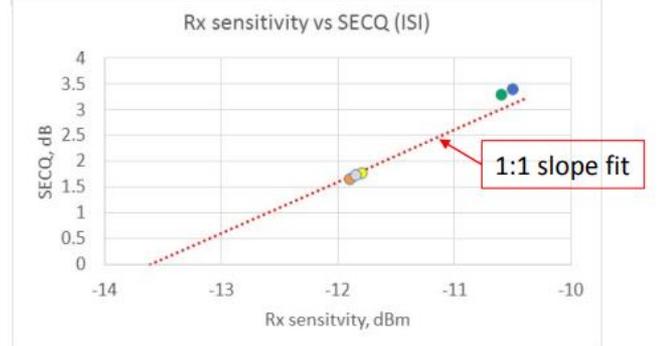
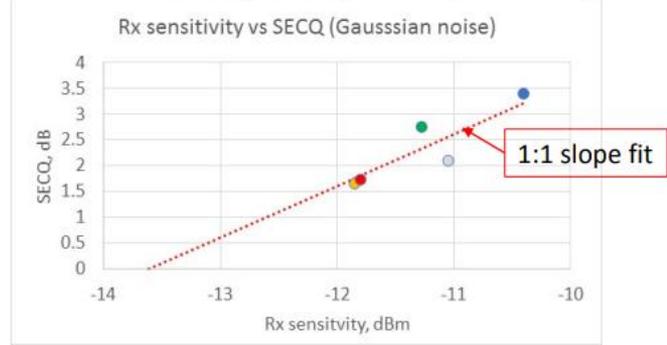
Gaussian noise dominant  
RMS error < 0.3 dB



SI dominant  
RMS error < 0.2 dB



Very good dB/dB fit for both cases



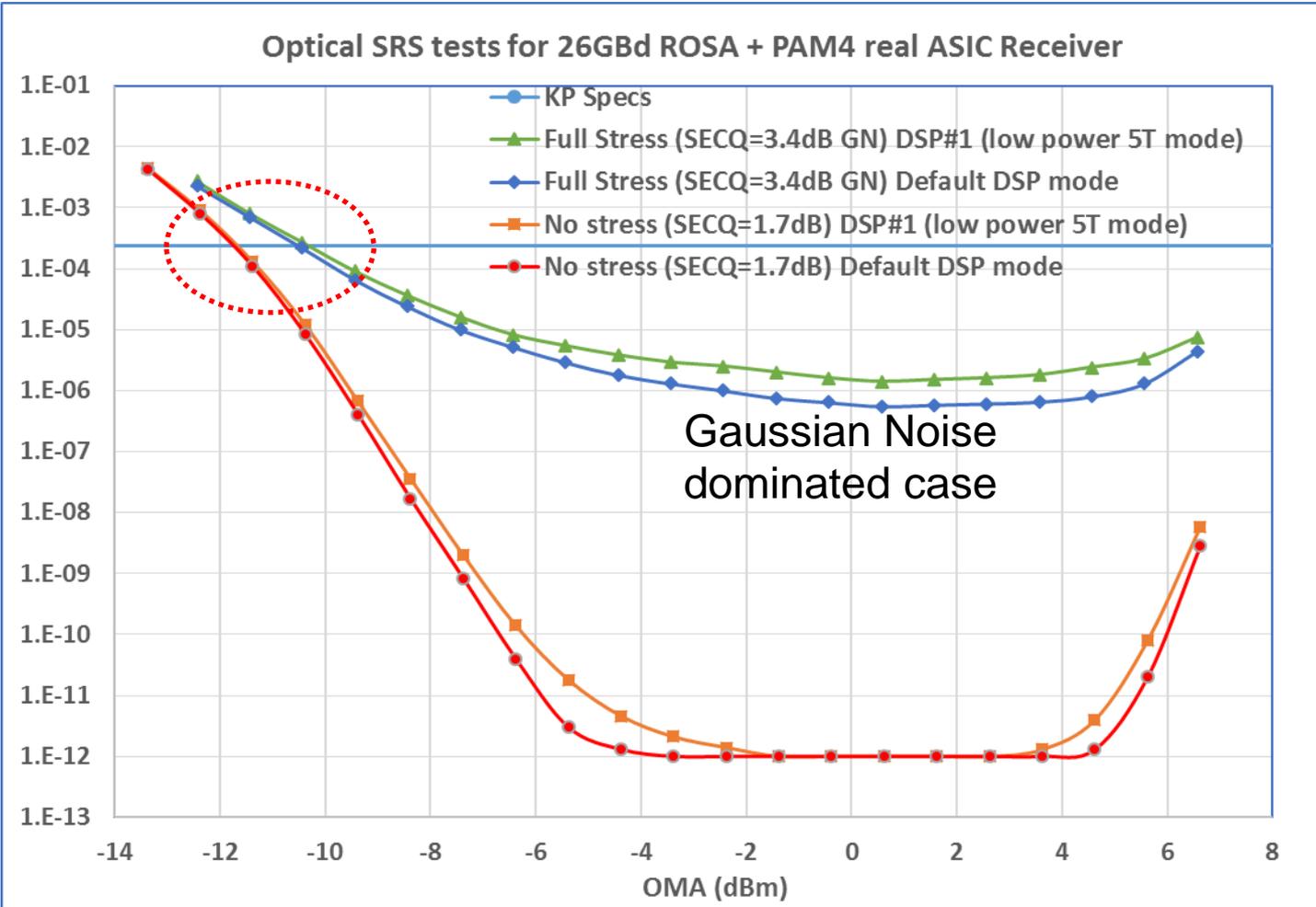
- chang\_3cd\_01\_1117 concluded that “There exists strong interplay between G.N and S.I (with S.J.). G.N. impact most the BER degradation in SRS.”. But the data shows very good correlation between SECQ and Rx sensitivity for both GN and SI dominant stress (RMS error of <0.3 dB)

# Impact to RX SRS (D3.1) by different DSP modes

- Negligible impact on RX SRS Sensitivity by different DSP modes. (only little degrade on BER flooring) [chang\\_3cd\\_01\\_1117](#)

LM MZM TX  
SSPRQ pattern

Compare Rx  
SRS under  
different DSP  
modes for no  
(B2B) and fully  
stressed

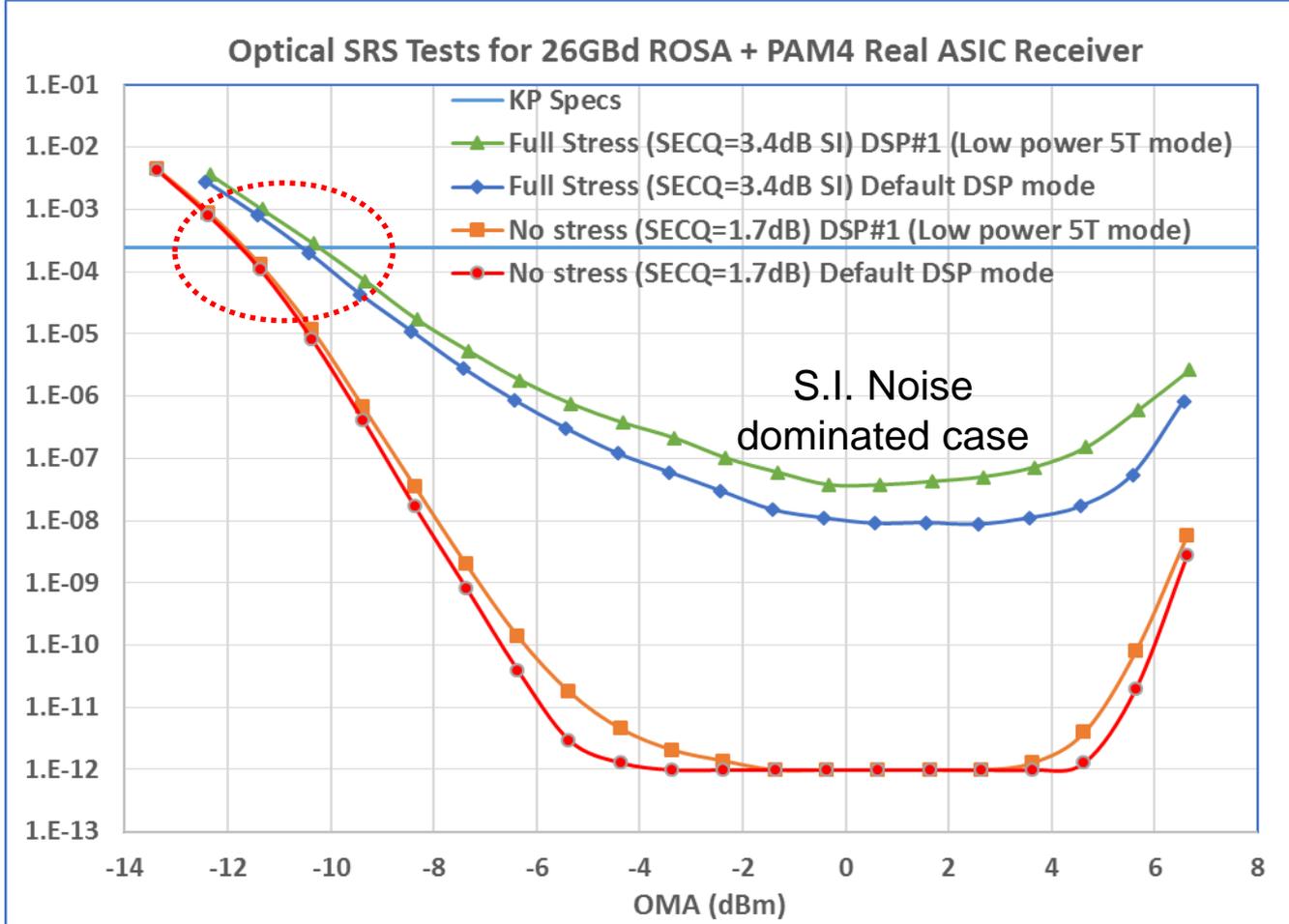


# Impact to RX SRS (D3.1) by different DSP modes

- Negligible impact on RX SRS Sensitivity by different DSP mode. (only little degrade on BER flooring) [chang\\_3cd\\_01\\_1117](#)

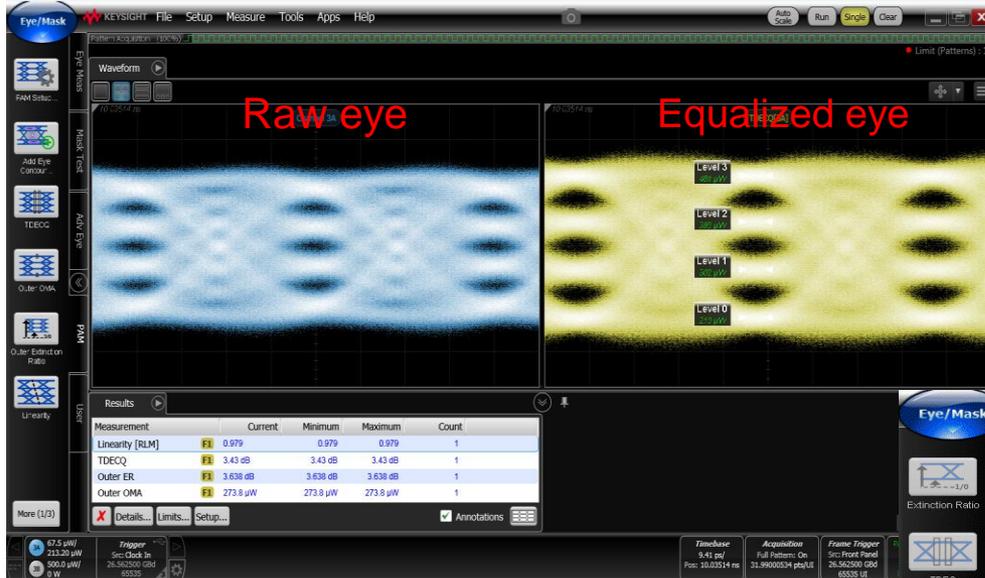
LM MZM TX  
SSPRQ pattern

Compare Rx  
SRS under  
different DSP  
modes for no  
(B2B) and fully  
stressed

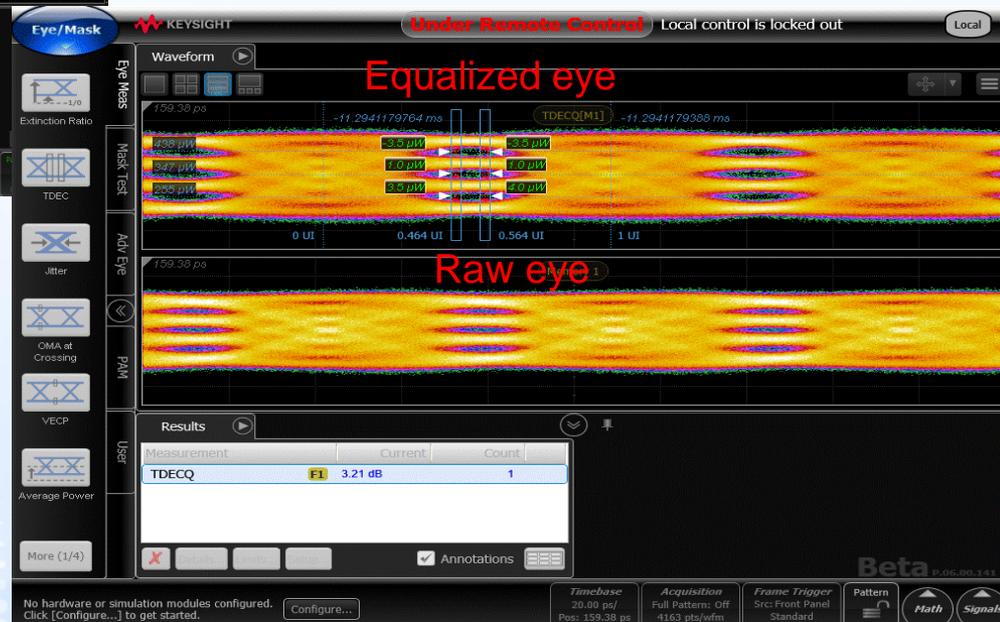


# The Impact to RX SECQ

D3.1 Full stressed, RX LPF~13.28GHz  
 - SECQ=3.43dB, ER=3.6dB



Re-process using new beta FW release  
 with threshold Adj  
 SECQ=3.21dB, Adj within 1.46%

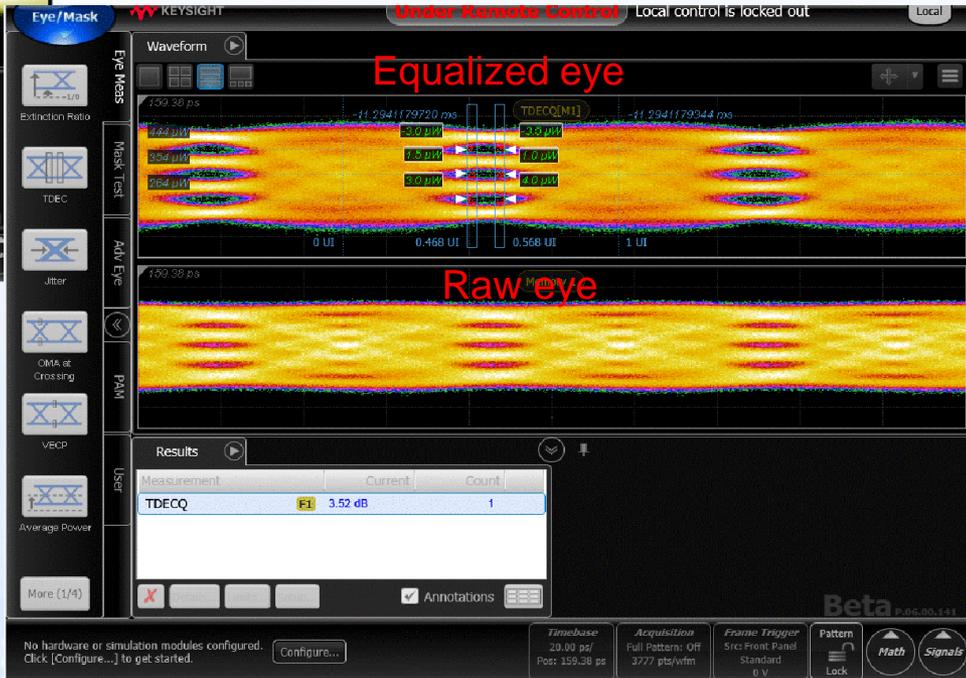


	uW	Adj (uW)	
Pth3	438	-3.5	-1.28%
Pavg	347	1	0.37%
Pth1	255	4	1.46%
OMAouter	273.8		

# The Impact to RX SECQ

D3.1 over-stressed, RX LPF~13.28GHz  
 SECQ=3.64dB, ER=3.5dB

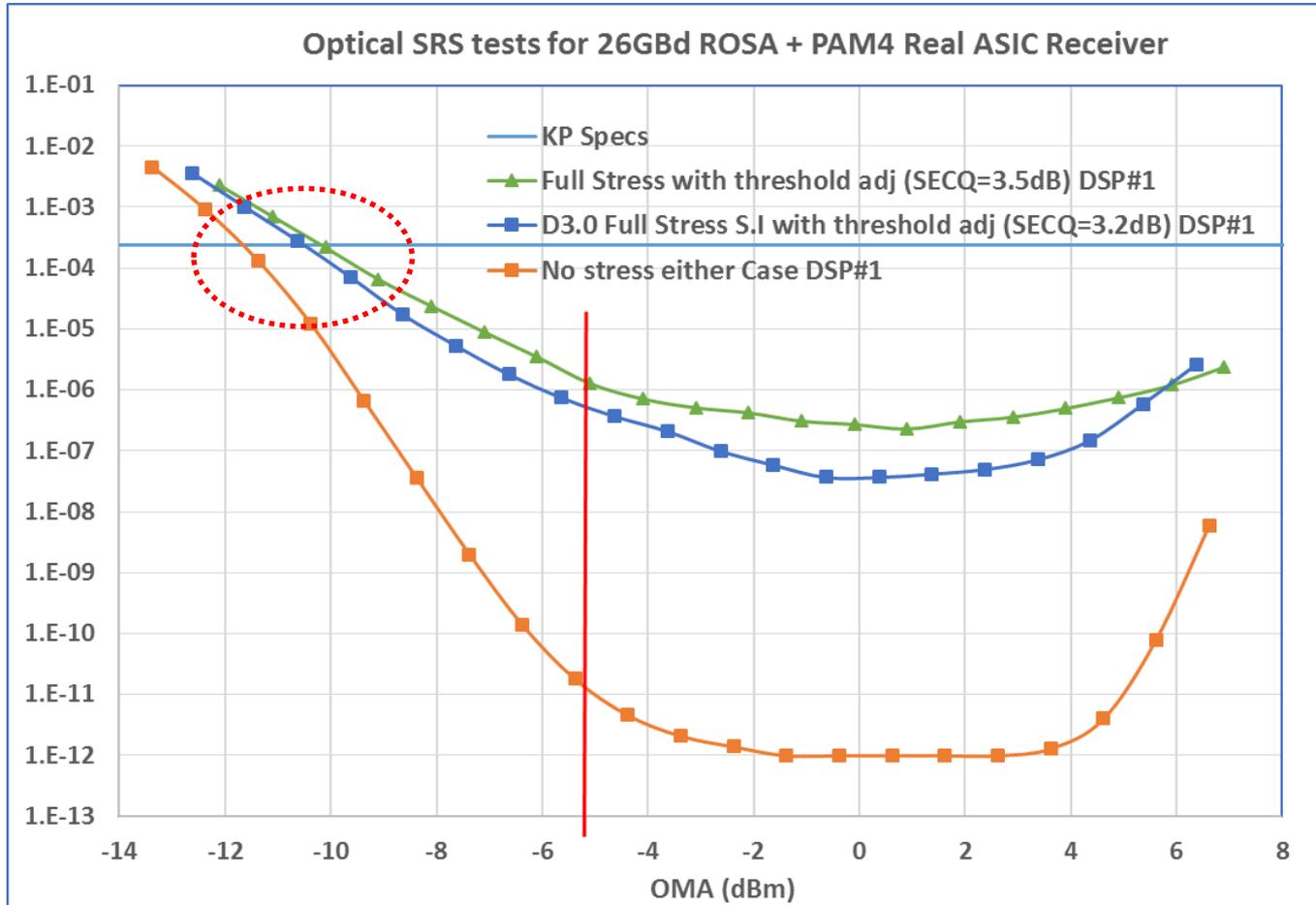
Re-process using new beta FW  
 release with threshold Adj  
 SECQ=3.52dB, Adj within -0.73%



	uW	Adj (uW)	
Pth3	446	-2	-0.73%
Pavg	354	1	0.37%
Pth1	263	1.5	0.55%
OMAouter	274.7		

# The Impact to RX SRS Sensitivity

- The impact on the Rx SRS is  $<0.2\text{dB}$ .
  - The real ASIC has threshold adjustment implemented.



# Concluding Remarks (1)

- Adding threshold adjustment help resolve the implementation issue to leave the guard band reserved for environmental variations like temperature and aging.
- Measured link BER with an emulate 5T equalizers by operating at low power DSP mode.
  - Eliminate the dilemma due to the non-availability of analog equalizers usable for such kinds of tests.
- Show threshold adjustments significantly improves correlation between TDECQ vs measured receiver sensitivity.
- The stress on RX SRS tests falls well within 0.1-0.2dB (or less). It seems much less than what we originally thought after setting the limits to the adjustable range.

# Concluding Remarks (2)

- Minimum risks to add threshold adjustment into TDECQ algorithm.
  - Unless real receiver have threshold adjustment, the transmitter environmental variations and aging will result in TDECQ degradation requiring TDECQ guard band, otherwise there will be a “hole” in specification.
  - Real receivers optimize the decision thresholds, so the TDECQ reference receiver can also be allowed to optimize thresholds. If the adjustment range for each threshold is much smaller than that of real receivers, the receiver specifications can remain unchanged.
- This will make significant improvement over D3.1
  - Lower risk for compliance test.

# Proposed Change: 138.8.5

Insert the text shown below in red to the list of exceptions

<b>138.8.5 Transmitter and dispersion eye closure - quaternary (TDECQ)</b>	17
	18
TDECQ is a measure of each optical transmitter's vertical eye closure as measured through an optical to electrical converter (O/E) with a bandwidth equivalent to a combined reference receiver and worst case optical channel, and equalized with the reference equalizer specified in 138.8.5.1. Table 138-9 specifies the test pattern to be used for measurement of TDECQ.	19
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TDECQ of each lane shall be within the limits given in Table 138-8 if measured using the methods specified in 121.8.5, with the following exceptions:	24
	25
— The polarization rotator and test fiber shown in Figure 121-4 are not used	26
	27
— The optical channel requirements in 121.8.5.2 do not apply	28
	29
— The combination of the O/E and the oscilloscope used to measure the optical waveform has a fourth-order Bessel-Thomson filter response with a bandwidth of 11.2 GHz.	30
	31
— The reference equalizer to be used for TDECQ for 50GBASE-SR, 100GBASE-SR2, and 200GBASE-SR4 is specified in 138.8.5.1.	32
--- $P_{th1}$ , $P_{th2}$ , and $P_{th3}$ are varied by up to 2% of $OMA_{outer}$ .	

# Proposed Change: 139.7.5.3

Change the text as shown below in red.

## 139.7.5.3 TDECQ measurement method

~~TDECQ for 50GBASE-FR and 50GBASE-LR is measured as described in 121.8.5.3 with the exception that the reference equalizer is as specified in 139.7.5.4.~~

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TDECQ for 50GBASE-FR and 50GBASE-LR is measured as described in 121.8.5.3 with the following exceptions:

- The reference equalizer is as specified in 139.7.5.4
- $P_{th1}$ ,  $P_{th2}$ , and  $P_{th3}$  are varied by up to 2% of  $OMA_{outer}$

# Proposed Change: 140.7.5

Insert the text shown below in red to the list of exceptions

## 140.7.5 Transmitter and dispersion eye closure for PAM4 (TDECQ)

The TDECQ shall be within the limits given in Table 140–6 if measured using the methods specified in 121.8.5.1, 121.8.5.2, and 121.8.5.3 using a reference equalizer as described in 140.7.5.1, with the following exceptions:

- The optical return loss of the transmitter compliance channel is 15.5 dB.
- The signaling rate of the test pattern generator is as given in Table 140–6 and uses a test pattern specified for TDECQ in Table 140–10.
- There are no interfering optical lanes and therefore the delay requirement of at least 31 UI between test pattern on one lane and any other lane, as specified in 121.8.5.1, is redundant.
- The combination of the O/E converter and the oscilloscope has a fourth-order Bessel-Thomson filter response with a bandwidth of approximately 26.5625 GHz.
- The normalized noise power density spectrum,  $N(f)$  in Equation (121–9), is equivalent to white noise filtered by a fourth-order Bessel-Thomson response filter with a bandwidth of 26.5625 GHz.
- $P_{th1}$ ,  $P_{th2}$ , and  $P_{th3}$  are varied by up to 2% of  $OMA_{outer}$ .

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Thank You