

Automotive link segment for 10SPE including multidrop

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Overview

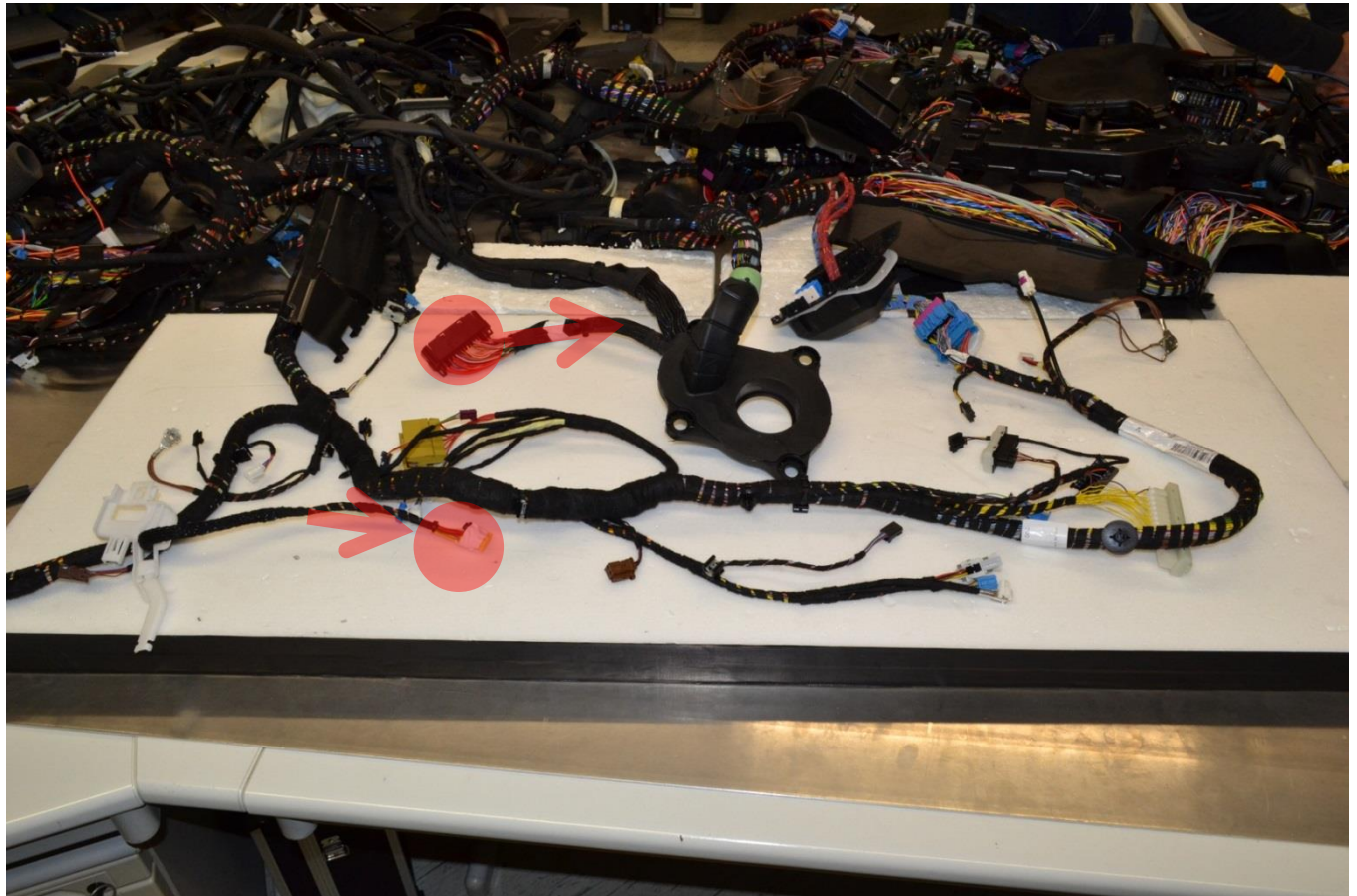
- Goal for 10SPE automotive PHY must be to run on “CAN-like” or “FlexRay-like” cabling and connector configurations
- Bert Bergner showed measurements of 4mm pitch connectors showing the need to relax RF parameters to accommodate for 4mm pitch, see:
http://www.ieee802.org/3/cg/public/July2017/DiBiao_Bergner_01a_0717.pdf
- Another set of measurements you can find under:
http://www.ieee802.org/3/bw/public/buntz_tazebay_3bw_01_0914.pdf
- Supplementing data from re-use of available “old” measurement data from RTPGE (measurement of a 100ohms FlexRay link out of a real automotive cable harness) to confirm this.
- Derive a possible set of parameters for the automotive P2P link segment
- **This presentation does only focus on the Point-2-Point link segment. However, we believe the analysis applies to the passive linear multidrop link as well. This needs to be confirmed.**

Part 1

- Re-visit of supplementing measurement data from [http://www.ieee802.org/3/bw/public/buntz tazebay 3bw 01 0914.pdf](http://www.ieee802.org/3/bw/public/buntz_tazebay_3bw_01_0914.pdf)

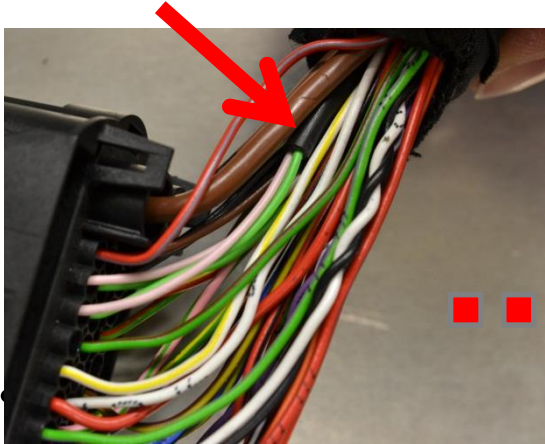
Device under test/measurement setup

- 2x0,35mm² 100 ohm jacketed cable in harness (approx. 3600mm) with inline connector (FlexRay).

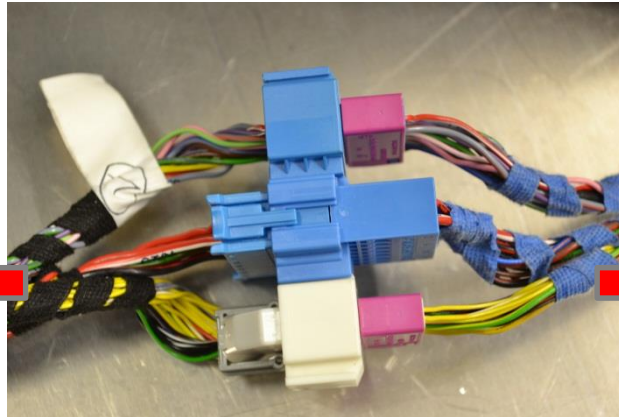


Device under test/measurement setup

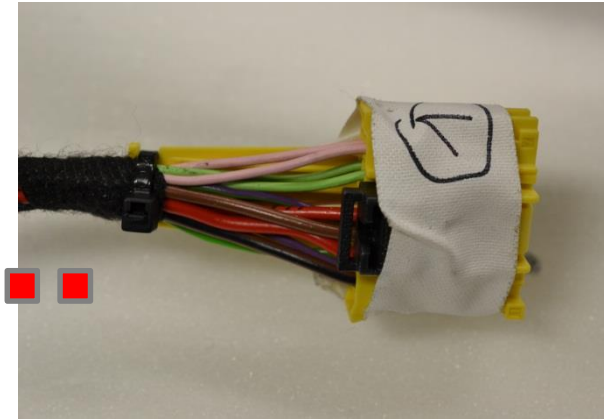
Connector1/jacketed cable



inline



Connector2



Test adapter

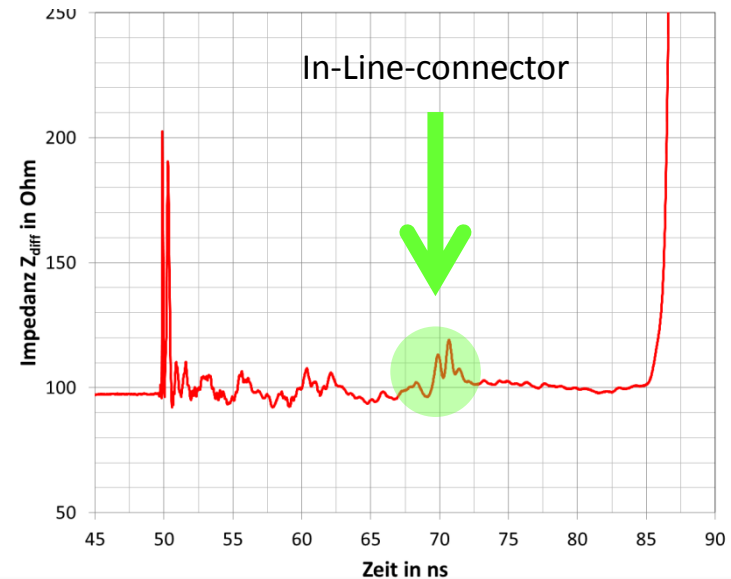
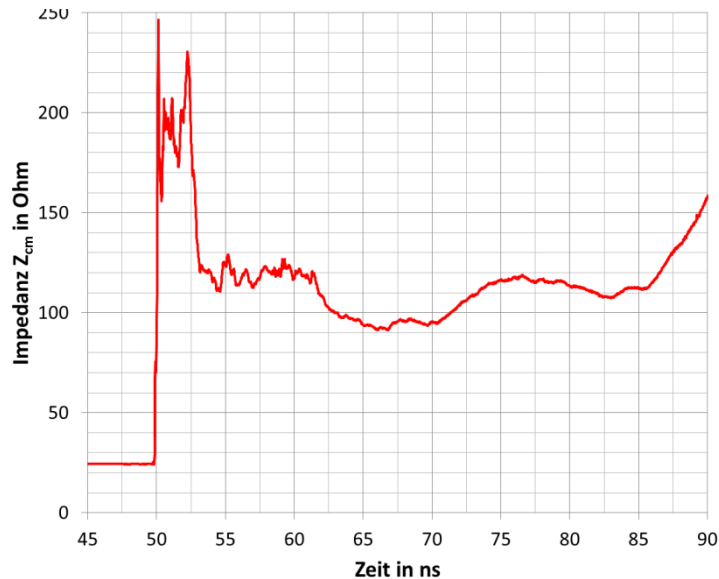
(as these were older measurements the test adapter is maybe not perfect...)

- Direct connection to GND plane.
- SMA heads soldered to Pins which are plugged into harness header.
- Complete harness on GND plane.
- No special treating of harness and assemblies to achieve high symmetry



TDR results Z_{cm} and Z_{diff}

- as harness is placed 50mm above GND plane Z_{CM} is nearly constant

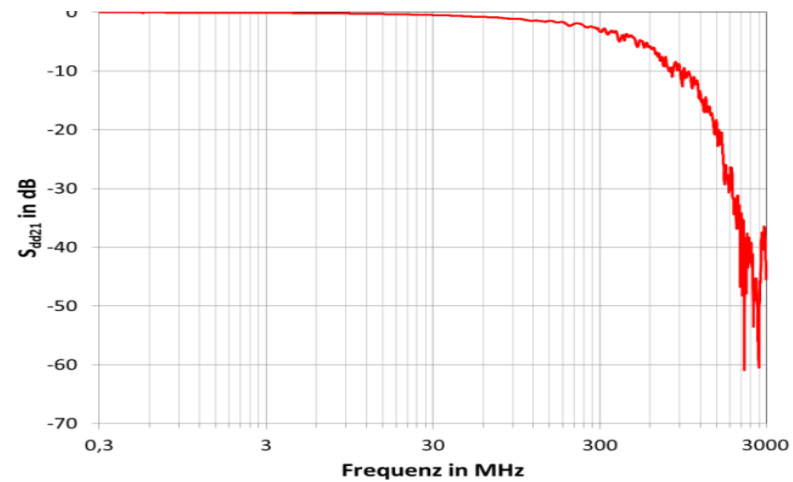
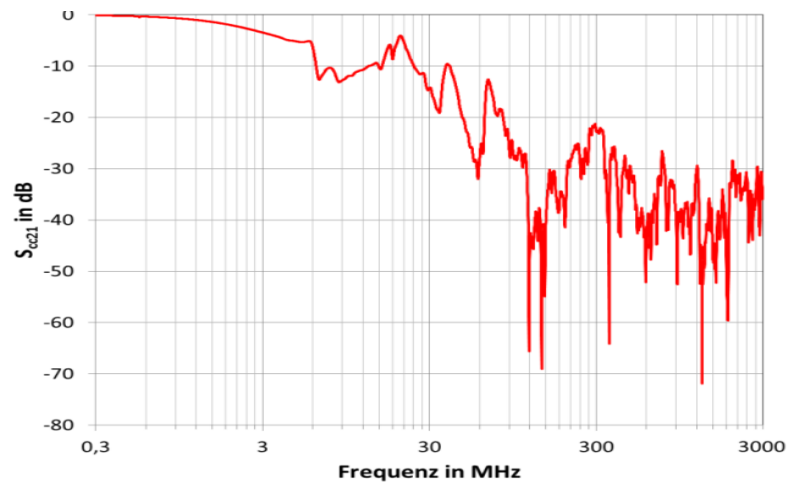
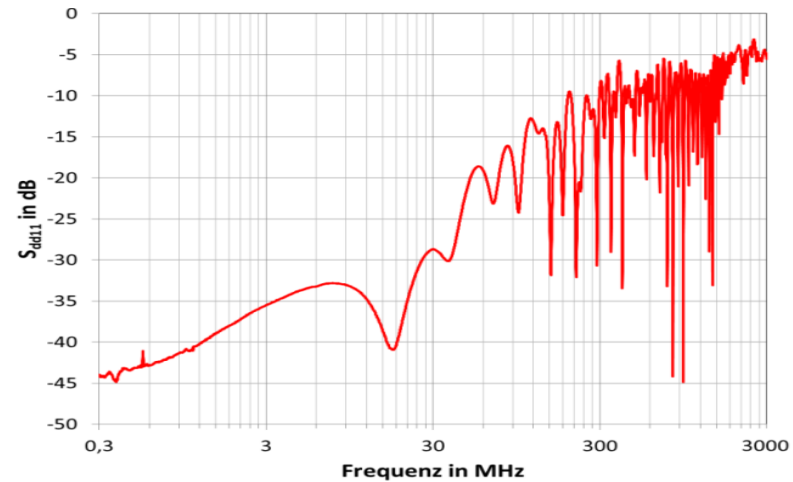
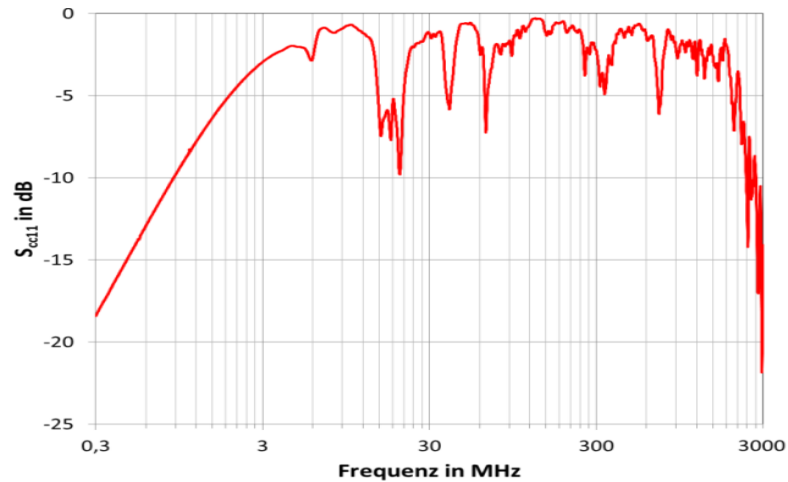


Z_{DM} may vary from 80ohms to 120ohms.
→ according RL influence to consider.

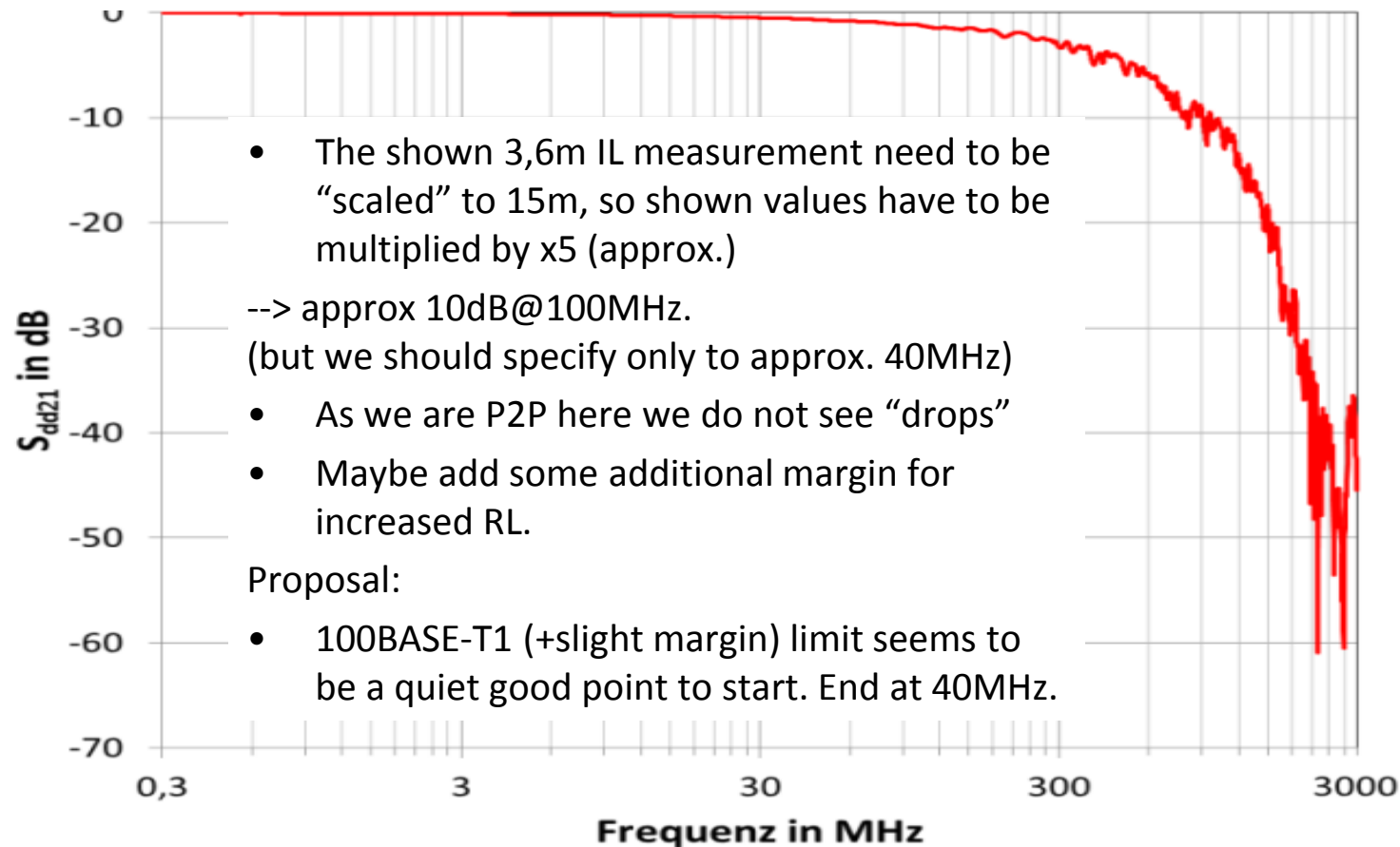
$$RL = 20 * \log_{10} \left(\left| \frac{Z_2 - Z_1}{Z_2 + Z_1} \right| \right)$$

RL = 14dB (from DC)

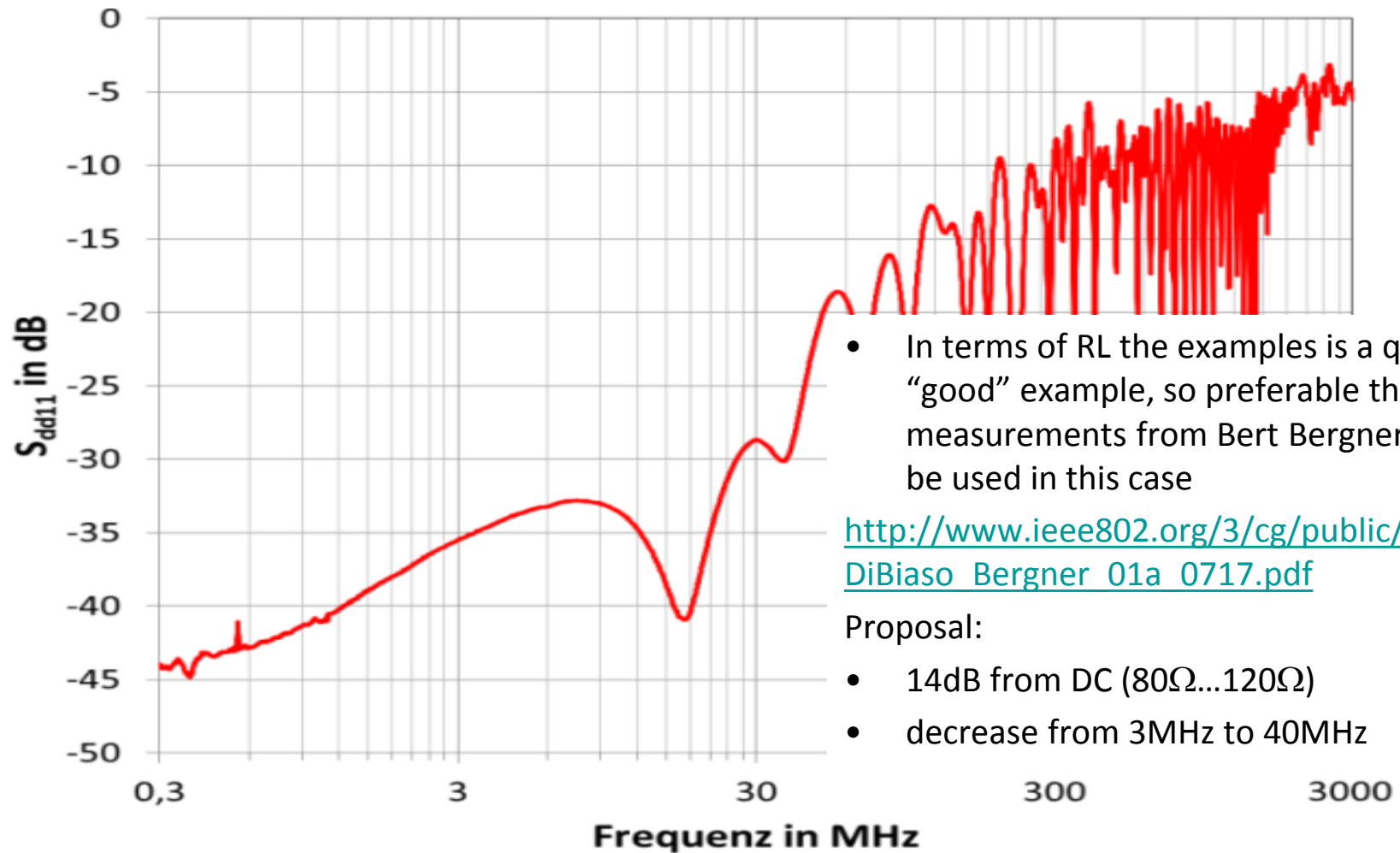
S_{cc11} , S_{dd11} , S_{cc21} , S_{dd21}



S_{dd21} (IL)



S_{dd11} (RL)



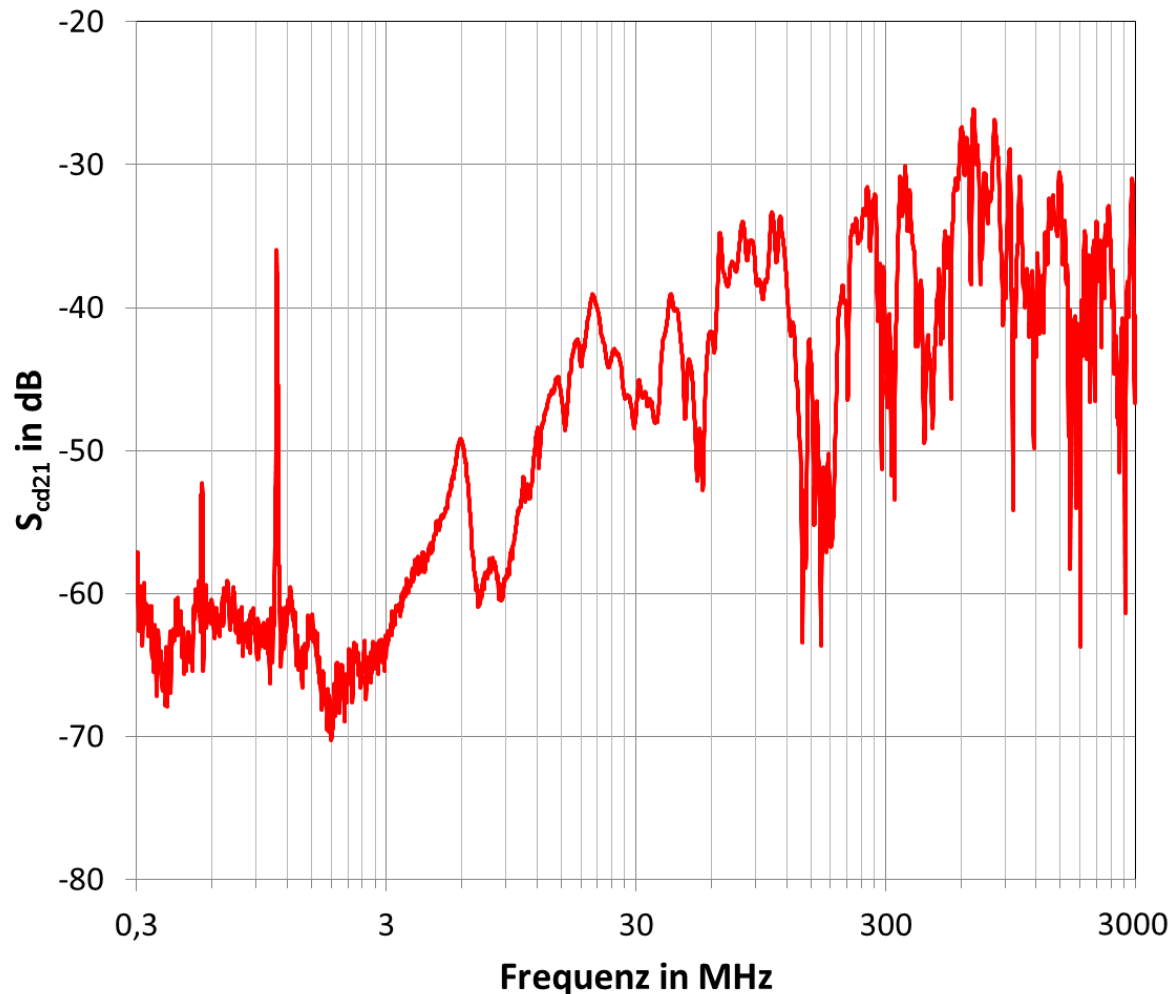
- In terms of RL the examples is a quiet “good” example, so preferable the RL measurements from Bert Bergner should be used in this case

http://www.ieee802.org/3/cg/public/July2017/DiBiao_Bergner_01a_0717.pdf

Proposal:

- 14dB from DC (80Ω...120Ω)
- decrease from 3MHz to 40MHz

S_{cd21} (TCTL)



- This is just an example, mode conversion may not be worst case.
- Bert Bergners measurement have to be taken into account as well.

Proposal

- **30dB up 20MHz seems to give some reasonable margin.**
- **Above 20MHz decrease of MC is expected**

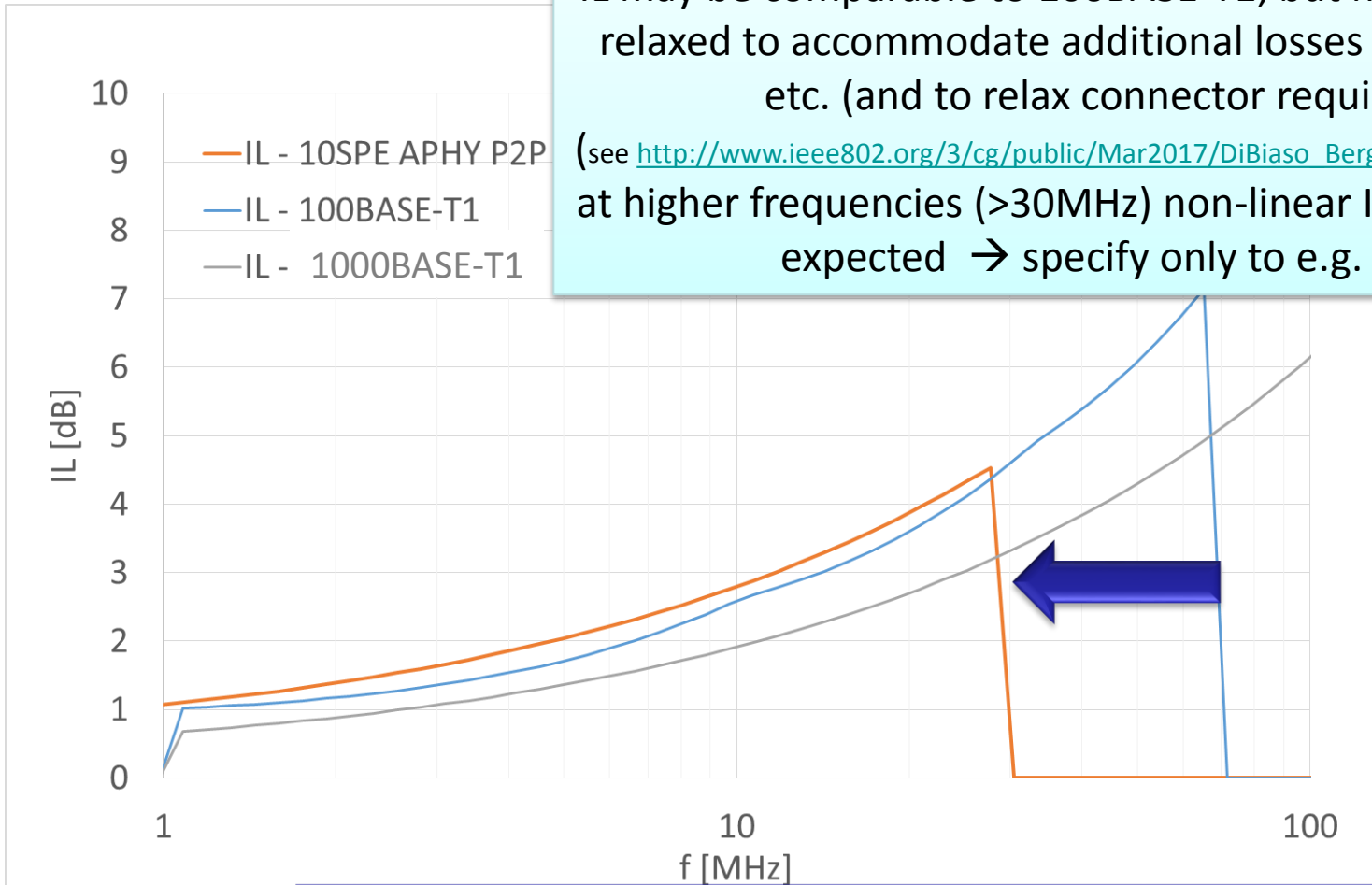
Part 2

- proposal for automotive P2P link segment
- (always with comparison to 100BASE-T1/1000BASE-T1)

Look on RF parameter – comparison to 100BASE-T1/1000BASE-T1

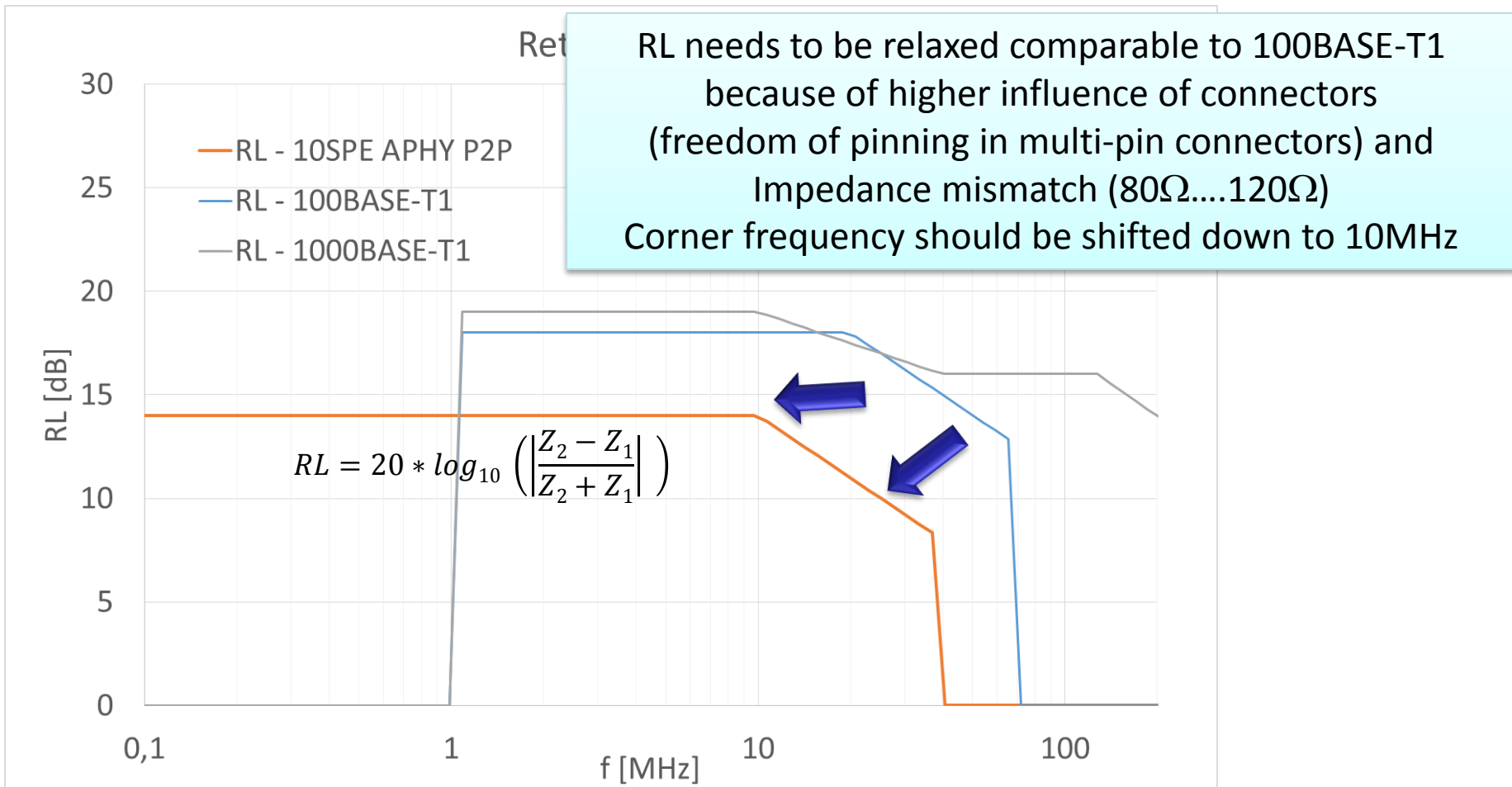
IL may be comparable to 100BASE-T1; but needs to be slightly relaxed to accommodate additional losses due to higher RL, etc. (and to relax connector requirement)

(see http://www.ieee802.org/3/cg/public/Mar2017/DiBiao_Bergner_01a_0314.pdf, slide 3)
at higher frequencies (>30MHz) non-linear IL behavior may be expected → specify only to e.g. 40MHz

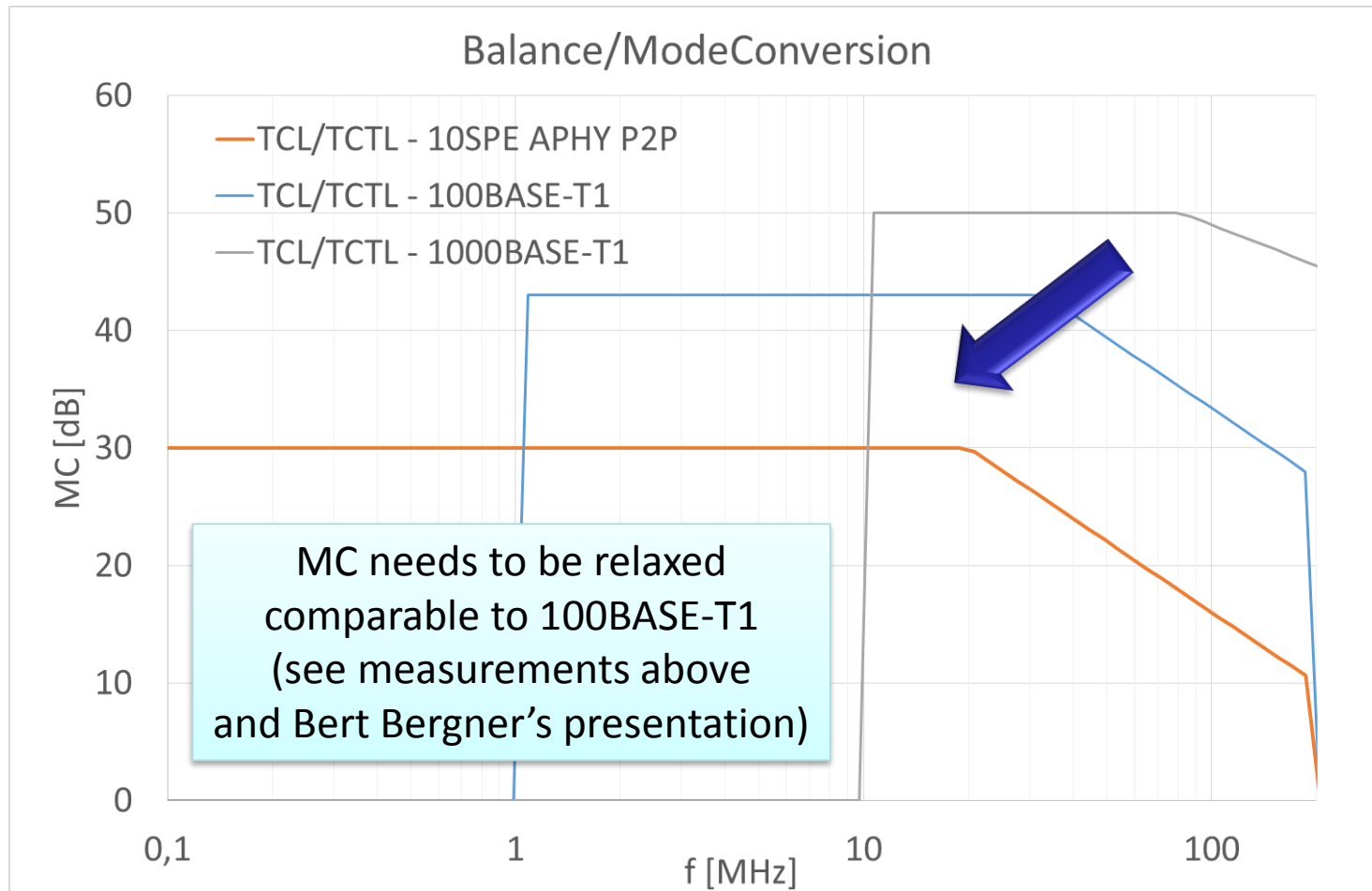


$$IL = 0,2 + 0,004*f + 0,8*SQRT(f) + 0,07*(1/SQRT(f)) \quad f=0,1...40MHz$$

Look on RF parameter – comparison to 100BASE-T1/1000BASE-T1



Look on RF parameter – comparison to 100BASE-T1/1000BASE-T1



MC =	30	f=0,1...20MHz
	$30-20*\text{LOG}_{10}(f/30)$	f=20...200MHz

Modeling of diagrams

For information here the used formulas for the shown diagrams for a potential 10SPE automotive PHY P2P link segment:

$$IL = 0,2 + 0,004 * f + 0,8 * \text{SQRT}(f) + 0,07 * (1/\text{SQRT}(f))$$

$$f = 0,1 \dots 40 \text{MHz}^*$$

$$RL = 14 \quad f = 0,1 \dots 3 \text{MHz}$$

*coefficients are derived from
matching to 100BASE-T1 curve

$$14 - 10 * \text{LOG}_{10}(f/3) \quad f = 3 \dots 40 \text{MHz}$$

$$MC = 30 \quad f = 0,1 \dots 20 \text{MHz}$$

$$30 - 20 * \text{LOG}_{10}(f/30) \quad f = 20 \dots 200 \text{MHz}$$

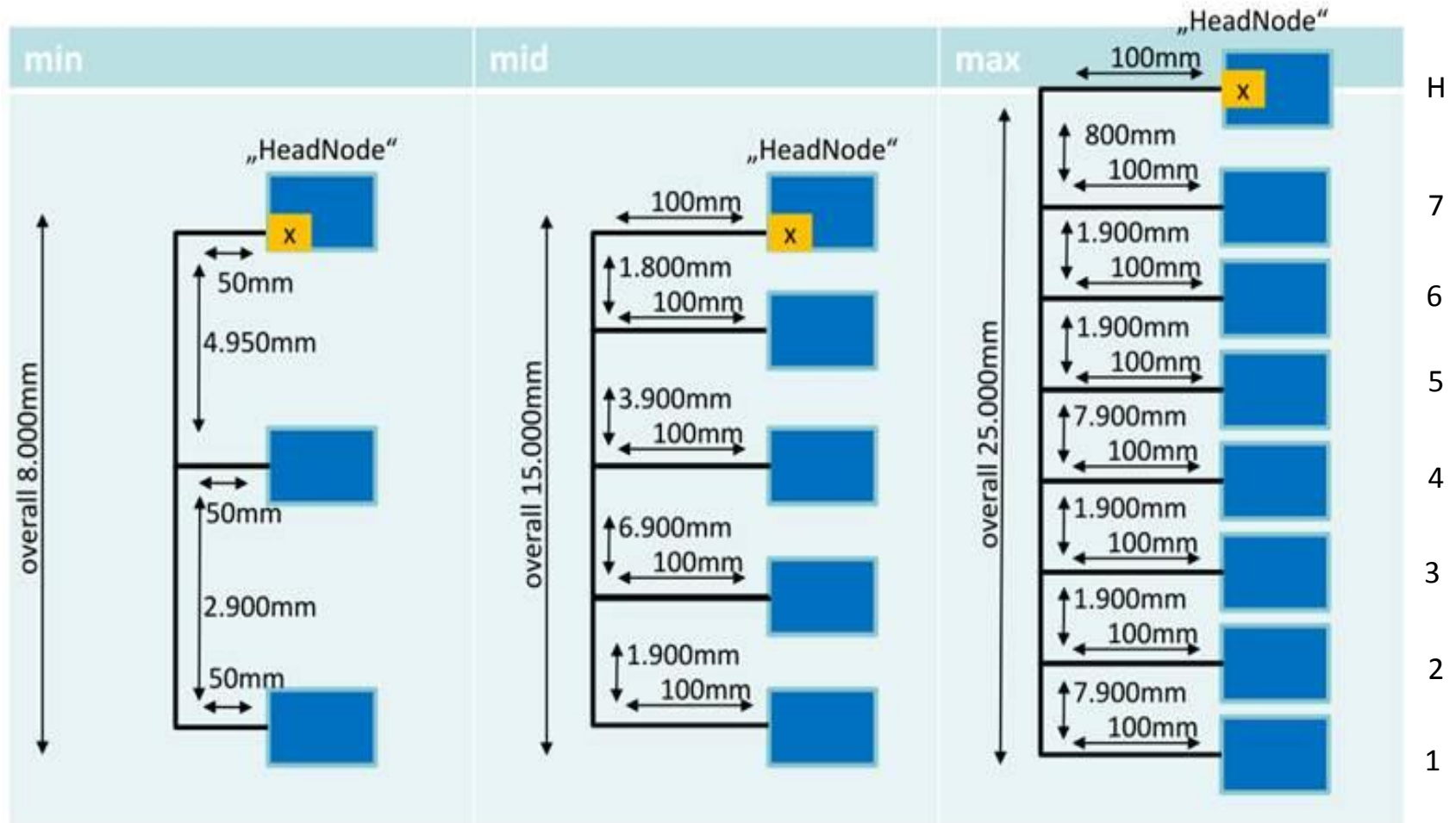
In addition, impedances of $Z_{DM} = 80 \dots 120 \text{ohms}$ are seen (this may not match to RL now...)

remark: MC = ModeConversion (in-pair) and CrossConversion (between pairs)

Part 3

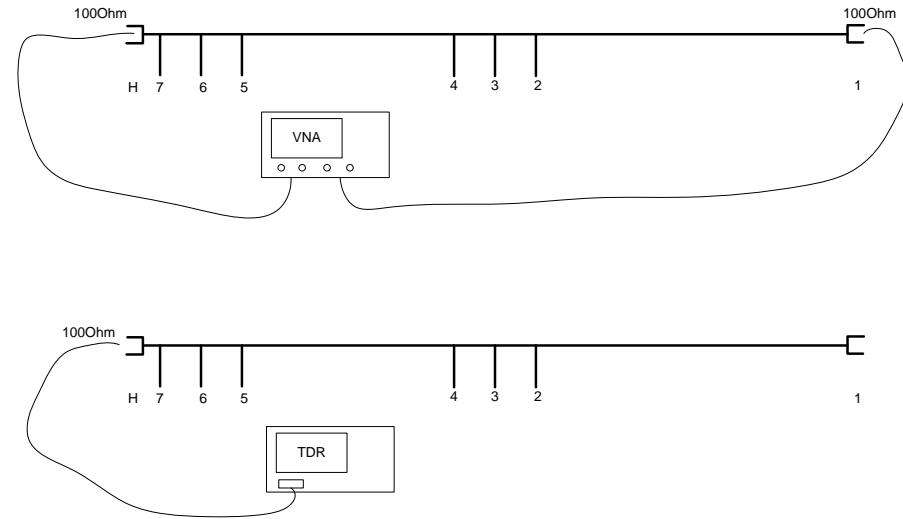
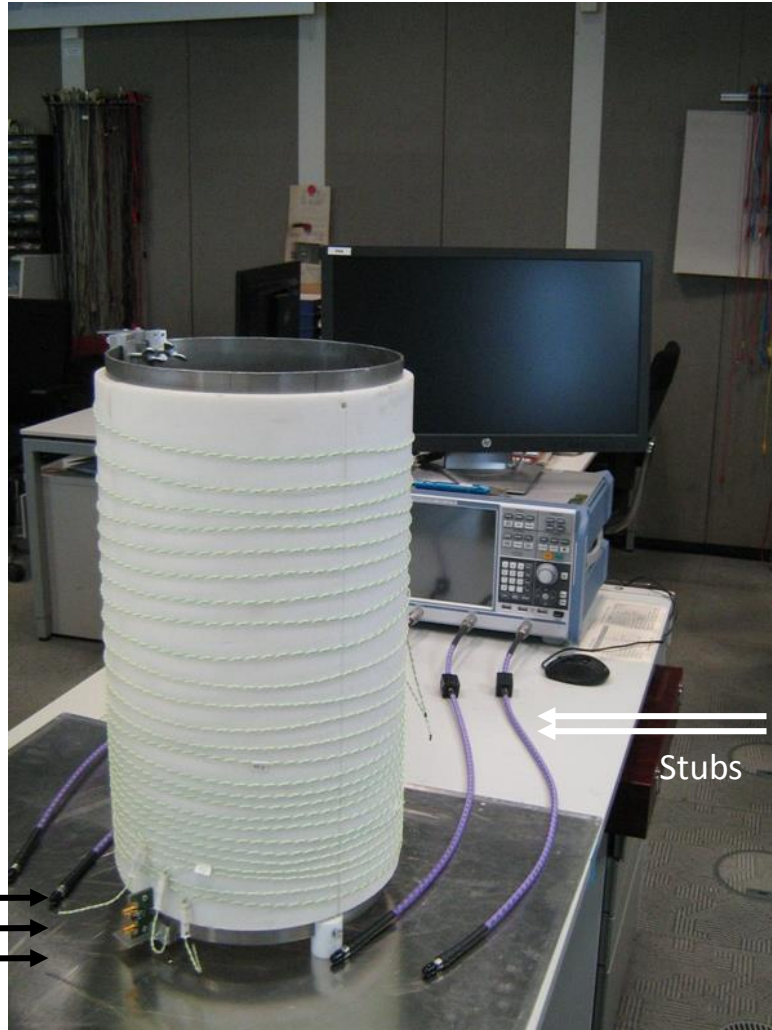
- Channel measurement for 10SPE Multidrop

Passive linear topologies

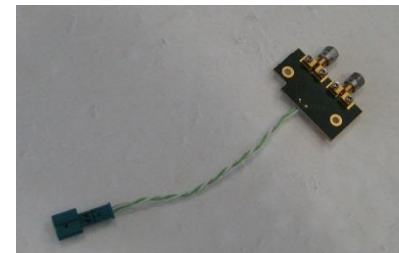


Max Topology Test

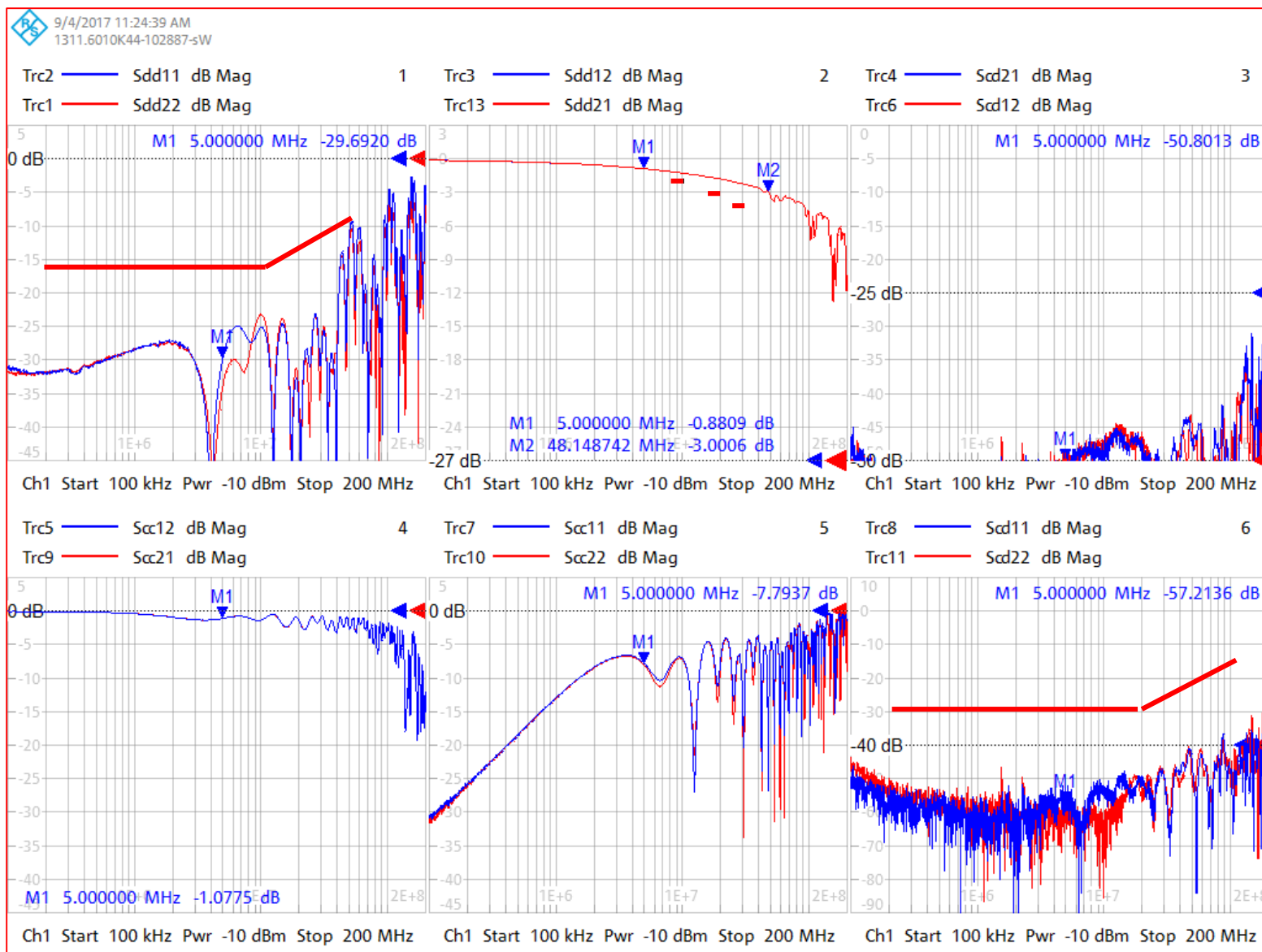
With TDR
With VNA



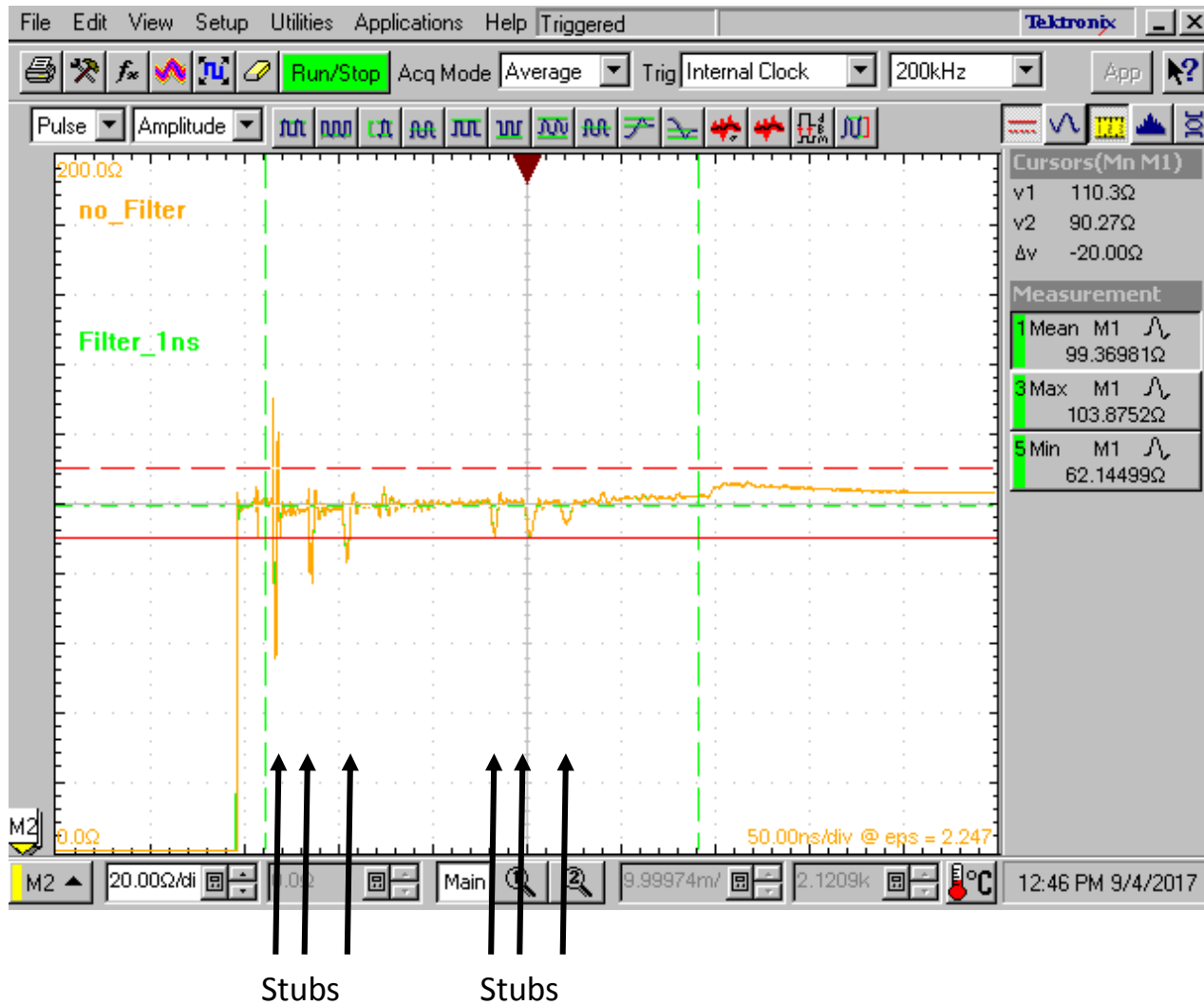
Used Termination at Stubs



Measurement over complete channel node H –node 1

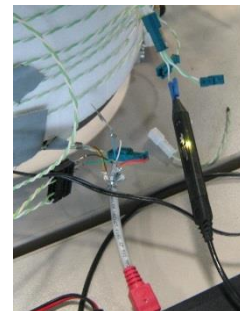
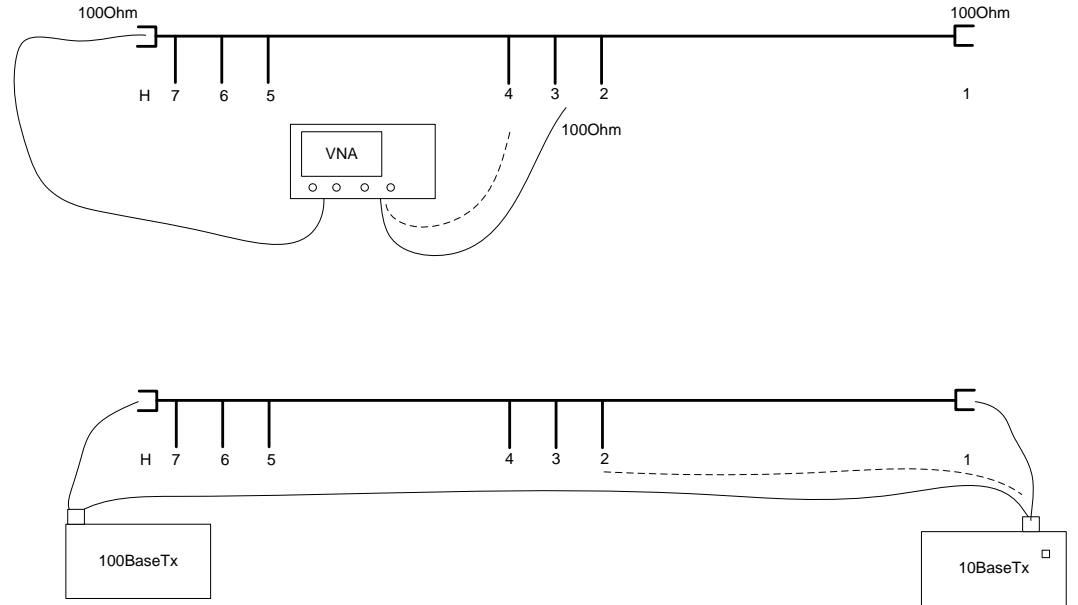
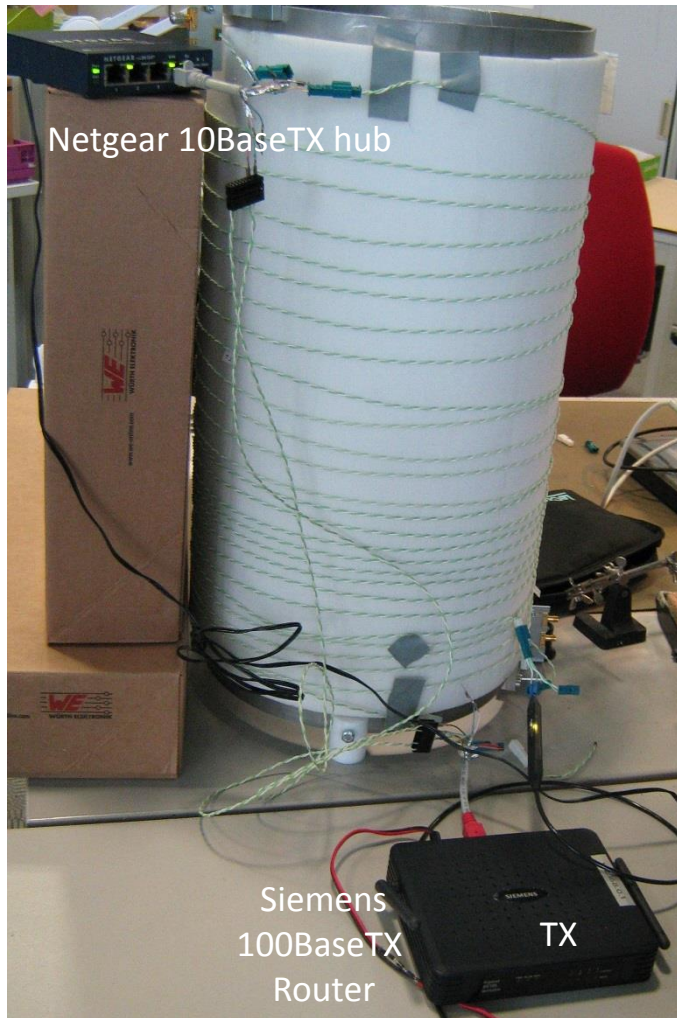


Measurement over complete channel node H



Max Topology Test

With TDR
With 10BaseTX



Scope Access at Stub

Measurement over node H –node 2 node 1 terminated



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Trc2 — Sdd11 dB Mag

1

Trc3 — Sdd12 dB Mag

2

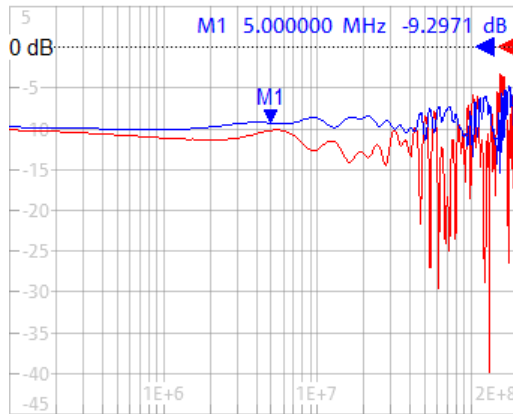
Trc4 — Sdd21 dB Mag

3

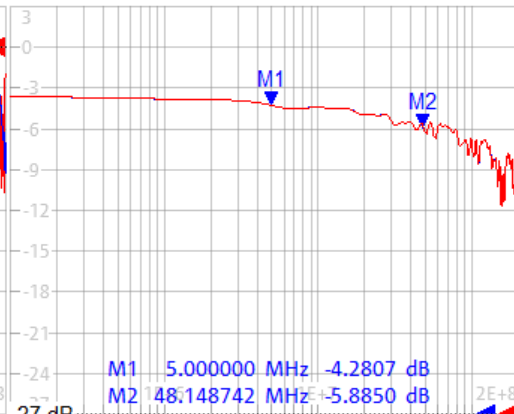
Trc1 — Sdd22 dB Mag

Trc13 — Sdd21 dB Mag

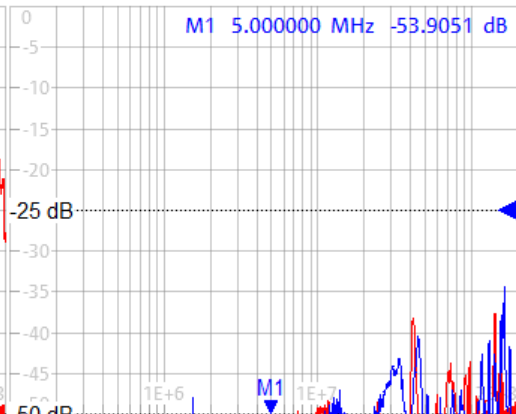
Trc6 — Sdd12 dB Mag



Ch1 Start 100 kHz Pwr -10 dBm Stop 200 MHz



Ch1 Start 100 kHz Pwr -10 dBm Stop 200 MHz



Ch1 Start 100 kHz Pwr -10 dBm Stop 200 MHz

Trc5 — Scc12 dB Mag

4

Trc7 — Scc11 dB Mag

5

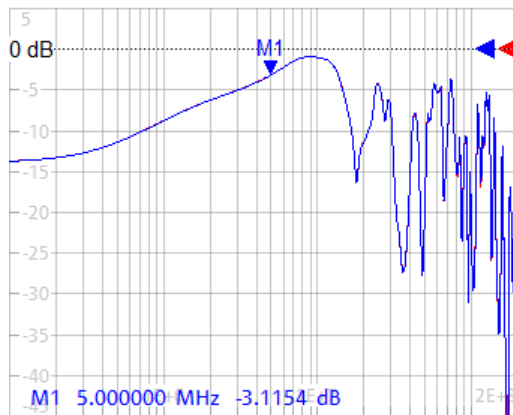
Trc8 — Scc11 dB Mag

6

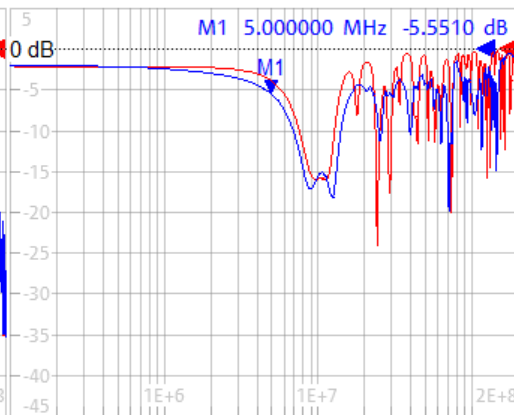
Trc9 — Scc21 dB Mag

Trc10 — Scc22 dB Mag

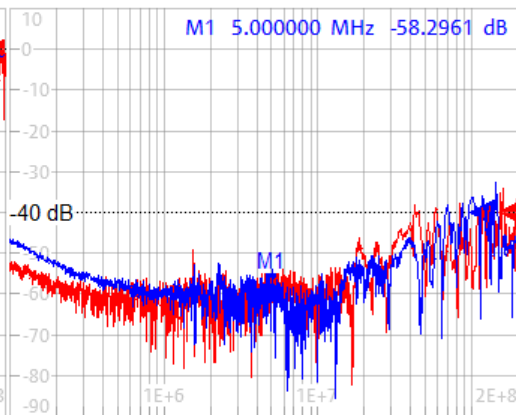
Trc11 — Scc22 dB Mag



Ch1 Start 100 kHz Pwr -10 dBm Stop 200 MHz



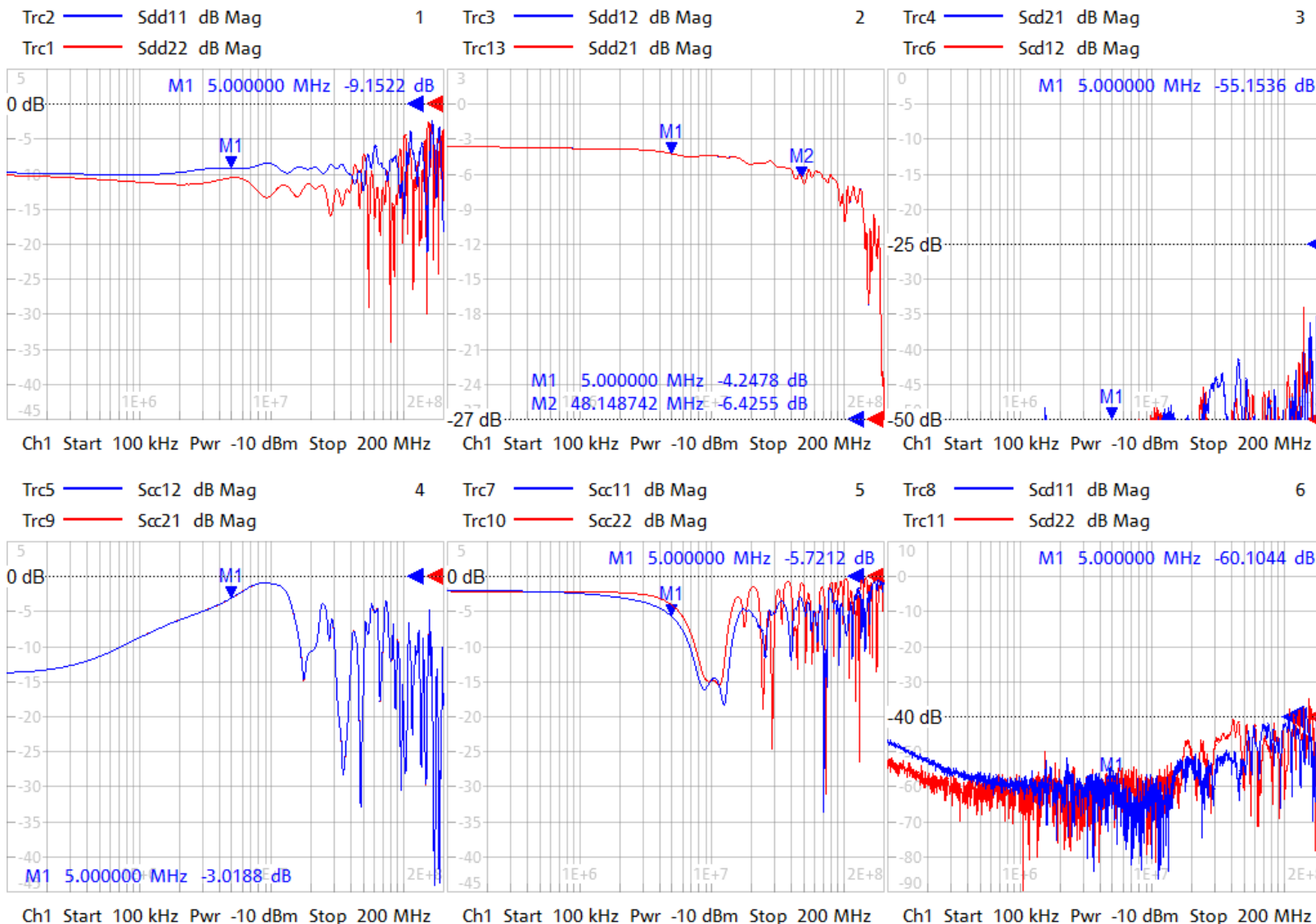
Ch1 Start 100 kHz Pwr -10 dBm Stop 200 MHz



Ch1 Start 100 kHz Pwr -10 dBm Stop 200 MHz

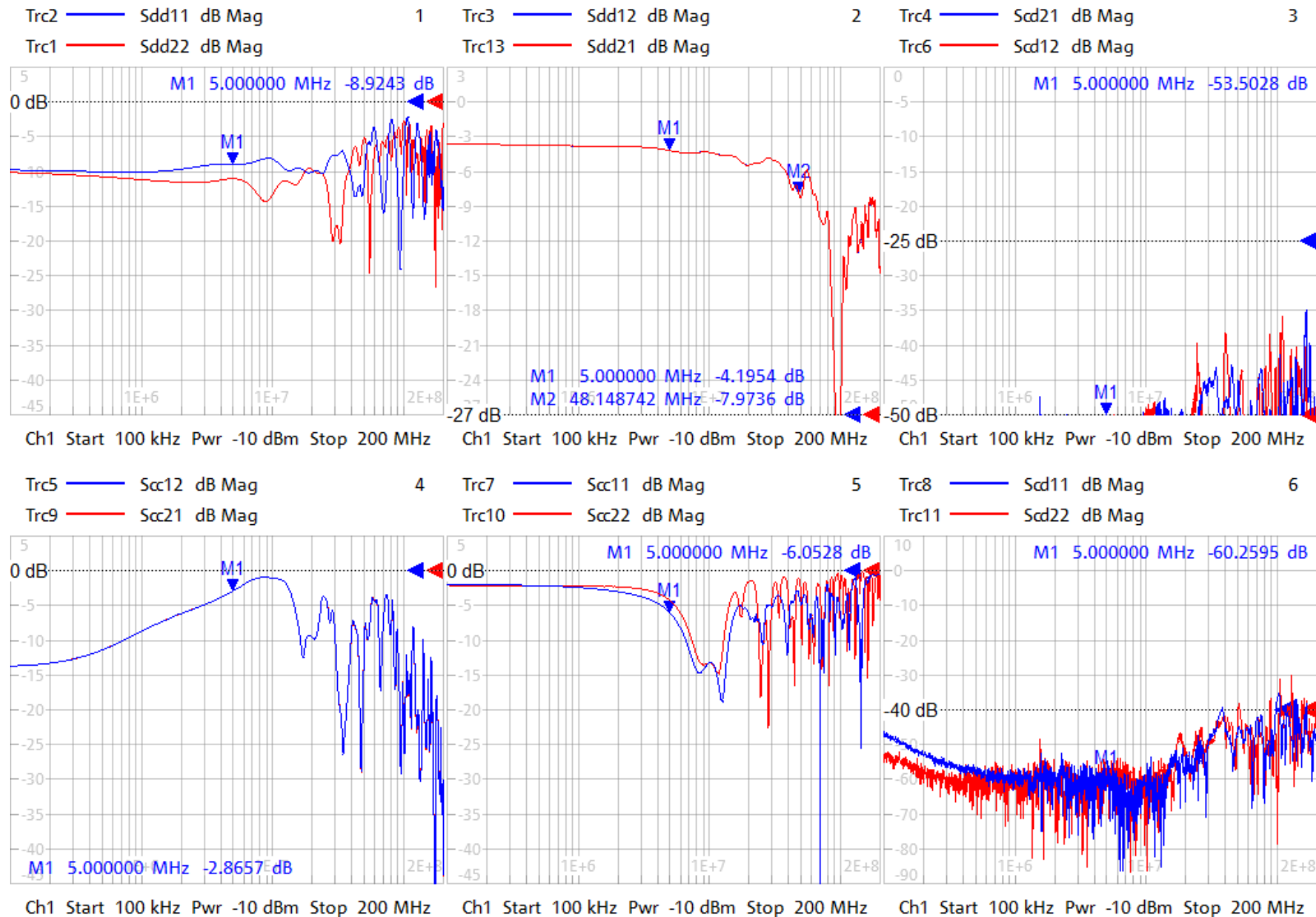
Measurement node H –node 2 node 4 Stub 20cm node 1 terminated

9/5/2017 9:00:27 AM
1311.6010K44-102887-sW



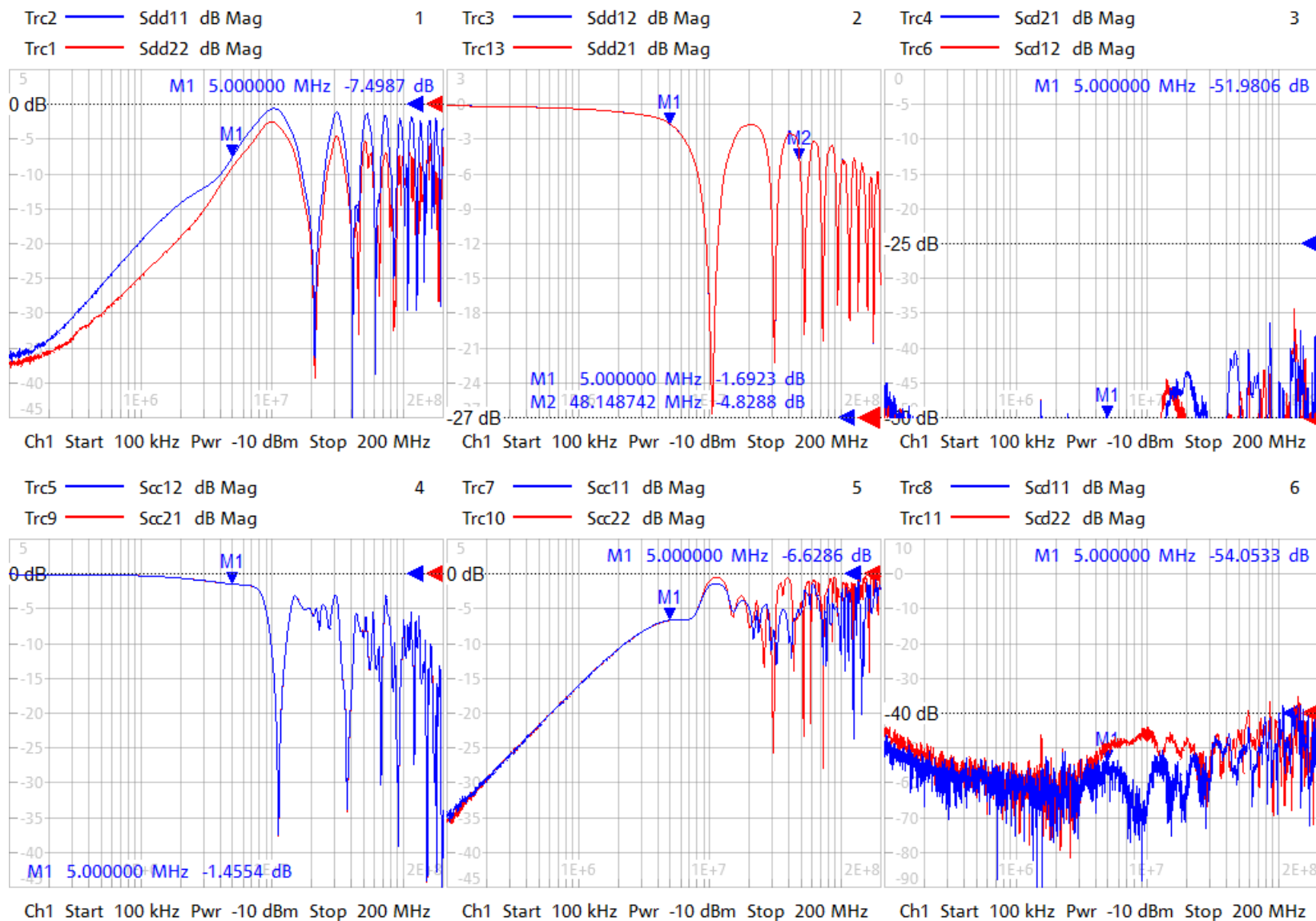
Measurement over complete channel node H –node 2 node 4 Stub 50cm node 1 terminated

9/5/2017 8:58:38 AM
1311.6010K44-102887-sW

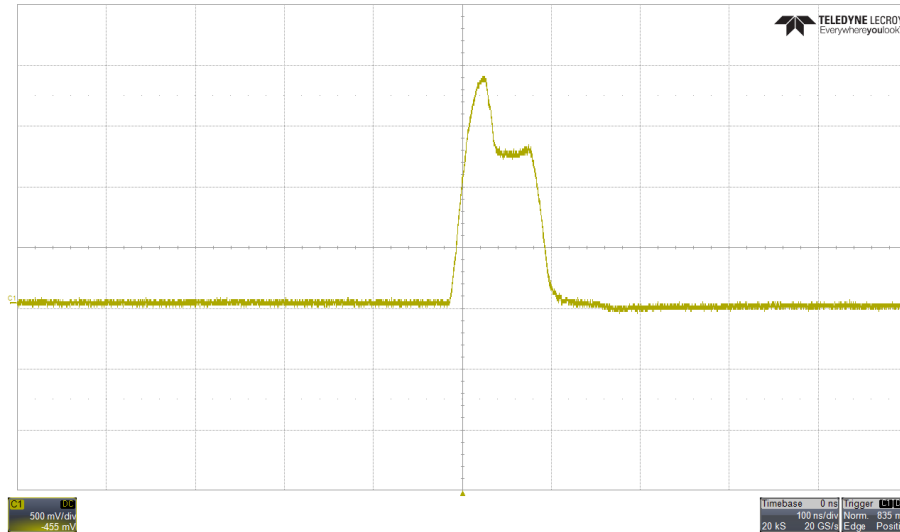


Measurement over complete channel node 5 –node 2 node 1 termination at H open

9/5/2017 8:34:06 AM
1311.6010K44-102887-sW



Test 10MB



Pulseform @ Netgear
Over Node H—Node 1

observed:

- Even attaching the TX Devices in the middle of the topology and adding a termination at the end
Only the amplitude was mainly influenced;
Not a massive increase of „noise“ echo's etc,
- Most critical: removing the termination at one of the topology end:
- Massive Echo occur.

Conclusion

- The influence of the vehicle environment can not be neglected.
- Additional measurements of different OEMs and different connector/cable systems (which maybe are intended to be used for 10SPE automotive PHY) within a cable harness or a vehicle would be greatly appreciated to provide a better data basis.
- **Based on the available data a baseline proposal could be made next meeting cycle**
 - ➔ **The baseline proposal for the channel seem valid for Multipoint (as far as we can setup a reasonable test)**
 - ➔ **Standard VNA, TDR tests have only limited value**
 - ➔ **.**
 - 1. This proposal is for the Point-2-Point link segment. We expect that it is suitable also for the passive linear link.
 - 2. These inputs are intended to support semiconductor manufacturers in their investigations, if this indeed the case

Found during tests:

- ➔ **The length of stub and the termination at the end have major impact.**
- ➔ **10..20cm stubs seem o.k.**