

# **NePhotonics**

## A Methodology to Obtain OSNR Penalty vs Optical Inter-Channel Crosstalk

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Way\_3cw\_01\_200716

## Introduction

- Inter-channel crosstalk was proposed as a black link parameter (way\_3cw\_01a\_200423)
  - The crosstalk power integration filter was arbitrarily chosen to be 75GHz
  - The crosstalk was assumed to be flat
- Inter-channel crosstalk was calculated for different MUX/DEMUX filter shapes and a pulseshaped TX spectrum (maniloff\_3cw\_01\_200528), but not directly related to rOSNR penalty
  - Calculated electrical domain crosstalk NSR to map to rOSNR penalty
- In this contribution, we propose a general methodology to relate rOSNR penalty to interchannel crosstalk (=adjacent-channel crosstalk in coherent systems)
  - Define worst-case receiver bandwidth and DSP parameters
  - Increase the crosstalk via laser/mux/demux frequency drifts and scaling mux/demux bandwidths
  - Worst-case optical power imbalance among wavelengths
  - Define a "soft" integration filter after DEMUX to calculate optical crosstalk to signal ratio

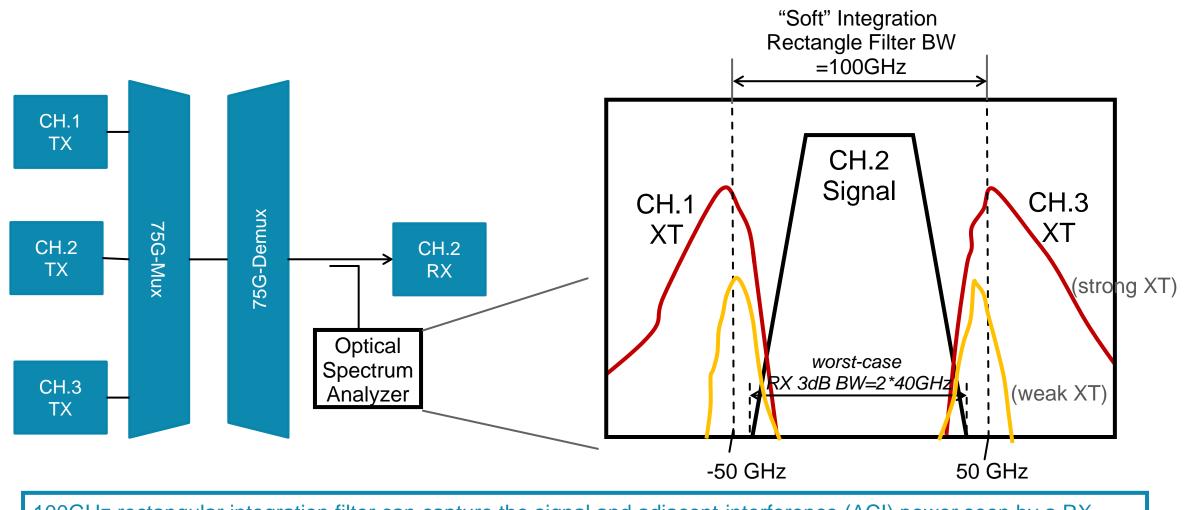


## **Worst-case Assumptions**

- Middle channel optical power 4dB lower than neighbors
- No pulse shaping, TX OSR=1, RX OSR=1.2
- Laser frequency drifts up to +/-1.8GHz
- Local Oscillator Offset (LOO)= 1.8GHz (for [+1.8 0 -1.8] laser drifts)
- Mux/Demux frequency drifts up to +/-4GHz
- RX 3dB bandwidth (including ADC) = 30, 35, and 40GHz, with a trapezoidal filter shape
- TX 3dB bandwidth 30GHz RRC  $\alpha$ =0.3, 0.4, and a realistic shape
- rOSNR baseline starts at 26dB @ pre-FEC BER=1.25e-2
- Inter-channel crosstalk (XT) is increased by laser/mux/demux frequency drifts and scaling the mux/demux bandwidth from 1 to 1.15



# **Integration Filter for Measuring XT/Signal Power**



100GHz rectangular integration filter can capture the signal and adjacent-interference (ACI) power seen by a RX whose BW is as wide as 40GHz. 100GHz is also not too wide to capture ACI power that the receiver does not see.

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# **Reference Receiver (PIN+TIA+ADC)**

#### • 30GHz RX

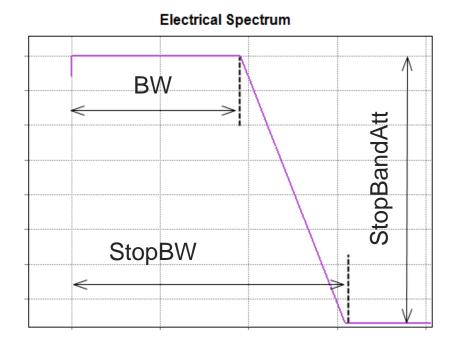
BW= 28.6 GHz StopBW= 46.4 GHz StopBandAtt= 38.5 dB

#### • 35GHz RX

BW= 33.4 GHz StopBW= 54.1 GHz StopBandAtt= 38.5 dB

#### • 40GHz RX

BW= 38.2 GHz StopBW= 61.9 GHz StopBandAtt= 38.5 dB

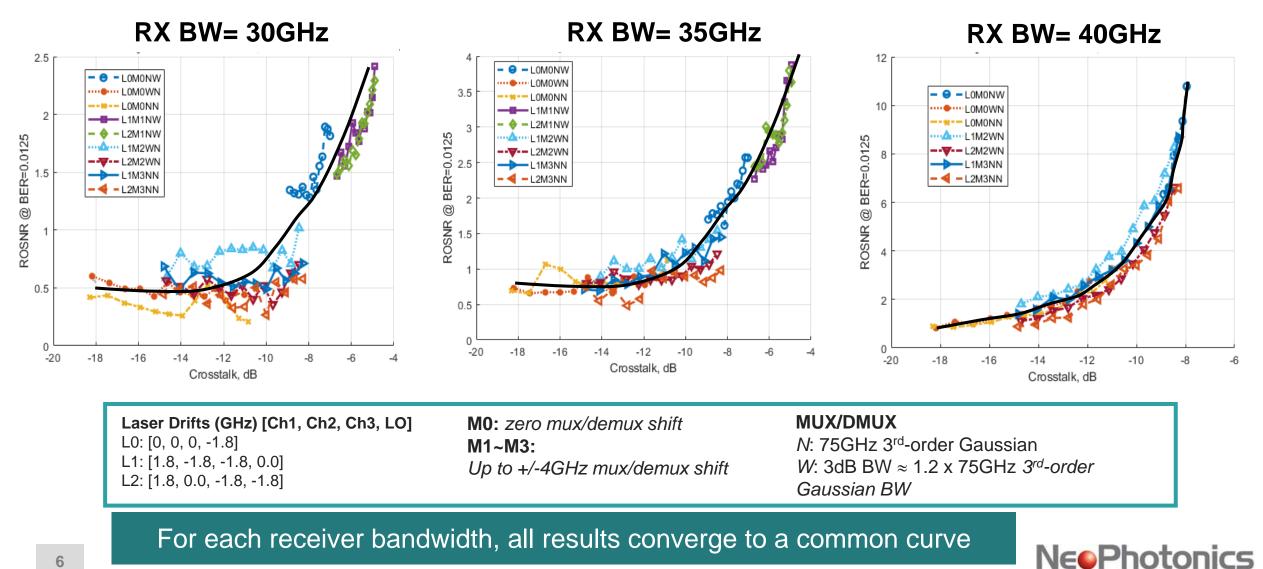


StopBW / BW= 1.62

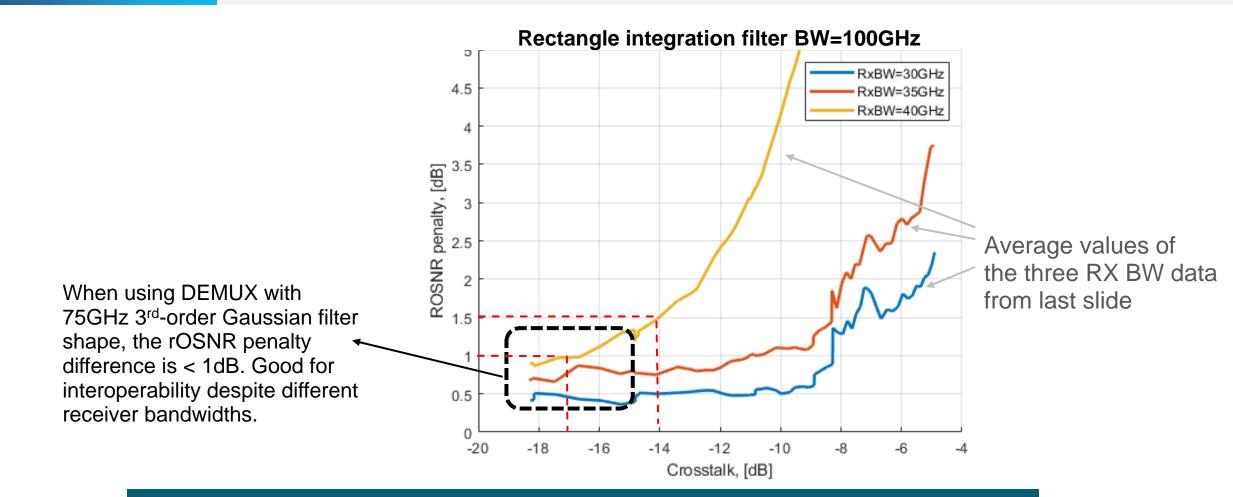


#### rOSNR Penalty @ BER=1.25e-2 vs Optical Crosstalk

3 RX BW and various combinations of MUX/DEMUX filter shape /bandwidths and laser/mux/demux frequency shifts [rectangle integration filter BW=100GHz]



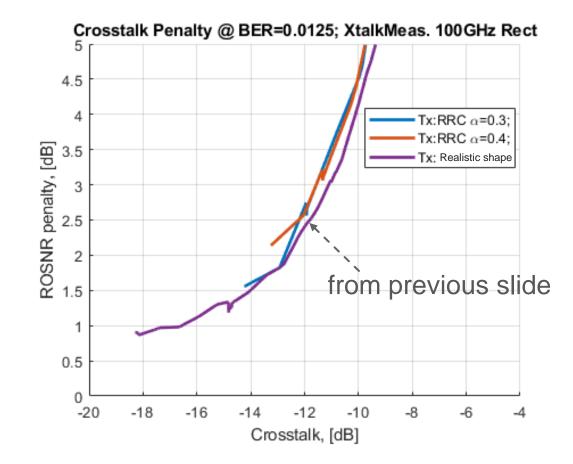
## Worst-Case rOSNR Penalty vs Optical Crosstalk



If rOSNR penalty=1 or 1.5dB, max inter-channel xtalk = -17 or -14dB when using 100GHz rectangle integration filter

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### Effects of TX Optical Spectral Shape (RX BW=40GHz)





# **OSNR Penalty vs Inter-Channel Crosstalk**

- A methodology is proposed to obtain OSNR penalty vs inter-channel crosstalk based on:
  - RX BW=40GHz with a trapezoidal shape; TX OSR=1, RX OSR=1.2, LOO=1.8GHz, TX output power 4dB lower than neighbors
  - TX BW modeled by RRC  $\alpha$  = 0.3, 0.4, and a realistic shape
  - Increase crosstalk via laser/mux/demux frequency drifts and scaling the mux/demux bandwidths
  - Define a soft integration rectangle filter with a 100GHz bandwidth to calculate optical crosstalk to signal power ratio

#### Observations

- DEMUX with a 75GHz third-order Gaussian filter shape (see maniloff\_3cw\_01\_200528, with manufacturing variation) is necessary to maximize 400ZR transceiver inter-operability
- MUX with a 75GHz third-order Gaussian filter shape (see maniloff\_3cw\_01\_200528, with manufacturing variation) could alleviate TX bandwidth constraint
- MUX/DEMUX with a 75GHz third-order Gaussian filter shape causes least interference with 400ZR transceiver design
- More simulations can be carried out with respect to reference transmitter and receiver spectral shapes and see the impact on rOSNR vs inter-channel crosstalk results

