Improved MPI "Upper Bound" Analysis

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Outline

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- Setup
- Defining MPI as optical vertical eye closure penalty
- Improved Upper Bound Method
- Statistical upper bound method
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Objective

• This presentation makes improvements on bhatt_01_0512 "upper bound" method by introducing two incrementally improved methods

• Method shown as "*Improved Upper Bound*" which takes into account the fact that MPI impact varies as a function of received symbol power

• Method shown as "*Statistical Upper Bound*" which takes into account statistical distribution of the interfering signals

• We preserve the conservative nature of penalty analysis.

• We show that the return loss spec of -35dB is a good choice to keep MPI impact to manageable values

Definitions

Signal representation in the Optical Field:

We use the same nomenclature as bhatt_01_0512 starting from page 18 for "Upper-bound based analysis". Since this presentation is trying to deal with "Upper-Bound" methods, assuming the Laser source is perfectly "coherent" is the right pessimistic assumption. The coherent signal in the optical field is represented as complex function

 A_i is the optical amplitude of the signal with $i(t) \in [1,m]$. *m* is the modulation order. (ie 16 for PAM-16) A_1 is the lowest transmit level and A_m is the highest transmit level.

Photo-Detector /TIA function maps the "optical power" to "electrical current" $I(t) \propto |e(t)|^2 = A_{i(t)}^2$

The return-loss factor RL of a connection, specifies the amount of optical power that is reflected by the connection

Setup

How many reflections are there for "n" connector link?



Modeling MPI as Vertical Eye reduction penalty

MPI Penalty

• In the following analysis we make some pessimistic assumptions and then calculate the MPI as an amplitude dependent closure of the signal eye for PAM modulation.

• Define Optical MPI penalty in dB as

10Log10 <u>Signal_Eye_Height_Without_MPI</u> Reduced_Signal_Eye_Height_due_to_MPI

Similar to bhatt_01_0512 starting from page 18 for "Upper-bound based analysis"

Page 18 Pessimistic assumptions:

- Pessimistic Assumption 1: Fiber insertion loss is zero
- Pessimistic Assumption 2: Connector insertion loss is zero
- Pessimistic Assumption 3: All interfering optical signals are perfectly aligned in polarization

Additional Pessimistic assumptions

Pessimistic Assumption 4: Laser spectral width is zero (perfect coherent laser) **Pessimistic Assumption 5**: All interfering optical signals are perfectively constructively added

$$\mathbf{e}(t) = \mathbf{A}_{i(t)} \mathbf{e}^{jwt} + \mathbf{e}^{j(wt+\theta)} \sum \mathbf{A}_{k(t)} \sqrt{(\mathbf{R}_{k1} \mathbf{R}_{k2})}$$

 A_i is the amplitude of the received signal in optical field. i(t) ϵ [1,m] and m is modulation order $A_{k(t)}$ are the interfering signals. The relative phase of all interfering signals to received signals is θ . R_1 and R_2 are the two reflection points return-loss

Pessimistic Assumption 6: Assume all interfering signals are at their maximum

Which is

$$\mathbf{e}(t) = \mathbf{A}_{i(t)} \mathbf{e}^{jwt} + \mathbf{e}^{j(wt+\theta)} \sum \mathbf{A}_m \sqrt{(\mathbf{R}_{k1} \mathbf{R}_{k2})}$$

$$\mathbf{e}(t) = \mathbf{A}_{i(t)} \mathbf{e}^{jwt} + \mathbf{e}^{j(wt+\theta)} \mathbf{A}_m \sum \sqrt{(\mathbf{R}_{k1} \mathbf{R}_{k2})}$$

Replace the sum $\sum \sqrt{(R_{k1}R_{k2})}$ with the variable S calculated as

 $S=n(n-1)R_{Conn}/2+n\sqrt{(R_{Conn}R_{TOSA})}+n\sqrt{(R_{Conn}R_{ROSA})}+\sqrt{(R_{TOSA}R_{ROSA})}$

 $e(t)=A_{i(t)}e^{jwt}+e^{j(wt+\theta)}A_mS$

The receive current is proportional to $I(t) \propto |e(t)|^{2} = A_{i(t)}^{2} + 2A_{i(t)}A_{m}SCos(\theta) + S^{2}A_{m}^{2}$ $I(t) \propto I_{i(t)} + 2SCos(\theta)\sqrt{(I_{i(t)}I_{m})} + S^{2}I_{m}$

And finally the MPI Eye Closure is

MPI_Eye_Closure=2SCos(θ)√(I_{i(t)}I_m)+S²I_m

•The worst case MPI happens for all levels from 2 to m-1 when Cos θ is +1 or -1. For level 1 the worst case is when Cos θ is +1 and for level m the worst case is when Cos θ is -1.

•Since the MPI is amplitude dependent, the penalty for level 1 is pretty small.

Pessimistic assumption 7: Cos θ =-1 and the term S^2I_m is so small that it can be ignored in practical cases.

$$\begin{split} S = n(n-1)R_{Conn}/2 + n\sqrt{(R_{Conn}R_{TOSA}) + n\sqrt{(R_{Conn}R_{ROSA}) + \sqrt{(R_{TOSA}R_{ROSA})}} \\ MPI_Eye_Closure = -2S\sqrt{(I_{i(t)}I_m)} \end{split}$$

•Bhatt_01_0512 further assumed the received signal Ii is at maximum I_m and calculated the MPI penalty as

 $S=n(n-1)R_{Conn}/2+n\sqrt{(R_{Conn}R_{TOSA}) + n\sqrt{(R_{Conn}R_{ROSA}) + \sqrt{(R_{TOSA}R_{ROSA})}}$ $MPI_Eye_Closure=-2S\sqrt{(I_mI_m)}$

•For example setting R_{TOSA}=R_{ROSA}=R_{Conn}=R and ER=6dB, the following MPI table is produced

MPI Penalty upper bound in dB, for the worst case combination of all reflecting terms at the highest PAM amplitude, zero error rate, Extinction Ratio E = 4 (6 dB), dual-trunk cabling, 4 connectors (six reflectance points, N = 15), m = number of PAM amplitude levels. Results do not include the effect of backscatter.

R (dB)	PAM-2	PAM-4	PAM-8	PAM-16
-26	0.97	4.01		
-30	0.36	1.19	3.57	
-35	0.11	0.34	0.85	2.07
-40	0.03	0.11	0.25	0.56

Assuming $I_{i(t)}=I_m$ and then applying the flat penalty to all levels is too pessimistic. Lets model the amplitude dependent MPI.

Using $R_{ROSA}=R_{TOSA}=R_{Conn}=-35$ dB ,4 connectors and 6dB ER, below graph shows level-dependent MPI penalty



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Lets make the "Upper Bound" Analysis more statistical by taking into account the fact that interfering signals have random optical amplitude rather than always staying at maximum. Let's call this "Statistical Upper Bound method"

Refine the following pessimistic assumption **Pessimistic Assumption 6**: Assume all interfering signals are at their maximum

We are going to assume the sum of all interfering sources are going to look more like "Normal" distribution $\chi(\mu_m, \sigma_m^2)$

•This assumption is a good estimate if there are more connectors (ie 4). Keep in mind that the more connectors, the more the MPI impact so 4 connector is a reasonable assumption.

• It is a good estimate if the Connector RL, TOSA RL and ROSA RL are close to each other.

We call this type of analysis "Statistical Upper Bound" not to be confused with Minneapolis time domain simulations.

The following table shows PAM16,8 and 4 mean and variance with ER=6dB assuming a peak vale of 1.

Modulation	Mean µ _m	Variance σ_m^2
PAM16	7.76E-1	2.29E-2
PAM8	7.74E-1	2.62E-2
PAM4	7.69E-1	4.03E-2

Start from original equation

 $e(t)=A_{i(t)}e^{jwt}+e^{j(wt+\theta)}\sum A_{k(t)}\sqrt{(R_{k1}R_{k2})}$

Replace the sum $\sum A_{k(t)} \sqrt{(R_{k1}R_{k2})}$ with the variable $\chi(\mu_{scale} \mu_m, \sigma^2_{scale} \sigma_m^2)$ which takes into account proper scaling of μ_m and σ_m^2 as function of $R_{k1}R_{k2}$.

 $\mu_{\text{scale}} = n(n-1)R_{\text{Conn}}/2 + n\sqrt{(R_{\text{Conn}}R_{\text{TOSA}}) + n\sqrt{(R_{\text{Conn}}R_{\text{ROSA}}) + \sqrt{(R_{\text{TOSA}}R_{\text{ROSA}})}} \sigma^2_{\text{scale}} = n(n-1)R_{\text{Conn}}^2/2 + nR_{\text{Conn}}R_{\text{TOSA}} + nR_{\text{Conn}}R_{\text{ROSA}} + R_{\text{TOSA}}R_{\text{ROSA}} + R_{\text{TOSA}}R_{\text{ROSA}} + nR_{\text{CON}}R_{\text{ROSA}} + R_{\text{TOSA}}R_{\text{ROSA}} + nR_{\text{CON}}R_{\text{ROSA}} + nR_{\text{CON}}R_{\text{ROSA}} + nR_{\text{CON}}R_{\text{ROSA}} + nR_{\text{ROSA}} +$

 $\mathbf{e}(\mathbf{t}) = \mathbf{A}_{i(t)} \mathbf{e}^{jwt} + \mathbf{e}^{j(wt+\theta)} \chi(\mu_{\text{scale}} \mu_{\text{m}}, \sigma^2_{\text{scale}} \sigma_{\text{m}}^2)$

The receive current is proportional to $I(t) \propto |e(t)|^{2} = A_{i(t)}^{2} + 2A_{i(t)} \chi(\mu_{scale} \ \mu_{m}, \ \sigma^{2}_{scale} \ \sigma_{m}^{2}) \cos(\theta) + \chi(\mu_{scale} \ \mu_{m}, \ \sigma^{2}_{scale} \ \sigma_{m}^{2})^{2}$

It is safe to assume $\chi(\mu_{scale} \ \mu_m, \sigma^2_{scale} \ \sigma_m^2)^2$ is very small and can be omitted. $I(t) \ \propto | \ e(t) |^2 = A_{i(t)}^2 + 2A_{i(t)} \ \chi(\mu_{scale} \ \mu_m, \sigma^2_{scale} \ \sigma_m^2) \ Cos(\theta)$ $I(t) \ \propto I_{i(t)} + 2 \ \chi(\mu_{scale} \ \mu_m, \sigma^2_{scale} \ \sigma_m^2) \ Cos(\theta) \ \sqrt{I_{i(t)}}$

And finally the MPI noise is

 $\begin{array}{l} \mathsf{MPI_Eye_Closure_Mean=2} \ \mu_{scale} \ \mu_{m} \ \mathsf{Cos}(\theta) \\ \forall \mathsf{I}_{i(t)} \\ \mathsf{MPI_Eye_additive_noise=2} \ \chi(0, \ \sigma^{2} \ _{scale} \ \sigma_{m}^{\ 2}) \ \mathsf{Cos}(\theta) \\ \forall \mathsf{I}_{i(t)} \end{array}$

•The worst case MPI happens for all levels from 2 to m-1 when Cos θ is +1 or -1. For level 1 the worst case is when Cos θ is +1 and for level m the worst case is when Cos θ is -1.

•Since the MPI is amplitude dependent, the penalty for level 1 is pretty small.

Pessimistic assumption 7: Cos θ=-1

 $\mu_{\text{scale}} = n(n-1)R_{\text{Conn}}/2 + n\sqrt{(R_{\text{Conn}}R_{\text{TOSA}}) + n\sqrt{(R_{\text{Conn}}R_{\text{ROSA}}) + \sqrt{(R_{\text{TOSA}}R_{\text{ROSA}})}} \sigma^2_{\text{scale}} = n(n-1)R_{\text{Conn}}^2/2 + nR_{\text{Conn}}R_{\text{TOSA}} + nR_{\text{Conn}}R_{\text{ROSA}} + R_{\text{TOSA}}R_{\text{ROSA}} + R_{\text{TOSA}}R_{\text{ROSA}} + nR_{\text{CON}}R_{\text{ROSA}} + R_{\text{TOSA}}R_{\text{ROSA}} + nR_{\text{CON}}R_{\text{ROSA}} + nR_{\text{CON}}R_{\text{ROSA}} + nR_{\text{ROSA}} + nR_{\text{ROS$

MPI_Eye_Closure_Mean=-2 $\mu_{scale} \mu_m \sqrt{I_{i(t)}}$ MPI_additive_noise=2 $\chi(0, \sigma^2_{scale} \sigma_m^2) \sqrt{I_{i(t)}}$

It is reasonable to practically ignore the MPI additive noise component since it is very small. For example, assuming $R_{ROSA}=R_{TOSA}=R_{Conn}=-35$ dB and ER=6dB and assuming $I_{i(t)}=I_m$, below table shows MPI noise component for different PAM modulation schemes.

PAM modulation order	MPI noise limited RX SNR
PAM-16	36.6dB
PAM-8	43.2dB
PAM-4	50.6dB

 $\mu_{\text{scale}} = n(n-1)R_{\text{Conn}}/2 + n\sqrt{(R_{\text{Conn}}R_{\text{TOSA}})} + n\sqrt{(R_{\text{Conn}}R_{\text{ROSA}})} + \sqrt{(R_{\text{TOSA}}R_{\text{ROSA}})}$

MPI_Eye_Closure_Mean=-2 $\mu_{scale} \mu_m \sqrt{I_{i(t)}}$

Using $R_{ROSA}=R_{TOSA}=R_{Conn}=-35$ dB ,4 connectors and 6dB ER, below graph shows level-dependent MPI penalty



Using R_{ROSA}=R_{TOSA}=R_{Conn}=-35dB ,4 connectors and 6dB ER, the table below shows the **maximum** statistical upper bound MPI penalty compared to Bhatt_01_0512 Upper Bound method MPI penalty

PAM order	Bhatt_01_0512 Upper Bound MPI penalty	Max Statistical Upper Bound MPI penalty	Delta for the upper Eye
PAM-16	2.07 dB	1.52 dB	0.55 dB
PAM-8	0.85 dB	0.64 dB	0.19 dB
PAM-4	0.34 dB	0.26 dB	0.08 dB

The statistical upper bound method does result in some saving. However, the bigger part of the saving comes from correct modeling of amplitude dependent MPI as shown earlier in this presentation.

To understand the impact of the MPI on the slicer SNR, lets use the following method

• Similar to RIN and Shot noise, MPI Penalty is amplitude dependent. The higher the amplitude, the more MPI penalty is.

• There are other noise components such as TX electrical noise, TIA thermal noise and RX electrical noise that are not amplitude dependent

• The combination of the above noise sources make the segment SNR to look very close to a linear ramp going from value *a* to *b* starting from lowest eye to the highest eye. Assuming 1.5dB SNR change from *a* to *b*, is a good typical assumption for demonstration purposes

• Because the segment SNR varies as a function of segment number, each segment will make a different contribution to Symbol-Error-Rate (SER)

• The overall SER of the system is the average of all the segment SERs.

• The average SER can then be converted back to the "Effective SNR" for the modulation order under investigation.

• We then calculate the Effective SNR with and without MPI and define MPI Electrical SNR penalty as

"MPI Electrical SNR Penalty"="Effective Slicer SNR without MPI"-"Effective Slicer SNR with MPI"

Using R_{ROSA}=R_{TOSA}=R_{Conn}=-35dB ,4 connectors and 6dB ER, SNR ramp with 1.5dB delta, below graph shows MPI Electrical SNR Penalty for different PAM options at different "Effective SNR without MPI"



• As shown in the above graph, if the Slicer SNR was 22.5dB before MPI, with MPI if will be reduced by **0.26dB to 0.51dB** as a function of PAM modulation order. This is a manageable penalty.

• For slicer SNR of 28dB the PAM16 MPI Electrical SNR penalty is **1.4dB**. (for PAM16 to work with bj FEC, Slicer SNR should be actually bigger than 31dB)

Field Measurements

• Pete Anslow provided anslow_02_1012_smf presentation that analyses reflectance measurement over 650 links

• The data was collected from 8 operators measured between 2003 to 2005.

• Because these were, in general, fairly long links it can be assumed that reflections from connectors at the far end of the link (or part way down for multi-segment links) are negligible due to the loss of the fiber. In most cases, the measurement is likely to be dominated by a single connector pair at an optical distribution frame prior to the buried cable.

• A graph of the cumulative distribution for link optical return loss is shown



Installed link return loss

Field Measurements

- A high resolution Cumulative-Mass-Function (CMF) was extracted from the provided graph
- 4000 random return-loss values were generated using the CMF to represent 1000 links with 4 connectors
- ROSA/TOSA return-loss was assumed to be fixed -35dB and ER was set to 6dB
- Statistical Upper Bound method was used to calculate worst case MPI penalty for PAM4 and PAM8



MPI Statistical Upper Bound Max Penalty for RL=-35dB and ER=6dB was **0.26dB** for PAM4 and **0.64dB** for PAM8

Field Measurements

Using R_{ROSA}=R_{TOSA}=R_{Conn}=-35dB ,4 connectors and 6dB ER, SNR ramp with 1.5dB delta, below graph shows MPI Electrical SNR Penalty for PAM-4 and PAM8 options for 22.5dB "Effective SNR without MPI"



SNR without MPI of 22.5dB

Summary

• We started from Bhatt_01_0512 upper bound analysis method for MPI and refined it by introducing an improved statistical method, while preserving the conservative approach.

• We recommend to adopt the ISO 11801 return-loss spec to -35dB as stated in Bhatt_01_0512.

• We showed that with -35dB RL, for a reasonable slicer SNR assumption of around 22.5dB, the MPI impact is manageable.

Potential Future Work

• In this presentation we assumed a perfect Coherent Laser with zero line-width

• We then assumed all interfering noise sources are perfectly aligned in phase and polarization

• It is worth investigating if substantial improvement can be made by modeling the above two pessimistic assumptions more accurately

• Investigate the degree of prevalence of ISO 11801 compliant (-35 dB connector return loss) fiber plant in today's data centers.