

10GBASE-T Transmitter Key Specifications

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1000BASE-T Transmitter spec. overview



- Differential voltage at MDI output ~ 2V peak to peak as defined by Transmitter test mode 4
 - Fig. 40-21, IEEE Std 802.3-2002, Section Three

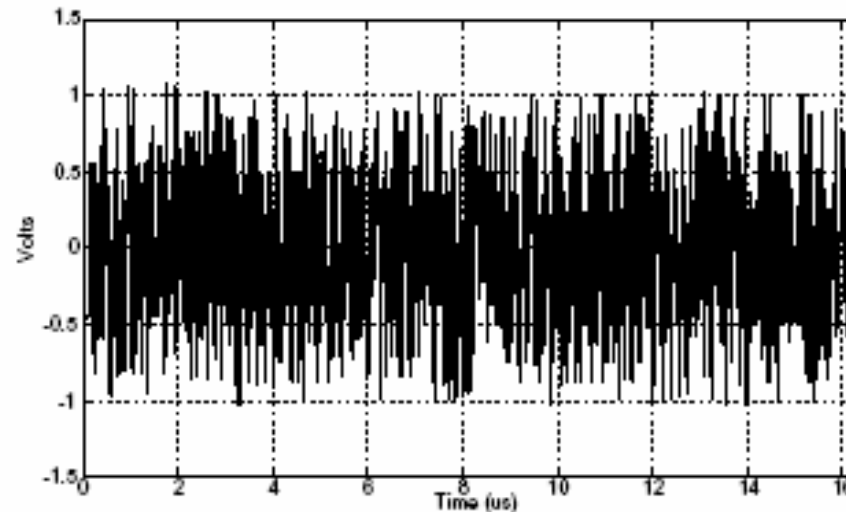


Figure 40-21—Example of Transmitter Test Mode 4 waveform (1 cycle)

- Transmitter distortion specified at the MDI output with
 - PHY transmitting sequence of symbols generated by the scrambler generator, in presence of a sine wave disturber of 5.4V Peak to Peak differential through a series 100 ohm resistor.

10GBASE-T transmitter

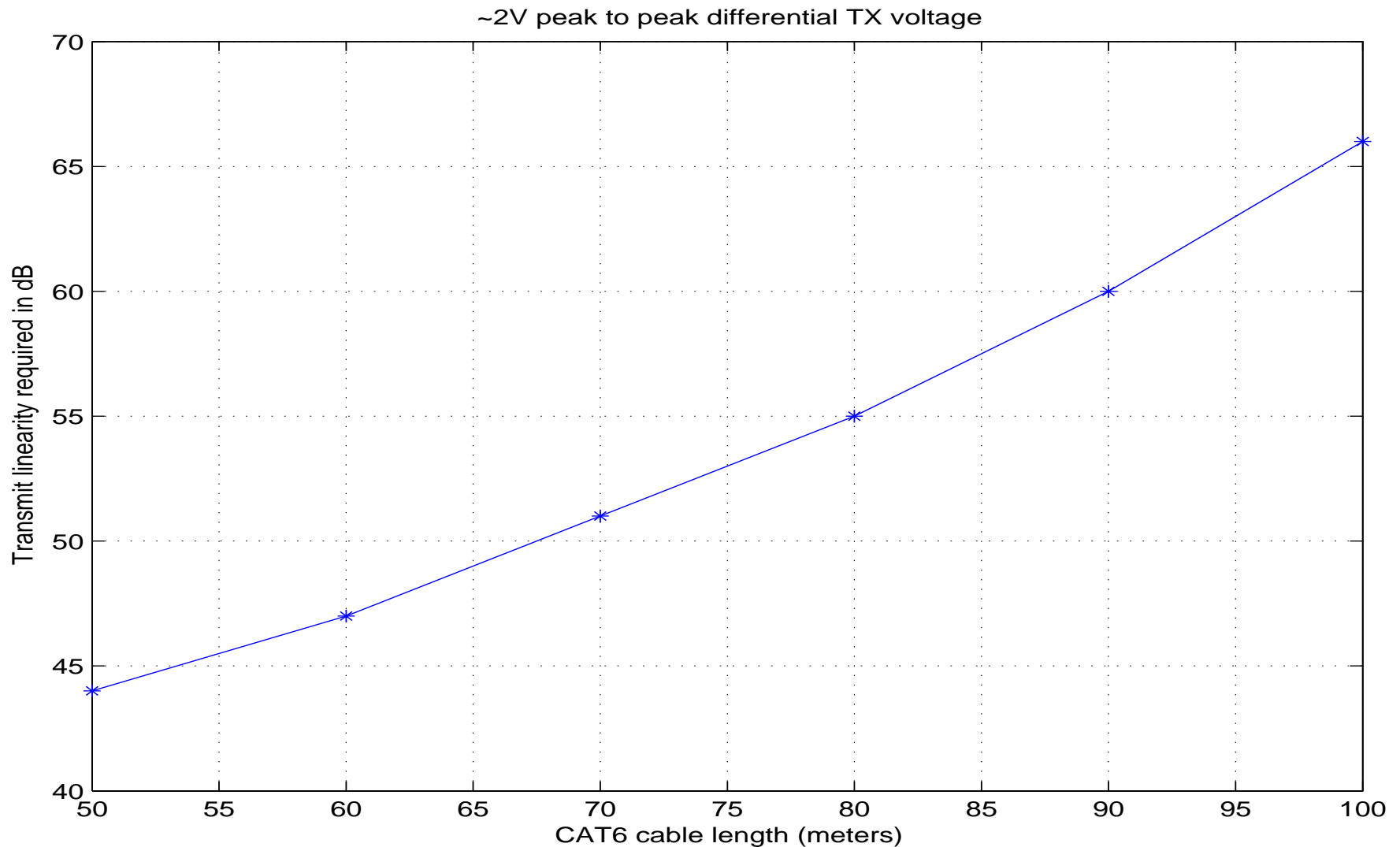
- Nonlinearity of transmitter has a transfer function of 1 (without a magnetic hybrid)
- Transmit linearity has to be high
 - Echo canceller cannot cancel the nonlinear component
 - Tough specification to meet in 10GBASE-T system.
- Transmit linearity required is highest at maximum cable length
 - In this situation, the far end transmitter signal is significantly attenuated
- Transmit linearity requirement relatively independent of the frequency.

Transmit power vs. voltage

- Spec. for the transmitter in terms of peak-to-peak output voltage
 - Output power level depends on the assumptions for filter and modulation scheme.
- Assumptions:
 - PAM8-PAM12 modulation scheme
 - For a given differential output, output power level from PAM8 to PAM12 changes by $< -0.5\text{dB}$.
 - Continuous time filter at the output of the DAC with -3dB frequency around $f_s/2$ (similar assumption to Gigabit)
- 2V peak to peak differential output (similar to gigabit) corresponds to 4.5-5dBm power level, $\sim 4\text{V}$ peak-to-peak differential (twice as Gigabit) corresponds to 10.5-11dBm power level
 - Digital filter similar to Gigabit ($0.75+0.25z^{-1}$) reduces output power level for a given voltage by another $\sim 2\text{dB}$.

Transmit linearity to meet 10G net rate

- Fixed Receiver input referred noise



Transmit linearity measurement

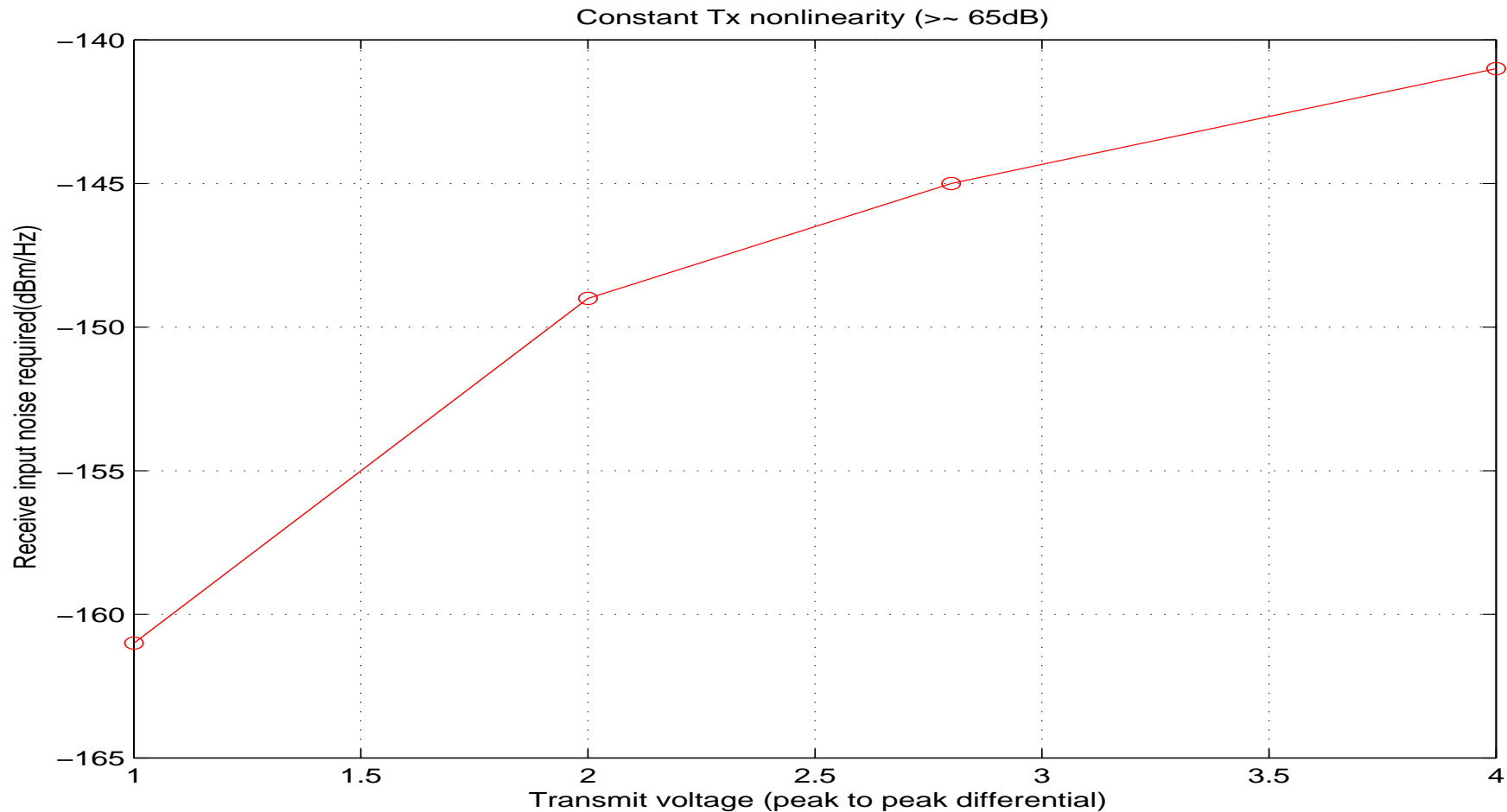
- Transmit linearity specified in 1000BASE-T in the presence of a disturber.
 - Specification requires peak distortion to be less than 10mV (post processing the output to remove disturber)
 - Disturber magnitude at transmitter output $\sim 5.4V/2 = 2.7V$ peak to peak differential sine wave at $f_s/6$
 - chosen to mimic far end transmit signal peak amplitude in presence of baseline wander assuming a short cable
 - Disturber causes $\sim 8dB$ increase in the output amplitude.
 - Makes the third order circuit nonlinearity $\sim 16dB$ larger.
- Overkill specification for 10GBASE-T because cable loss is high
 - At longer cable lengths, nonlinearity dominated by the local transmitter peak voltage, disturber magnitude being small ($\sim < 0.5V$ peak to peak differential) compared to 1000BASE-T.
 - At short cable lengths, system margin can tolerate higher non-linearity.
- Linearity specification to be defined in presence of a small disturber (0.5v peak to peak differential, sine wave $\sim f_s/8$ frequency), in terms of the peak distortion based on a transmitted sequence of symbols.

Tradeoffs on transmit voltage

- At the same spec as Gigabit Ethernet, i.e. 2V peak-to-peak differential output voltage at MDI port
 - Transmit linearity spec. ~ 65dB for channel models #1 and #3
 - In 1000BASE-T, the peak distortion spec would translate to ~48dB transmit linearity.
- Including baseline wander, and full duplex operation, worst case voltage at MDI port for 2V peak to peak differential output ~ 4.8V peak to peak differential.
- For 4V peak to peak differential output, the swing is 9.6V peak-peak differential !
- Given state of the art CMOS processes (90nm, 1v/2.5v, 0.13um, 1.2/2.5V, 0.18um, 1.8/3.3V), difficult to achieve this for any reasonable power

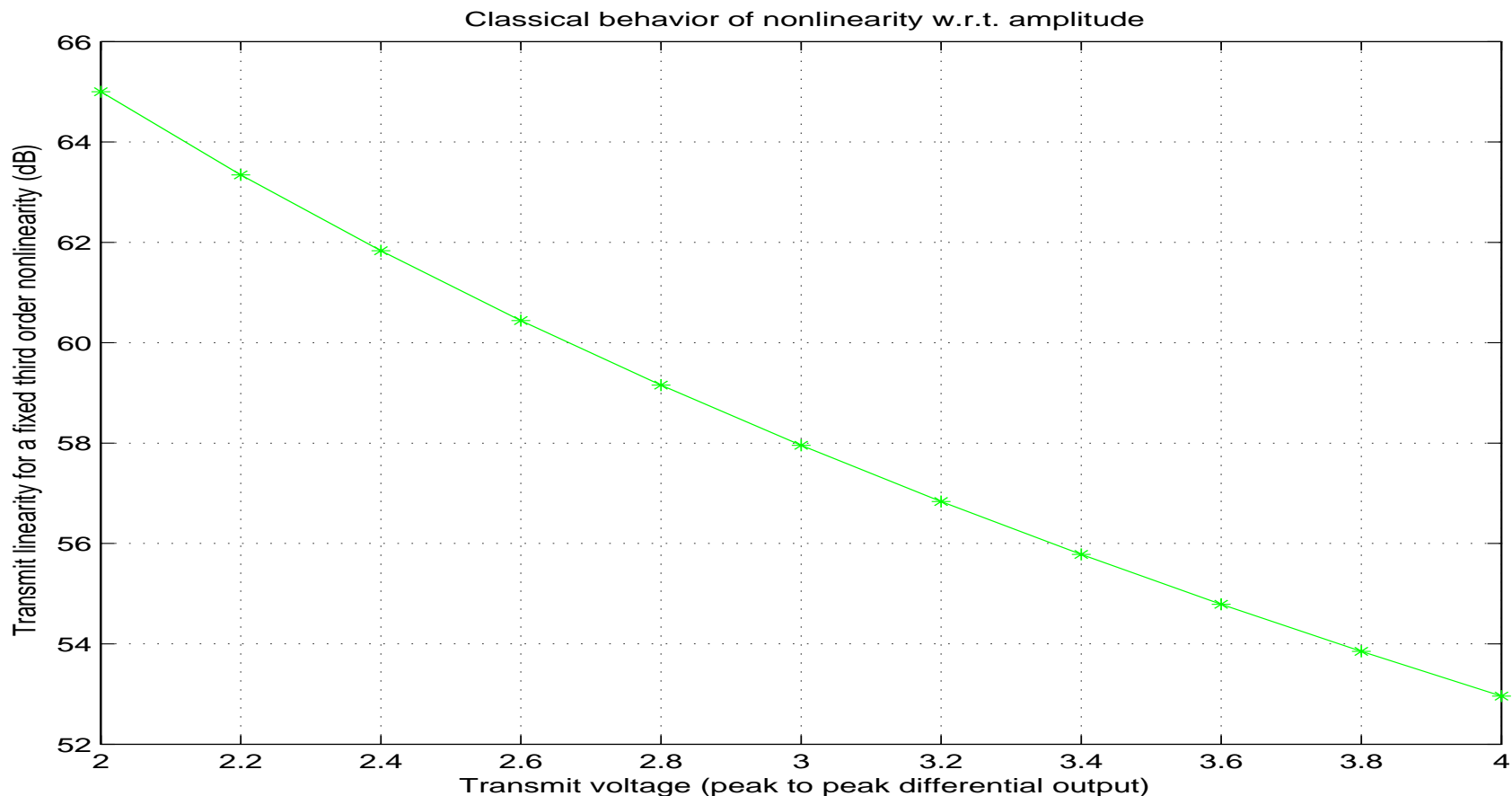
Tradeoffs on transmit voltage

- As the transmit output voltage is raised by x dB, the input referred noise of the receiver circuits reduces x dB
 - At low enough transmit output voltage, input referred noise has to go down significantly because large reductions cause very little advantage when other noise sources (background, ANEXT) limit SNR.



Tradeoffs on transmit voltage

- Transmit linearity specification **does not change** as we raise the transmitted power or voltage.
 - Differential circuits, nonlinearity dominated by HD3, HD3 2x dB worse for x dB higher transmit amplitude.
 - With 4V peak-to-peak differential, HD3 of the transmitter for the same circuit gets worse by 12dB (higher order harmonics like HD4, HD5, worse by ~ 18-24 dB as compared to 2V peak to peak differential)



MDI Return loss

- MDI return loss
 - Reflection due to differential signals incident upon the MDI from the cable
 - Different specification than the link segment return loss
- Specified in 1000BASE-T, with respect to a balanced cabling with an impedance of 100ohms +/-15%, as
 - -16dB over the frequency range of 1MHz to 40MHz
 - - $[10-20\log_{10}(f/80)]$ over the frequency range of 40MHz to 100MHz (f in MHz)
- Initial Proposal for MDI return loss for 10GBASE-T
 - **Based on**
 - The advancement in CMOS technology.
 - Available Wideband 10G transformer data.
 - Backward compliance with Gigabit Ethernet.
 - **Reflections with respect to a balanced cabling with an impedance of 100ohms +/- 15% should be attenuated by**
 - 16dB over the frequency range of 1MHz to 40MHz
 - At least $16-10\log_{10}(f/40)$ over the frequency range of 40MHz to 625MHz (To be better than 1000BASE-T by around 4dB at 100MHz)

Summary

- Transmit linearity of ~65dB needed for operating over specified channel models
- Transmit linearity measured in presence of small disturber (~0.5V peak to peak differential)
- Transmit peak to peak differential voltage ~ 2V
 - higher than 2V peak to peak, circuit nonlinearities and state of the art CMOS processes limit reasonable power implementation.
 - lower than 2V peak to peak, input referred noise required on the receiver stringent, limiting reasonable power implementation.
- Initial proposal for MDI return loss, -16dB from 0-40MHz, $-[16 - 10\log_{10}(f/40)]$ from 40MHz to 625MHz