

# C2M Redux

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Sept, 8 2021

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# CM voltage thoughts

Common mode voltage has a number of sources

## ❑ Coherent imbalance examples

- P/N not exactly complementary
- Skew
- Rise/fall time mismatch
- Tend to be higher frequencies

## ❑ Non coherent imbalance examples

- Power supply (tend to be lower frequencies)
- Bias wander (tend to be mixed frequencies)
- Crosstalk (tend to be mixed frequencies)

The present AC RMS specification

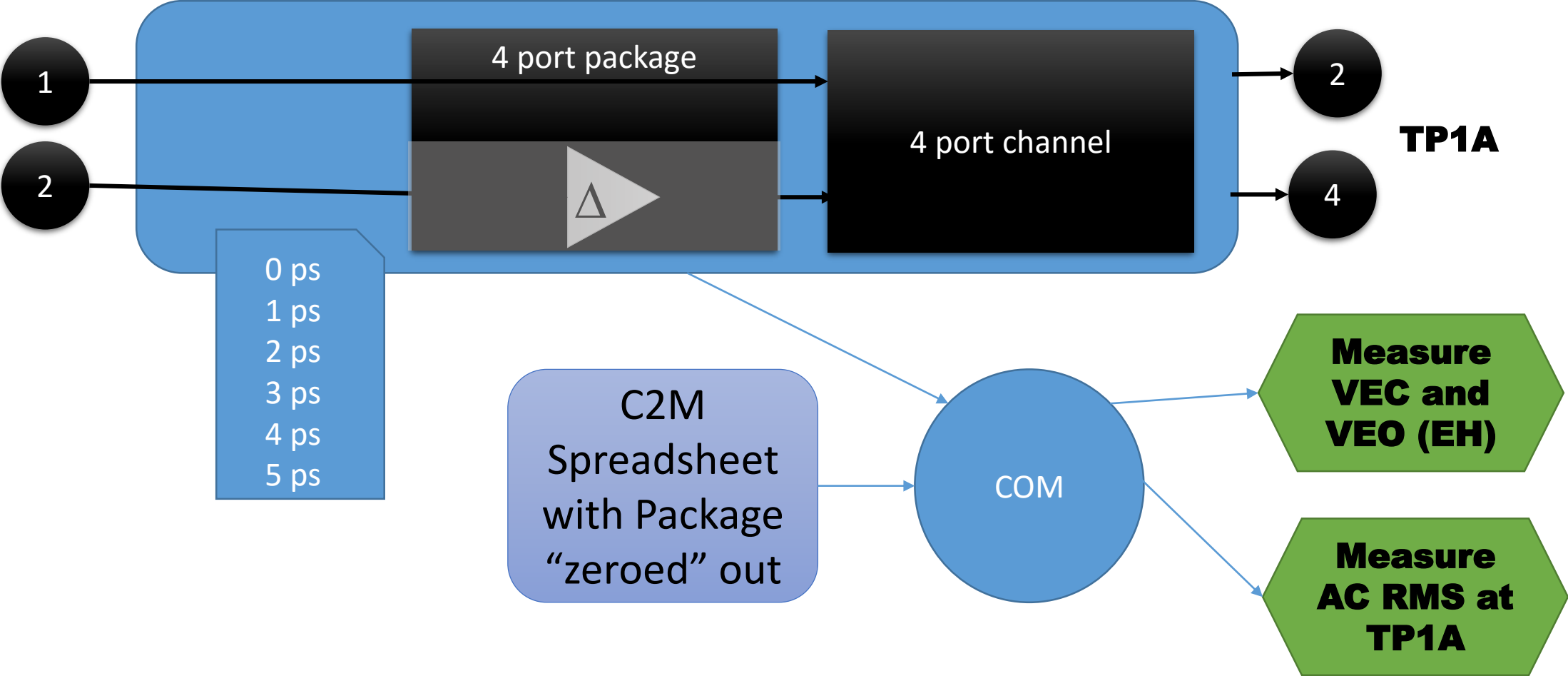
- ❑ May result in failing parts that in practice operate if the AC CM spec is too high
- ❑ May result in passing parts that to fail operate if the AC CM spec is too low

The present AC RMS method seems to put the coherent and non-coherent at odds

# Follow-on to mellitz\_3ck\_01b\_0721

- ❑ New data to focus on skew
  - See [mellitz\\_3ck\\_01b\\_0721](#)) slide 10
- ❑ Sweep skew from 0 to 5 ps
- ❑ Review TP1a data
- ❑ VEC, CM voltages, etc

Skew experiment use a synthesized s4p file which includes a modified reference package



# Channels considered

C2M\_\_Z100\_IL13\_BC-BOR\_N\_N\_N\_THRU\_tmp' (mellitz\_3ck\_01\_0518)

Channel5\_thru\_small\_pad\_2inch\_tmp' (lim\_3ck\_adhoc\_02\_073119)

Channel5\_thru\_small\_pad\_3inch\_tmp'' (lim\_3ck\_adhoc\_02\_073119)

Channel5\_thru\_small\_pad\_4inch\_tmp'' (lim\_3ck\_adhoc\_02\_073119)

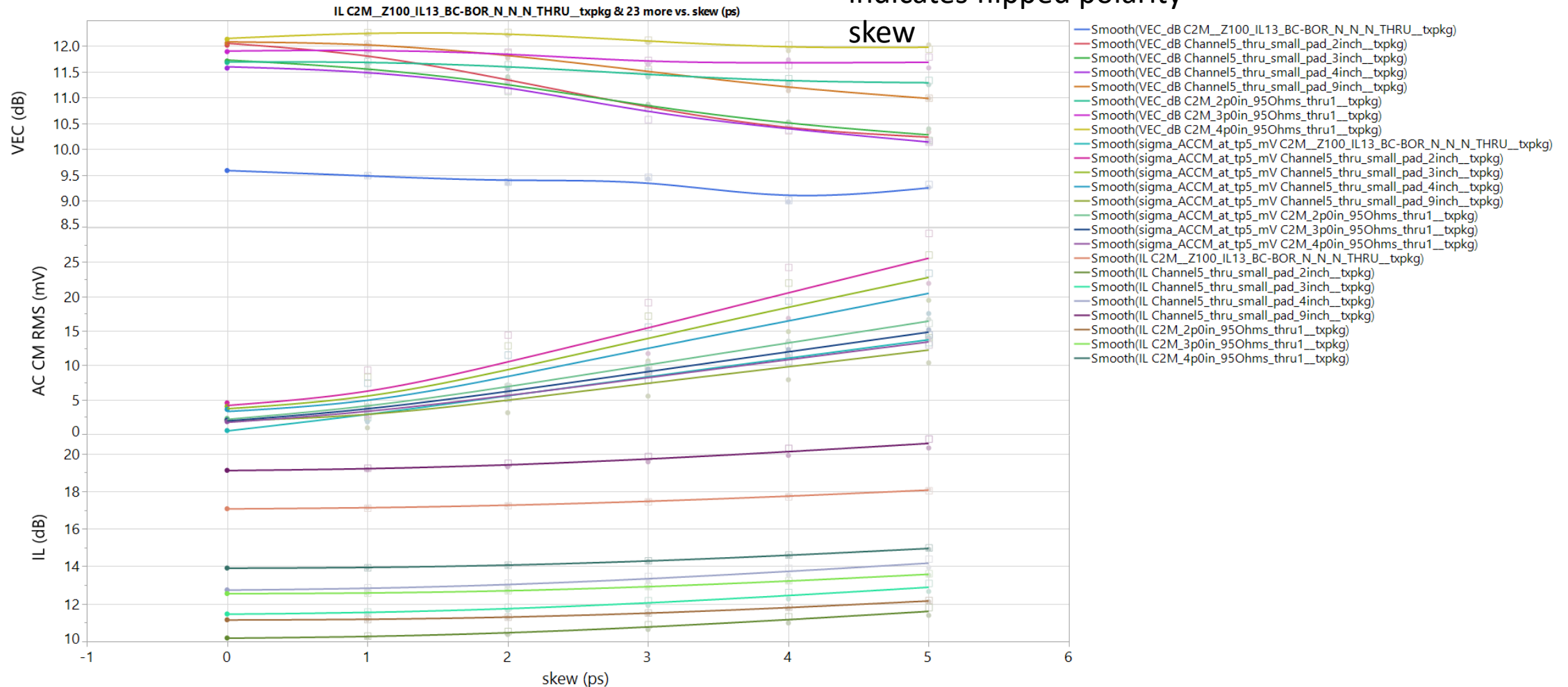
Channel5\_thru\_small\_pad\_9inch\_tmp'' (lim\_3ck\_adhoc\_02\_073119)

C2M\_3p0in\_95Ohms\_thru1\_tmp'' (akinwale\_3ck\_C2M\_08222019)

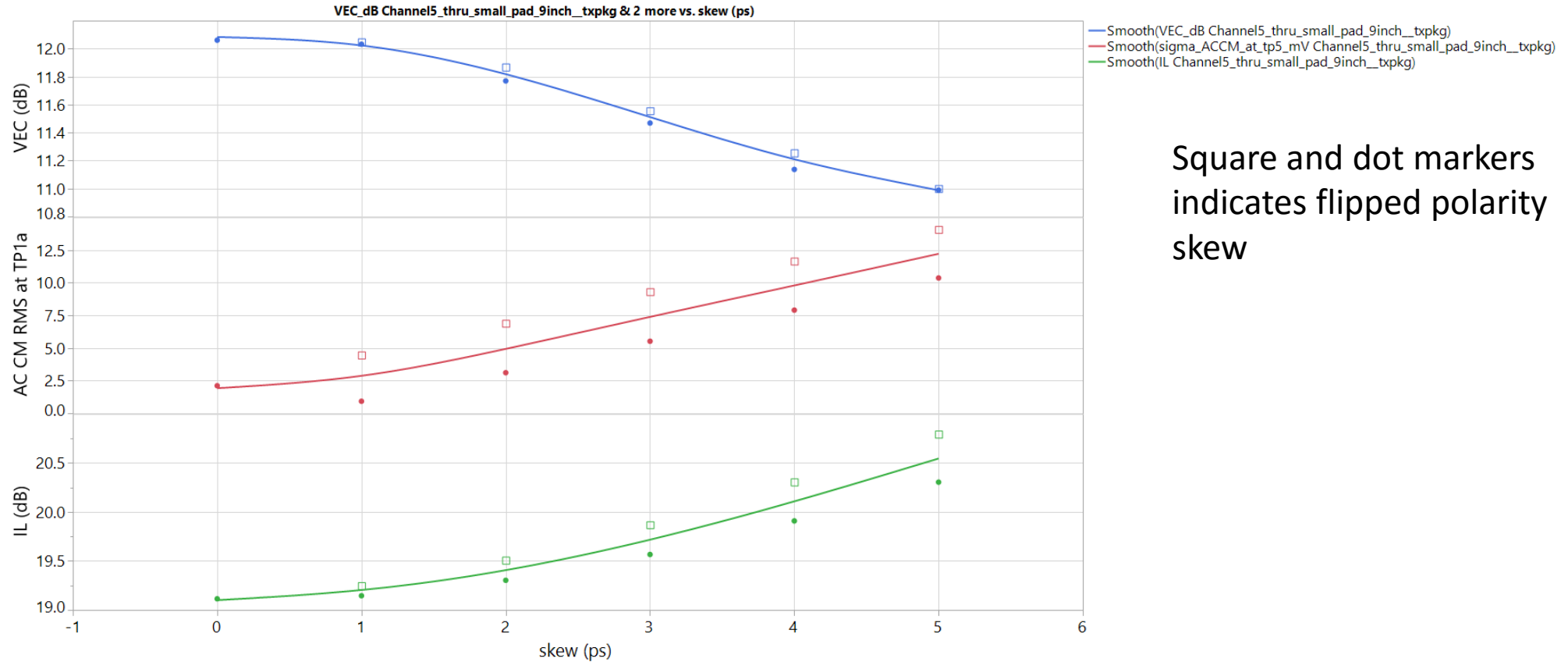
C2M\_4p0in\_95Ohms\_thru1\_tmp'' (akinwale\_3ck\_C2M\_08222019)

# High AC CM RMS does not always mean worse (Higher) VEC

Square and dot markers indicates flipped polarity



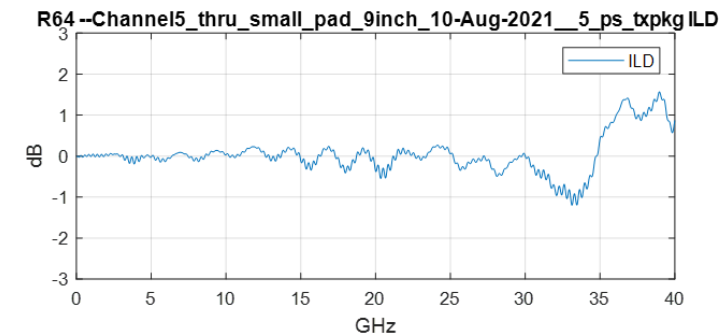
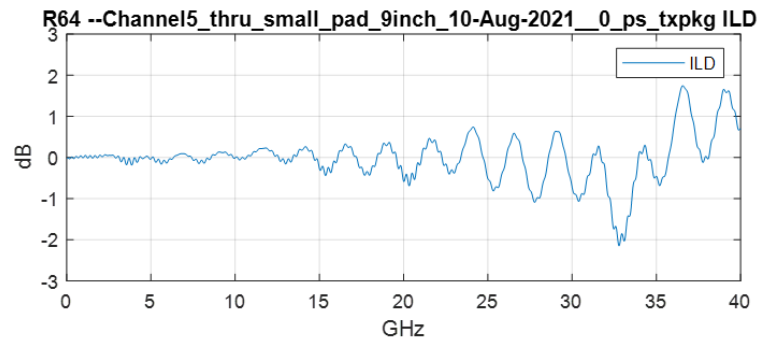
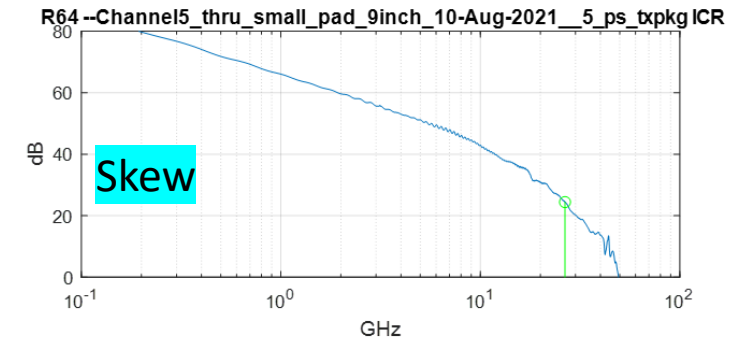
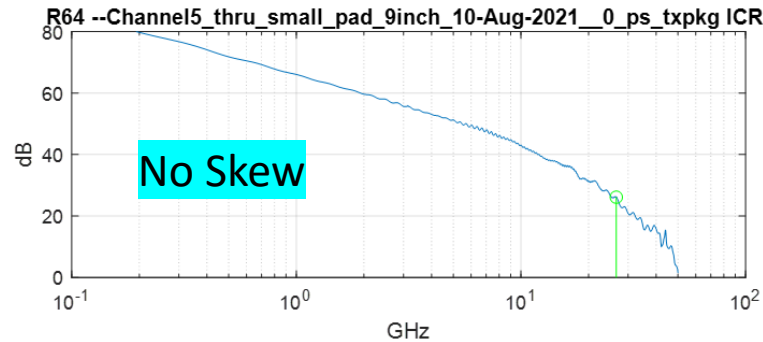
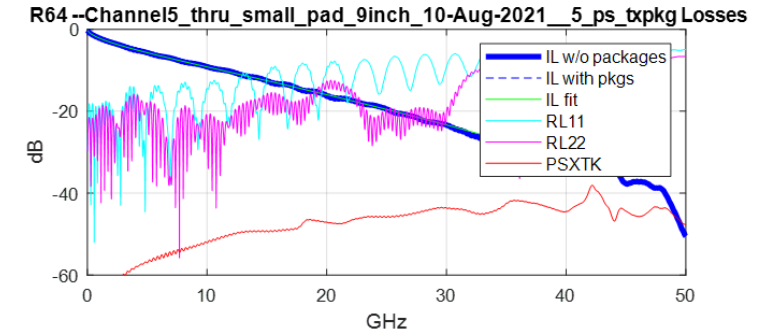
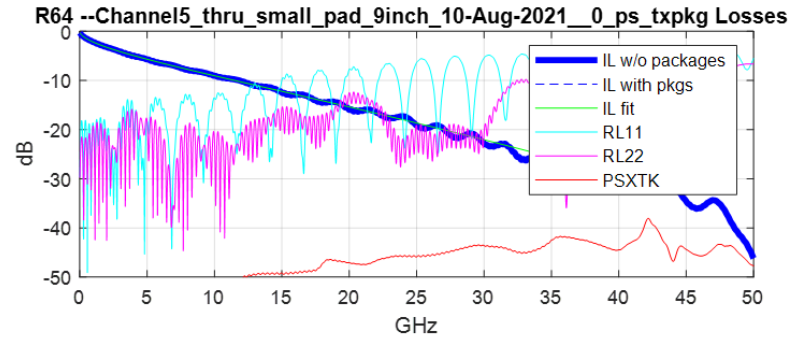
# Skew improves VEC on “channel5\_thru\_small\_pad\_9inch” (lim\_3ck\_adhoc\_02\_073119)



Perhaps coherent and non-coherent noise should be measured differently

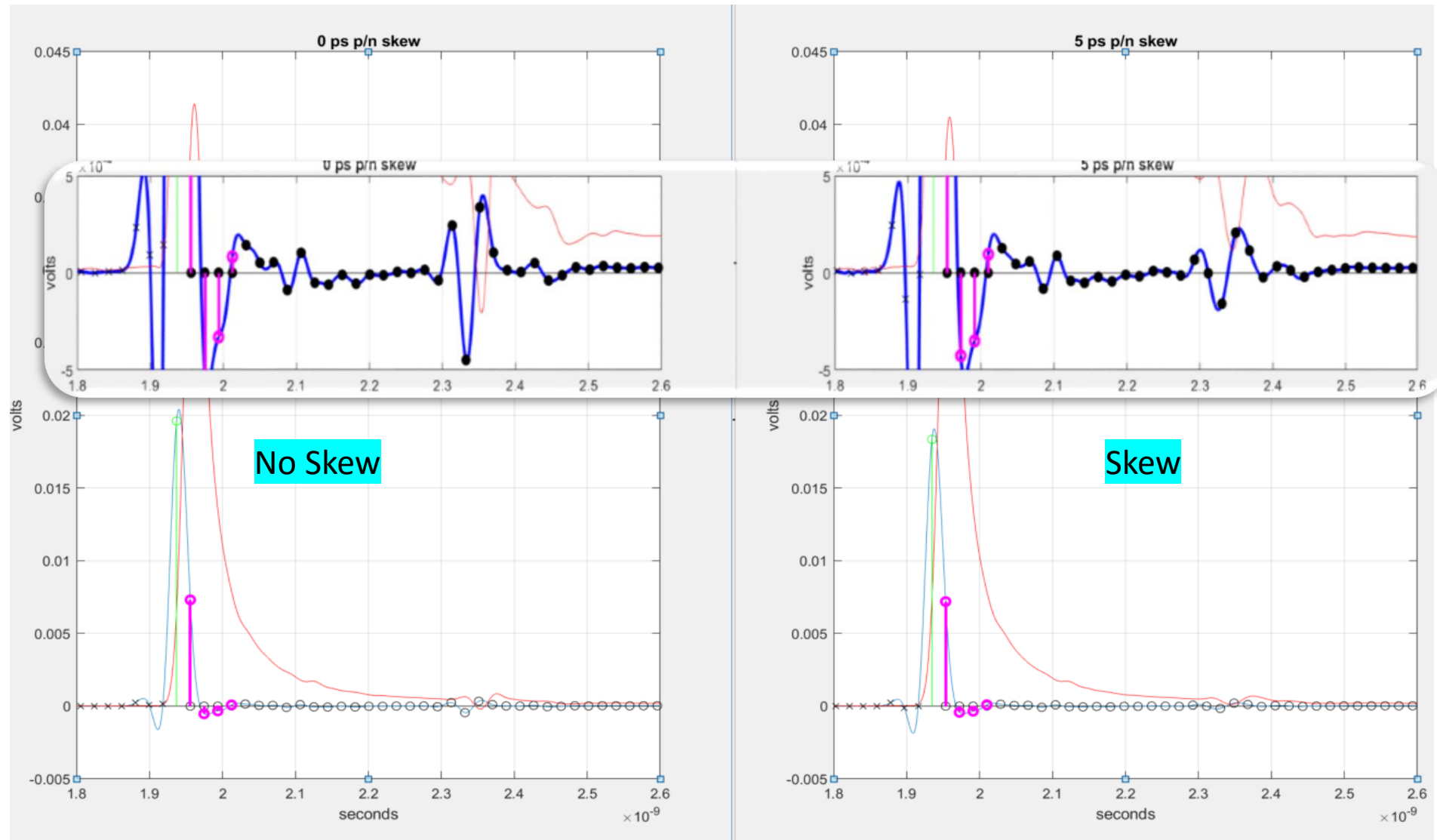


# Frequency domain plot w/o package skew



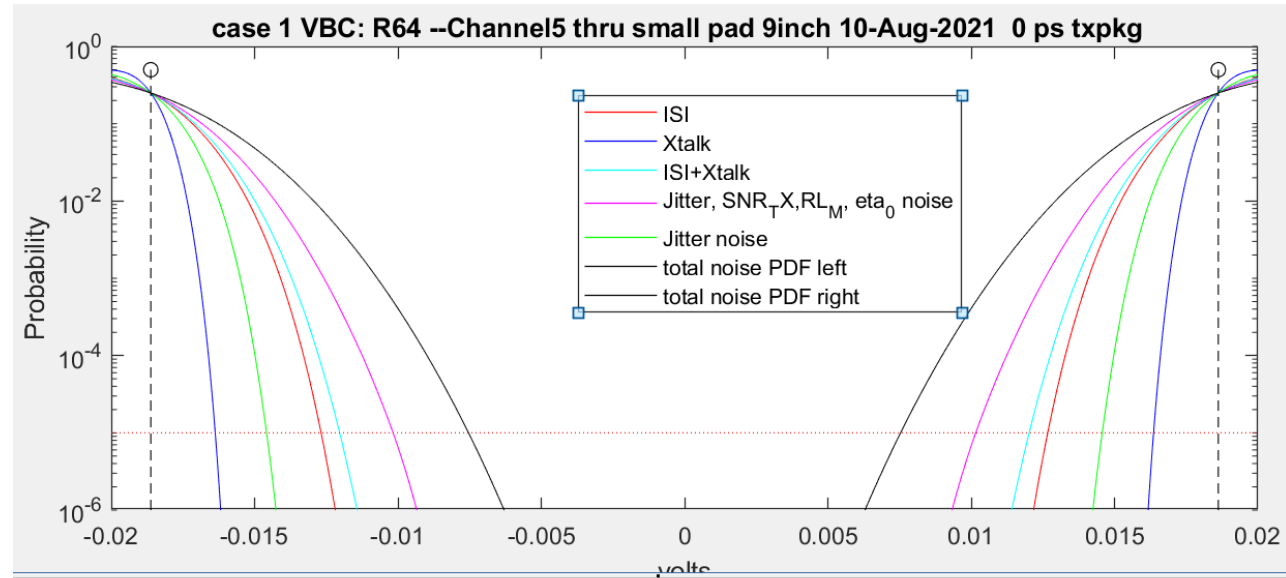
Skew improved ILD

# Pulse response comparison shows less reflection

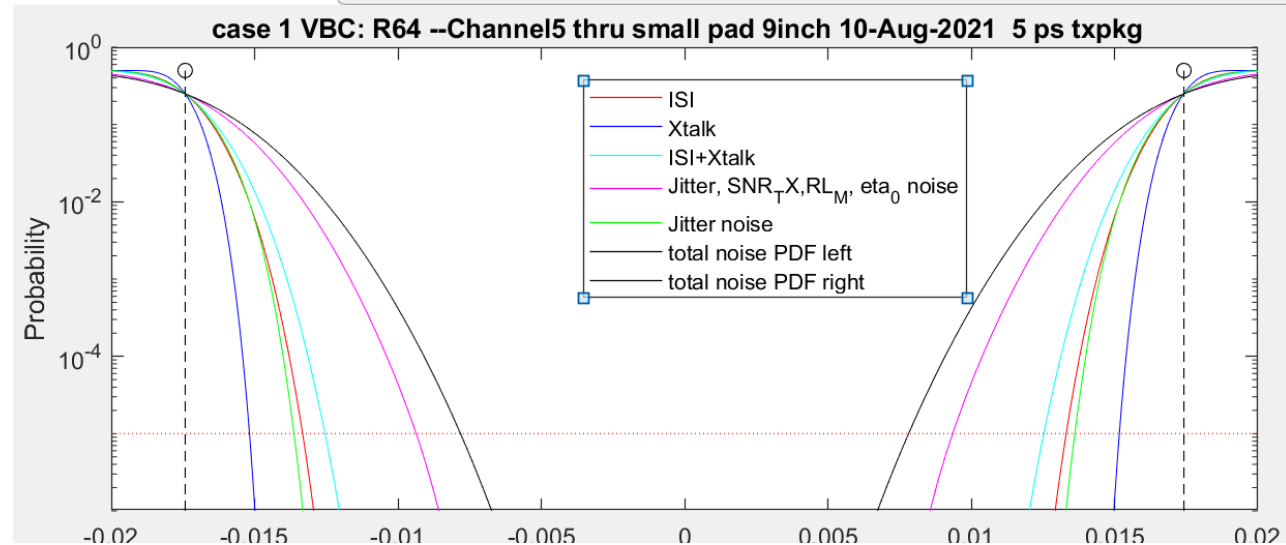


# Bathtub curves show wider eye open with skew

No Skew



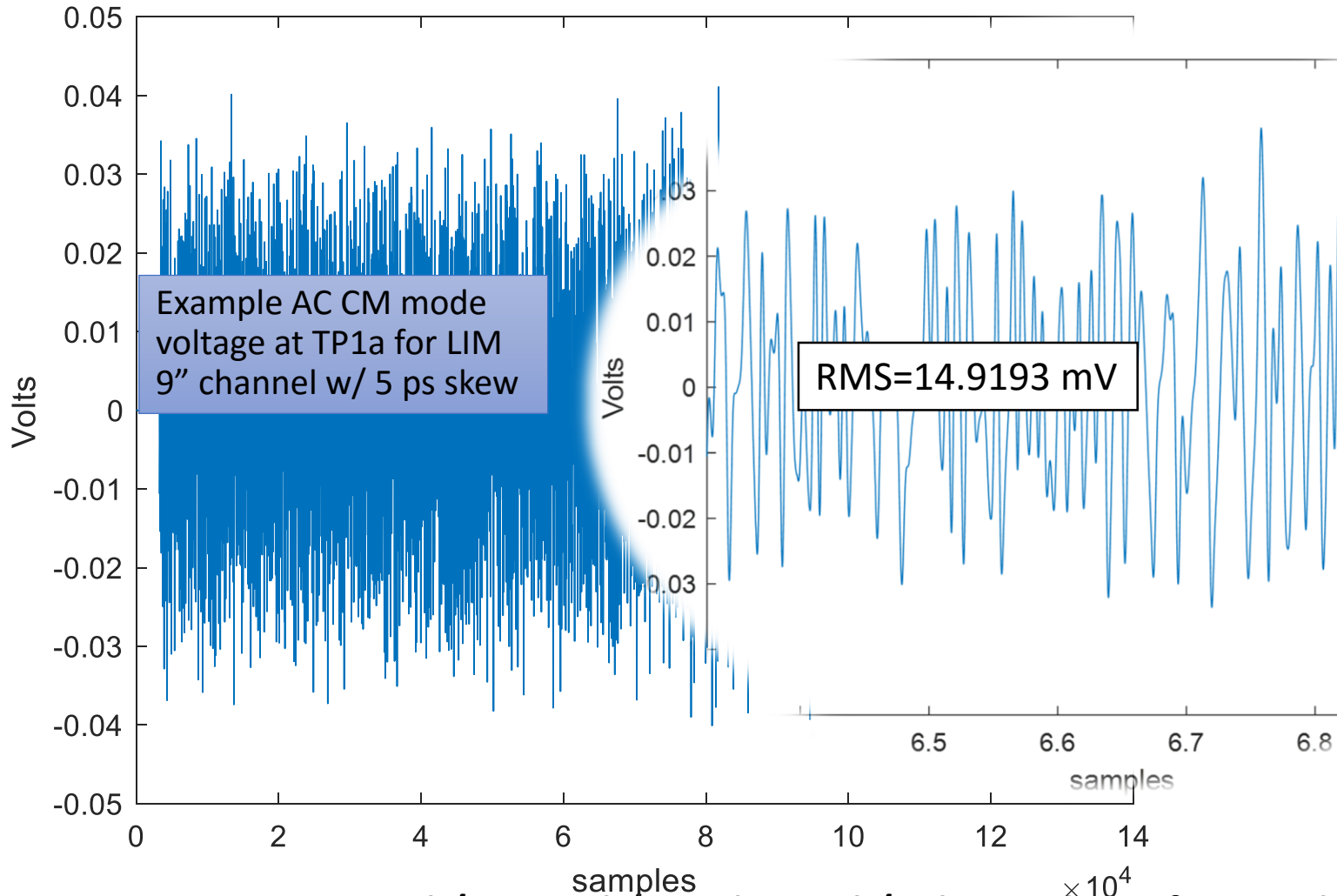
Skew



# Observations

- ❑ In some instances skew can be used to cancel reflection
  - i.e. an interconnect design tool
- ❑ The skew may increase RMS of the common mode voltage waveform

# Thinking about coherent CM noise



Consider

- ❑ Too much peak to peak AC CM voltage at TP1a may be detrimental Rx circuit operation
- ❑ Limiting p-p voltage could be the tact for coherent CM voltage
- ❑ Limiting non-coherent noise with a  $\sigma_e$  and  $\sigma_n$  computed for CM signal  $Y_{CM}(k)$  instead of DM signal  $Y(k)$

# Options for coherent CM – limit peak CM voltage for 120G and 162

Specify : AC CM Peak (max) = 50 mV for 120G and 162

## CM measurement using averaging

Option 1: Maximum  $|PX_1| < \text{AC CM Peak (max)}$

- Use  $PX_1$  from equation 85-8
- $PX_1$  is a “fitted CM waveform”

Option 2: Maximum  $|Y| < \text{AC CM Peak (max)}$

- $Y = \text{averaged}(CM \text{ Waveform})$

## CM measurement not using averaging

Option 3: Maximum  $|CM \text{ Waveform}| < \text{AC CM Peak (max)}$

- Includes both coherent and non-coherent signals

Recommend option 1

- Discussion needed

# Considerations for clauses which use TP0v

- ❑ Limit  $\text{SNDR}_{\text{CM}}$  instead of specifying a AC CM RMS and peak voltage
- ❑ Simulation of CM voltage at TP0v is not well defined
- ❑  $\text{SNDR}_{\text{CM}}$  is somewhat tolerant of test fixtures.

# Considerations for non-coherent and coherent CM for both 120G and sections which use TP0v

## □ Assuming

- the  $p(k)$ , and  $p_{cm}(k)$  are time synchronous
- CM and DM signal are sample synchronous

## □ Define $\sigma_{e\_}$ : from 84.8.3.3.5

- Replace  $Y$  with the common mode voltage and call  $Y_{CM}$
- Compute the linear fit to the captured waveform and the linear fit pulse response,  $p_{CM}(k)$ , and error,  $e_{CM}(k)$ , according to 120D.3.1.3. Denote the standard deviation of  $e_{CM}(k)$  as  $\sigma_{e\_CM}$ .

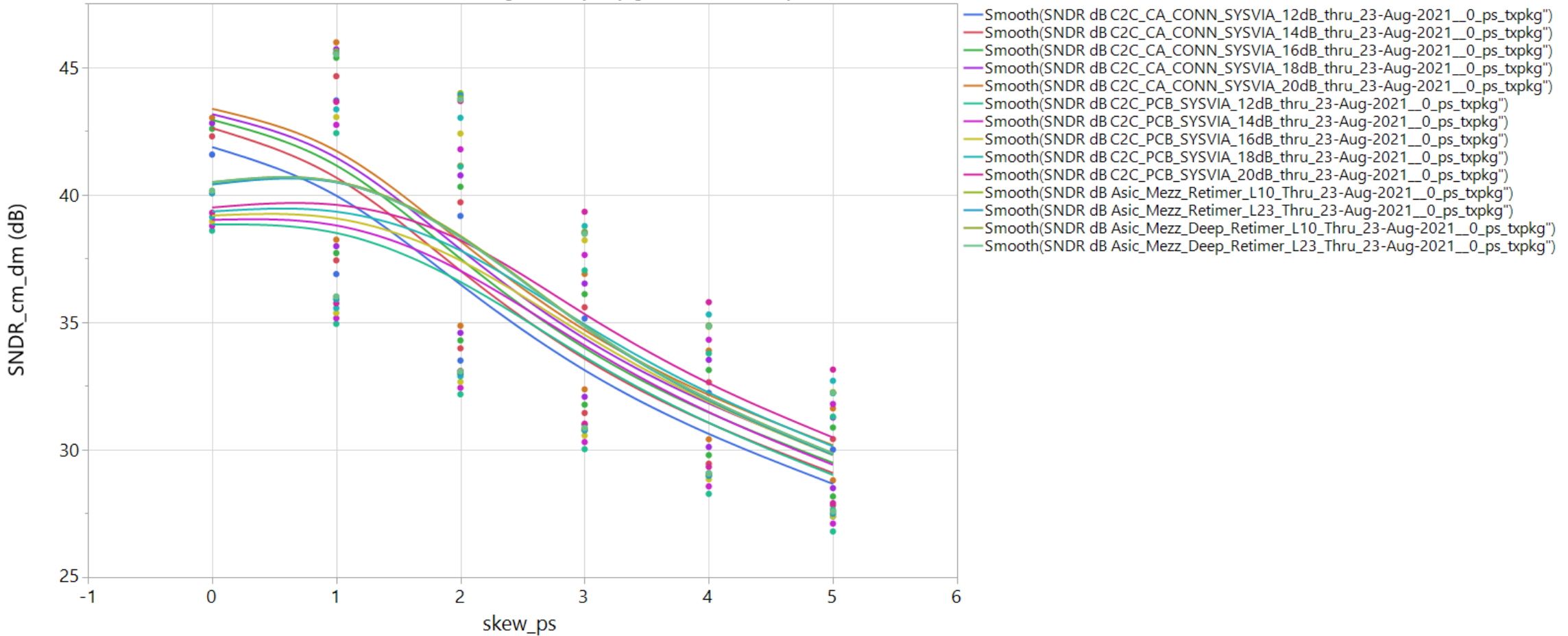
## □ Define $\sigma_{n\_CM}$ : from 120D.3.1.6 and

“Using the same configuration of the transmitter equalizer, measure the RMS deviation from the mean of the CM voltage at a time point corresponding to where the DM signal is at a fixed low-slope point in runs of at least 6 consecutive identical PAM4 symbols. PRBS13Q includes such a run for each of the PAM4 levels. The average of the four measurements is denoted as  $\sigma_{n\_CM}$ .”



# SNDR\_CM\_CM data for 120G

SNDR dB C2C\_CA\_CONN\_SYSVIA\_12dB\_thru\_23-Aug-2021\_\_0\_ps\_txpkg" & 13 more vs. skew\_ps



# SNDR

□ Specify  $\text{SNDR}_{\text{CM\_DM}} = 10 \log_{10} \left( \frac{P_{\text{max}}^2_{\text{DM}}}{\sigma_{e_{\text{CM}}}^2 + \sigma_{n_{\text{CM}}}^2} \right) > 27 \text{ dB}$

- From previous slide

□ Specify  $\text{SNDR}_{\text{CM\_CM}} = 10 \log_{10} \left( \frac{P_{\text{max}}^2_{\text{CM}}}{\sigma_{e_{\text{CM}}}^2 + \sigma_{n_{\text{CM}}}^2} \right) > 12 \text{ dB}$

- Covers the 30 mV specified in D3.2

# Summary

- ❑ For Annex 120G and CL 162
  - Maximum | *Fitted DM Waveform* | < 50 mV
- ❑ For Annex 120G, 120F and Clause 162, 163
  - $\text{SNDR}_{\text{CM\_DM}} < 27 \text{ dB}$
  - $\text{SNDR}_{\text{CM\_CM}} < 12 \text{ dB}$

**Thank you!**