## FEC/Framing/Modulation for 10GBASE-T1 PHY

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## Decision Factors for Selection of 10G PHY proposals

- We've focused so far on modulation only, but modulation doesn't make the whole PHY
- The top factor in modulation selection is the target performance feasibility
- Do the selected modulations deliver the target performance (Data rate \& BER) over the target medium?
- Presentations from May 2018 show 2 and 2.5b/symbol give best performance
- Simulations show similar SNR performance between PAM proposals
- PAM-4 best for in-band NBI and impulse immunity in this range: (Tu, Pandey, Souvegnier agree)
- We've seen this before: < 1 dB differences lie in implementation, mapping to framing \& coding
- Next decision factors power \& cost:
- Modulations proposed have similar complexity - everyone has a favorite for different reasons
- None are saying the differences are large
- Re-use of existing Ethernet technology impacts power \& cost as well
- This presentation discusses an approach to Framing \& Coding relative to noise and modulation


## PAM modulations are close in performance

10G PHY: Salz SNR Analysis - 15m Cable

| 15m Cable | PAM2 | PAM3 | PAM4 | PAM5 | PAM6 | PAM8 | PAM16 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Baud Rate (GBaud) | 11.2 | 7.5 | 5.6 | 5.0 | 4.5 | 3.7 | 2.8 |
| Nyquist Freq. (GHz) | 5.6 | 3.75 | 2.8 | 2.5 | 2.2 | 1.8 | 1.4 |
| IL@Nyquist (dB) | 46.9 | 35.7 | 29.7 | 27.5 | 25.7 | 22.9 | 19.3 |
| RL@Nyquist (dB) | 12.0 | 12.0 | 12.5 | 13.0 | 13.5 | 14.2 | 15.3 |
| Ideal SNR Margin (dB) | 14.3 | 18.5 | 19.3 | 19.1 | 18.6 | 17.5 | 13.7 |
| Echo cancellation (dB) | 17.0 | 24.3 | 26.9 | 28.2 | 28.8 | 29.5 | 30.0 |

## Pandey_3ch_01c_0518.pdf

SNR Margin to Uncoded SER

| Modulation | Bits/Sym | Symbol <br> Rate <br> (MBaud) | Uncoded <br> SNR @1e-12 <br> SER (dB) | Cat8 Salz <br> SNR (dB) | Cat7a <br> Salz SNR <br> (dB) | Cat8 <br> Margin <br> (dB) | Cat7a <br> Margin (dB) |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3B2T | $3 / 2$ | 7500 | 21.8 | 30.3 | 24.4 | 8.5 | 2.6 |
| DSQ-8 | $3 / 2$ | 7500 | 21.1 | 30.3 | 24.4 | 9.2 | 3.3 |
| PAM-4 | $2 / 1$ | 5625 | 24.0 | 34.6 | 29.1 | 10.6 | 5.1 |
| 32-Cross | $5 / 2$ | 4500 | 27.1 | 37.5 | 32.3 | 10.4 | 5.2 |
| DSQ-32 | $5 / 2$ | 4500 | 27.3 | 37.5 | 32.3 | 10.2 | 5.0 |
| PAM-8 | $3 / 1$ | 3750 | 30.4 | 39.6 | 34.6 | 9.2 | 4.2 |
| DSQ-128 | $7 / 2$ | 3200 | 33.4 | 41.3 | 36.5 | 7.9 | 3.1 |

Souvignier_3ch_01c_0518.pdf

Effect of ADC Power vs. ENOB on 10Gbps SNR Margin


- Presentations from multiple PHY vendors agree, SNR analyses for PAM4, DSQ or Cross 32 and PAM5 are well within 1dB of each other.
- Implementation losses will dominate
- Higher density constellations are more vulnerable to RF interference and implementation noise contributions


## Automotive Error Sources

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tu_3ch_01b_0518.pdf
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- Narrowband RF Interference
- Single tones: 1 MHz - 5 GHz at 100V/m (ISO 11452-2)
- Alien crosstalk/channel AWGN
- Negligible, dominated by receiver noise

NBI Immunity Simulation Results



- At lower frequencies, NBI immunity increased by $\sim 2.5 \mathrm{~dB}$ each from PAM8 to 32 -Cross to PAM4 At higher frequencies, denser constellations have superior immunity due to lower bandwidth and
analog low pass filtering IEEE 802 3ch Task Force- May 20

Chini_Tazebay_3bp_01a_0114.pdf
Transient Noise Model at Receiver


One cycle of a 20 MHz sinusoidal signal with magnitude of 100 mV is suggested for system analysis of transient noises

## Narrowband RF Interference

## - RF Interference Coupling to Differential Pairs

- BCI 1MHz - 400MHz (ISO11452-2/ OEM specs)
- BCI used to cover lower frequencies
- ALSE 80MHz - 5GHz (ISO11452-2/ OEM specs)
- Use actual antenna radiating an electric field at the cable
- ISO spec defines an electric field up to $100 \mathrm{~V} / \mathrm{m}$ at the cable
- Several worst-case frequencies within $1 \mathrm{MHz}-5 \mathrm{GHz}$ selected for analysis

Table C. 1 - Suggested test severity levels

| Test severity level | Value <br> $\mathrm{V} / \mathrm{m}$ |
| :---: | :---: |
| I | 25 |
| II | 50 |
| III | 75 |
| IV | 100 |
| V | Specific value agreed between the users of this <br> part of ISO 11452, if necessary |

Table C. 2 - Frequency bands

| Frequency band | Frequency range <br> MHz |
| :---: | :---: |
| F1 | $>80$ to $\leqslant 400$ |
| F2 | $>400$ to $\leqslant 1000$ |
| F3 | $>1000$ to $\leqslant 10000$ |
| F4 | $>10000$ to $\leqslant 18000$ |

## ALSE RFI Measurements for STP cable with H-MTD



Scaled to ALSE Field Strength $=100$ Volts/Meter, Corrected for Test Fixture Loss


## RFI Induced Differential Voltage at PHY Input



- The limit line used for the differential voltage magnitude at the PHY input induced by the RF fields coupled to the STP cable, which was used for the analysis

RF.Coupled.Input.Diff $\leq 4.5 \mathrm{mV}_{\mathrm{RMS}}\left(6.0 \mathrm{mV}_{\mathrm{Pk}}\right)$

## Burst Error Source

## - Transient Impulse (ISO 7637-3)

- Caused by Engine spark plus, etc
- Triangular impulse: Duration < 50nsec, Freq. < 10KHz
- Coupled magnitude estimated based on 1000BASE-T1
- Took into account the coupling attenuation difference between STP and UTP (Conservatively assumed 10dB delta)


## 


Cable Coupling Attenuation ISO + TIA




## Burst Error Source

## - Transient Impulse

- Triangular impulse: Duration < 50nsec, Freq. $<10 \mathrm{KHz}$
- One impulse affects several symbols in a row
- Example in 10Gbps PAM4
- Can corrupt up to 280 symbols in 10Gbps PAM4
- Can lead to BER ~1E-4 without FEC
- The shorter the symbol period, the higher the number of affected symbols

- The higher the PAM levels, the higher susceptibility the symbols get corrupted


## FEC Design Considerations

- Two major source of noise in automotive are
- Large RFI Noise $\rightarrow$ Need to heavy DFE instead of linear equalization $\rightarrow$ Large burst error
- Large Transient Impulses $\rightarrow$ Large burst errors
- Above considerations makes Reed-Solomon a right choice for FEC coding
- Reed Solomon Codes: RS(N, M, K) $\rightarrow$ Each RS-Symbol consists of K bits
- Frame $=N \times K$ bits $\left(N<2^{K}\right)$, Data $=M \times K$ bits
- Coding Overhead $=(N-M) / M \rightarrow$ Corrects $=(N-M) / 2$ RS-Symbols
- To stay error free $\rightarrow$ RS Symbol Error Rate < (N-M)/2M
- Improving FEC Error Correction Performance
- Higher coding overhead helps reduce all error types: Random, Burst, RFI,
- Higher correction per frame $\rightarrow$ Higher coding overhead $\rightarrow$ Higher baud rate!
- Code Interleaving further help with Burst errors $\rightarrow$ Increases latency


## Basic Ethernet PCS structure (post-Gigabit Era)

- Take XGMII interface
- Data and control words
- Transcode to new, blocked bit stream
- 64/66b, 64/65b, 256/257b, 512/513b...
- Add FEC on top of blocking
- Map to PAM levels
- Match block rates to use recovered efficiency to include FEC and match clock rates to be easily generated
- Lots of work going on in 802.3 for PAM-4 - we can look to other groups to borrow


## Basic Idea: 64B66 Compression

- The 01/10 frame marker used in 64B66 was driven by the noise model of the 10GBASE-R optical channel which was dominated by shot noise, and by the still reasonable 33/32 speed-up allowing a single PLL implementation of the CDR
- The 64/66B PCS of 10GBASE-R only uses 15 block field types to transport all of the Start-of-Frame, End-of-Frame, and Ordered Set information
- Result is that there are ways to compress this PCS, as burning 2-bits in 66 to convey this information is not very efficient

| Input Data |  | Block Payload |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Bit Position <br> Data Block Format: | 01 | 2 ( 65 |  |  |  |  |  |  |  |  |
| $\mathrm{D}_{0} \mathrm{D}_{1} \mathrm{D}_{2} \mathrm{D}_{3} / \mathrm{C}_{4} \mathrm{D}_{5} \mathrm{D}_{6} \mathrm{D}_{7}$ | 01 | Do | $\mathrm{D}_{1}$ | $\mathrm{D}_{2}$ | $\mathrm{D}_{3}$ |  |  | $\mathrm{D}_{5}$ | $\mathrm{D}_{6}$ | $\mathrm{D}_{7}$ |
| Control Block Formats: |  | Block Type Field |  |  |  |  |  |  |  |  |
| $\mathrm{C}_{0} \mathrm{C}_{1} \mathrm{C}_{2} \mathrm{C}_{3} / C_{4} \mathrm{C}_{5} \mathrm{C}_{6} \mathrm{C}_{7}$ | 10 | 0x1e | $\mathrm{C}_{0}$ | $\mathrm{C}_{1}$ | $\mathrm{C}_{2}$ | $\mathrm{C}_{3}$ | $\mathrm{C}_{4}$ | $\mathrm{C}_{5}$ | $\mathrm{C}_{6}$ | $\mathrm{C}_{7}$ |
| $\mathrm{C}_{0} \mathrm{C}_{1} \mathrm{C}_{2} \mathrm{C}_{3} \mathrm{O}_{4} \mathrm{D}_{5} \mathrm{D}_{6} \mathrm{D}_{7}$ | 10 | 0x2d | $\mathrm{C}_{0}$ | $\mathrm{C}_{1}$ | $\mathrm{C}_{2}$ | $\mathrm{C}_{3}$ | $\mathrm{O}_{4}$ | $\mathrm{D}_{5}$ | $\mathrm{D}_{6}$ | $\mathrm{D}_{7}$ |
| $\mathrm{C}_{0} \mathrm{C}_{1} \mathrm{C}_{2} \mathrm{C}_{3} / \mathrm{S}_{4} \mathrm{D}_{5} \mathrm{D}_{6} \mathrm{D}_{7}$ | 10 | 0×33 | $\mathrm{c}_{0}$ | $\mathrm{C}_{1}$ | $\mathrm{C}_{2}$ | $\mathrm{C}_{3}$ |  | $\mathrm{D}_{5}$ | $\mathrm{D}_{6}$ | $\mathrm{D}_{7}$ |
| $\mathrm{O}_{0} \mathrm{D}_{1} \mathrm{D}_{2} \mathrm{D}_{3} / \mathrm{S}_{4} \mathrm{D}_{5} \mathrm{D}_{6} \mathrm{D}_{7}$ | 10 | 0x66 | $\mathrm{D}_{1}$ | $\mathrm{D}_{2}$ | $\mathrm{D}_{3}$ | $0_{0}$ |  | $\mathrm{D}_{5}$ | $\mathrm{D}_{6}$ | $\mathrm{D}_{7}$ |
| $\mathrm{O}_{0} \mathrm{D}_{1} \mathrm{D}_{2} \mathrm{D}_{3} / \mathrm{O}_{4} \mathrm{D}_{5} \mathrm{D}_{6} \mathrm{D}_{7}$ | 10 | 0x55 | $\mathrm{D}_{1}$ | $\mathrm{D}_{2}$ | $\mathrm{D}_{3}$ | $\mathrm{o}_{0}$ | $\mathrm{O}_{4}$ | $\mathrm{D}_{5}$ | $\mathrm{D}_{6}$ | $\mathrm{D}_{7}$ |
| $\mathrm{S}_{0} \mathrm{D}_{1} \mathrm{D}_{2} \mathrm{D}_{3} / \mathrm{D}_{4} \mathrm{D}_{5} \mathrm{D}_{6} \mathrm{D}_{7}$ | 10 | 0x78 | $\mathrm{D}_{1}$ | $\mathrm{D}_{2}$ | $\mathrm{D}_{3}$ |  |  | $\mathrm{D}_{5}$ | $\mathrm{D}_{6}$ | $\mathrm{D}_{7}$ |
| $\mathrm{O}_{0} \mathrm{D}_{1} \mathrm{D}_{2} \mathrm{D}_{3} / \mathrm{C}_{4} \mathrm{C}_{5} \mathrm{C}_{6} \mathrm{C}_{7}$ | 10 | 0x4b | $\mathrm{D}_{1}$ | $\mathrm{D}_{2}$ | $\mathrm{D}_{3}$ | $0_{0}$ | $\mathrm{C}_{4}$ | $\mathrm{C}_{5}$ | $\mathrm{C}_{6}$ | $\mathrm{c}_{7}$ |
| $\mathrm{T}_{0} \mathrm{C}_{1} \mathrm{C}_{2} \mathrm{C}_{3} / \mathrm{C}_{4} \mathrm{C}_{5} \mathrm{C}_{6} \mathrm{C}_{7}$ | 10 | $0 \times 87$ | \| | $\mathrm{C}_{1}$ | $\mathrm{C}_{2}$ | $\mathrm{C}_{3}$ | $\mathrm{C}_{4}$ | $\mathrm{C}_{5}$ | $\mathrm{C}_{6}$ | $\mathrm{c}_{7}$ |
| $\mathrm{D}_{0} \mathrm{~T}_{1} \mathrm{C}_{2} \mathrm{C}_{3} / \mathrm{C}_{4} \mathrm{C}_{5} \mathrm{C}_{6} \mathrm{C}_{7}$ | 10 | 0x99 | $\mathrm{D}_{0}$ | Il | $\mathrm{C}_{2}$ | $\mathrm{C}_{3}$ | $\mathrm{C}_{4}$ | $\mathrm{C}_{5}$ | $\mathrm{C}_{6}$ | $\mathrm{c}_{7}$ |
| $\mathrm{D}_{0} \mathrm{D}_{1} \mathrm{~T}_{2} \mathrm{C}_{3} \mathrm{C}_{4} \mathrm{C}_{5} \mathrm{C}_{6} \mathrm{C}_{7}$ | 10 | 0xaa | $\mathrm{D}_{0}$ | $\mathrm{D}_{1}$ |  | $\mathrm{C}_{3}$ | $\mathrm{C}_{4}$ | $\mathrm{C}_{5}$ | $\mathrm{C}_{6}$ | $\mathrm{C}_{7}$ |
| $\mathrm{D}_{0} \mathrm{D}_{1} \mathrm{D}_{2} \mathrm{~T}_{3} / \mathrm{C}_{4} \mathrm{C}_{5} \mathrm{C}_{6} \mathrm{C}_{7}$ | 10 | 0xb4 | $\mathrm{D}_{0}$ | ${ }^{1}$ | $\mathrm{D}_{2}$ |  | c | $\mathrm{C}_{5}$ | $\mathrm{C}_{6}$ | $\mathrm{c}_{7}$ |
| $\mathrm{D}_{0} \mathrm{D}_{1} \mathrm{D}_{2} \mathrm{D}_{3} / T_{4} \mathrm{C}_{5} \mathrm{C}_{6} \mathrm{C}_{7}$ | 10 | 0xcc | $\mathrm{D}_{0}$ | $\mathrm{D}_{1}$ | $\mathrm{D}_{2}$ |  |  | $\mathrm{C}_{5}$ | $\mathrm{C}_{6}$ | $\mathrm{C}_{7}$ |
| $\mathrm{D}_{0} \mathrm{D}_{1} \mathrm{D}_{2} \mathrm{D}_{3} / \mathrm{D}_{4} \mathrm{~T}_{5} \mathrm{C}_{6} \mathrm{C}_{7}$ | 10 | 0xd2 | $\mathrm{D}_{0}$ | $\mathrm{D}_{1}$ | $\mathrm{D}_{2}$ |  |  | $\mathrm{D}_{4}$ | $\mathrm{C}_{6}$ | $\mathrm{c}_{7}$ |
| $\mathrm{D}_{0} \mathrm{D}_{1} \mathrm{D}_{2} \mathrm{D}_{3} / \mathrm{D}_{4} \mathrm{D}_{5} \mathrm{~T}_{6} \mathrm{C}_{7}$ | 10 | 0xe1 | $\mathrm{D}_{0}$ | ${ }^{D_{1}}$ | $\mathrm{D}_{2}$ |  |  | ${ }^{\text {D }}$ | ${ }^{\text {D }}$ | $\mathrm{C}_{7}$ |
| $\mathrm{D}_{0} \mathrm{D}_{1} \mathrm{D}_{2} \mathrm{D}_{3} / \mathrm{C}_{4} \mathrm{D}_{5} \mathrm{D}_{6} \mathrm{~T}_{7}$ | 10 | 0xff | $\mathrm{D}_{0}$ | $\mathrm{D}_{1}$ | $\mathrm{D}_{2}$ |  |  | $\mathrm{D}_{4}$ | $\mathrm{D}_{5}$ | $\mathrm{D}_{6}$ |

## More efficiency: 512/513b transcoding

- 512/513b coding takes $8 x$ 64/66b blocks (8x XLGMII transfers) and transports them with fewer total bits by virtue of combining the individual control/data frame bits
- For example, collect all 66b control frames within the block of $8 x$ 66b frames and puts them at the beginning of the block, and the data frames at the end of the block

8x 66b Frames


1x 513b Frame

| 1 | TH | C1 | C2 | C3 | C4 | C5 | C6 | C7 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7 | TH | C1 | C2 | C3 | C4 | C5 | C6 | C7 |
| 0 | D0 | D1 | D2 | D3 | D4 | D5 | D6 | D7 |
| 2 | D0 | D1 | D2 | D3 | D4 | D5 | D6 | D7 |
| 3 | D0 | D1 | D2 | D3 | D4 | D5 | D6 | D7 |
| 4 | D0 | D1 | D2 | D3 | D4 | D5 | D6 | D7 |
| 5 | D0 | D1 | D2 | D3 | D4 | D5 | D6 | D7 |
| 6 | D0 | D1 | D2 | D3 | D4 | D5 | D6 | D7 |

## Possible Transcoding

- Choice of PCS layer is tightly tied to RS FEC choice, which in turn is tied to symbol rate on line
- Goal is to have an integral number of 64B66 frames in an RS FEC frame
- RS FEC frame line rate should be a simple multiple of the bit rate so both can be synthesized with a single PLL
- for instance 64B66 has a 33/32 ratio between line rate and bit rate (NRZ so symbol rate = bit rate)
- Given the minimum FEC frame size requirements presented later in this presentation as being RS1024 $(564,514)$ the most reasonable multiple of line-rate to bit-rate is $9 / 8^{*}$, which gives RS1024 $(576,514)$ as the line code
- RS FEC payload is 5140 bits long $=20 \times 256$ B257 frames or $10 \times 512$ B513 +10 -bit OAM
- The latter is more optimal as it provides identical capacity as 20x 256B257 frames but also altows OAM signaling as per 1000BASE-T1



## Possible Transcoding (continued)

- Using this frame allows reuse of the Clause 134 framing and training machinery which sends one 257B long alignment marker every 1024 RS frames
- Alternatively, for the 512B513-based frame the 10 -bit OAM field and $1^{\text {st }} 513 \mathrm{~B}$ block can be replaced with the alignment marker 257B block, one normal 257B block, and a 9 -bit field, like a superframe counter.



## Reed Solomon code complexity, latency and cost

- RS code choices from Tu:
- m=10: GF(2^10) RS codes - cover ~50ns burst, latency ~ 10000BT
- Tu cites concern over DFE error propagation
- m=11: GF(2^11) RS codes - cover ~98ns burst, extra complexity, latency ~ 20000-21000 BT
- m=12: GF(2^12) RS codes - cover ~160ns burst, more complexity, latency ~ 21000-32000 BT
- Complexity of RS decoders grows exponentially in $m$ or faster
- Code latency grows exponentially in m , dominates the packet size (10000BT = 1250bytes), $5 x$ the code latency of 10GBASE-T!
- Fixed even if we DON'T have heavy impulse interference
- High-speed interconnects will be performance limited by latency
- Traditionally, long bursts, code complexity and ability to vary latency are managed by interleaving - not by growing the code


## Interleaving

- x2 Interleaving takes $2 x$ RS frames and commutates symbols before transmission


RS1024 $(576,514)$ frame \#0

- x4 Interleaving takes 4x RS frames and commutates symbols before transmission
- The point of interleaving is to distribute a burst error across a group of interleaved frames, each which can fix the portion distributed to it
- Design is a trade-off between the length of the burst, and how often it occurs
- Smaller fields yield simpler RS codes, but they can correct less and are shorter


## Possible interleave and performance

- Burst length can be met either by a large-GF RS code or by a shorter RS code with interleaving
- Large GF codes fix the coding latency for all applications...
- Shorter GF codes + interleaving make latency programmable.
- Not much value going to RS(288, 258, 9) or shorter as these would need $>\mathrm{L}=2$ interleaving
- Large GF codes increase complexity
- RS $(576,514,10)$ with $L=1$ or 2 appear good candidates
- L=2 meets burst error criterion as defined
- Could support greater interleaving as well if necessary


## PHY1 FEC Simulation Results

| 10Gbps PAM4 | $\begin{gathered} \text { Interleave } \\ \text { L= } \end{gathered}$ | \# of Tests | Output BER | Output FER | Simulation including error events: <br> - Automotive Transient impulse |
| :---: | :---: | :---: | :---: | :---: | :---: |
| RS(288,258,9) | 1 | $>1 \mathrm{E}+10$ | 1.7E-10 | 2.72E-9 | - Automotive Transient impulse <br> - +/-0.2V, 50n Triangular <br> - Occurring every 100us |
|  | 2 | $>1 \mathrm{E}+10$ | 1.4E-11 | 2.35E-9 |  |
| RS(564,514,10) | 1 | $>1 \mathrm{E}+10$ | 2.37E-13 | 5.14E-9 | - Different Narrowband RFI tones <br> - Different Sinewaves with $4.5 \mathrm{~m} V_{\text {RMs }}$ |
|  | 2 | >1E+10 | 0 | 0 |  |
| $\mathrm{RS}(576,514,10)$ | 1 | >1E+10 | 0 | 0 |  |
|  | 2 | >1E+10 | 0 | 0 | - DFE error propagation <br> - 1-Tap DFE |
| $\begin{aligned} & \text { 2.5G/5Gbps } \\ & \text { PAM2 } \end{aligned}$ | Interleave L= | \# of Tests | Output BER | Output FER |  |
| RS(288,258,9) | 1 | $>1 \mathrm{E}+10$ | 0 | 0 | - $S N R=\sim 18.5 \mathrm{~dB}$ at Slicer |
|  | 2 | >1E+10 | 0 | 0 |  |
| $\mathrm{RS}(564,514,10)$ | 1 | $>1 \mathrm{E}+10$ | 0 | 0 |  |
|  | 2 | >1E+10 | 0 | 0 |  |
| $\mathrm{RS}(576,514,10)$ | 1 | $>1 \mathrm{E}+10$ | 0 | 0 |  |
|  | 2 | >1E+10 | 0 | 0 |  |

## Conclusion

- Accelerate 802.3 ch standard by borrowing from other 802.3 efforts where possible
- PAM-4 offers good performance, compatibility to 802.3 standards, reuse and low complexity
- 2^10 RS codes with interleaving meet error correction requirement while managing complexity and latency


## Thank you. <br> AQUANTIA <br> ACCELERATING CONNECTIVITY

BCI Measurements for STP Cable with Grounded \& Float Shield For RF Ingress for Frequencies $<400 \mathrm{MHz}$


