

Measurement and Estimation of the Mode Partition Coefficient k

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Background & Objective

● **Background:**

- *Mode Partition Noise in MMF channel links is caused by pulse-to-pulse power fluctuations among VCSEL modes and differential delay due to dispersion in the fiber (Power independent penalty)*
- *“k” is an index used to describe the degree of mode fluctuations and takes on a value between 0 and 1, called the mode partition coefficient [1,2]*
- *Currently the IEEE link model assumes $k = 0.3$*
- *It has been discussed that a new link model requires validation of k*
- *The measurement & estimation of k is challenging due to several conditions:*
 - *Low sensitivity of detectors at 850nm*
 - *The presence of additional noise components in VCSEL-MMF channels (RIN, MN, Jitter – intensity fluctuations, reflection noise, thermal noise, ...)*
 - *Differences in VCSEL designs*

● **Objective:**

- *Provide an experimental estimate of the value of k for VCSELs*
- *Additional work in progress*

MPN Theory

Originally derived for Fabry-Perot lasers and SMF [3]

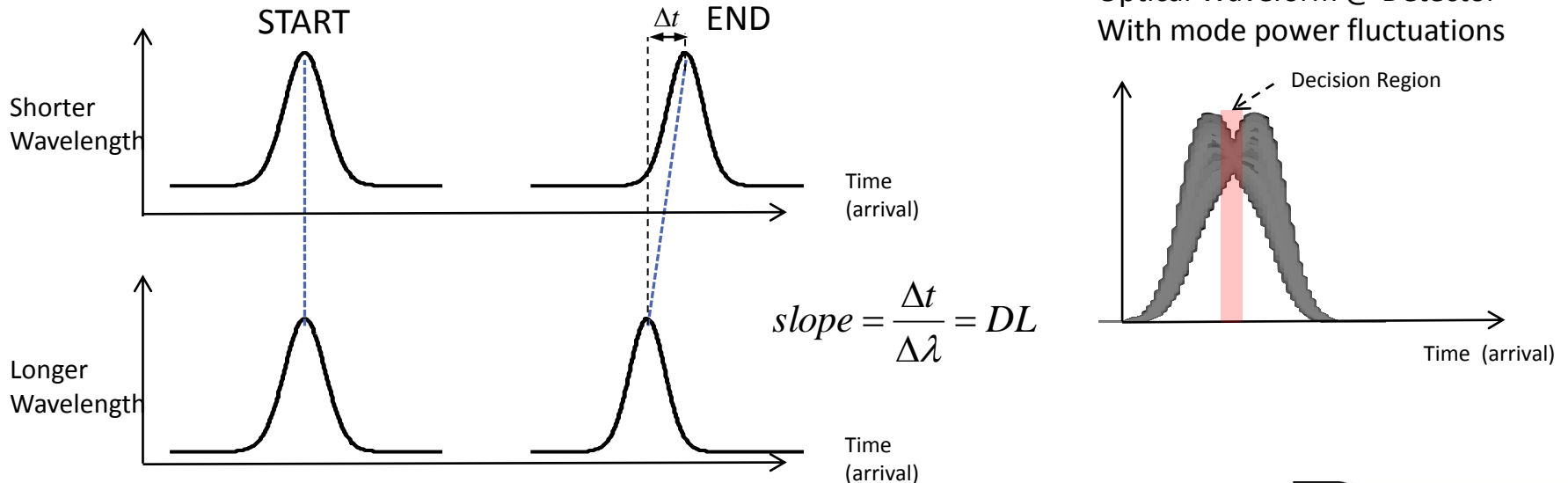
- **Assumptions:**

- Total power of all modes carried by each pulse is constant
- Power fluctuations among modes are anti-correlated

- **Mechanism:**

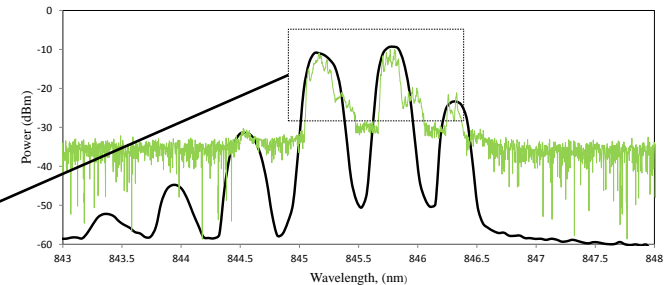
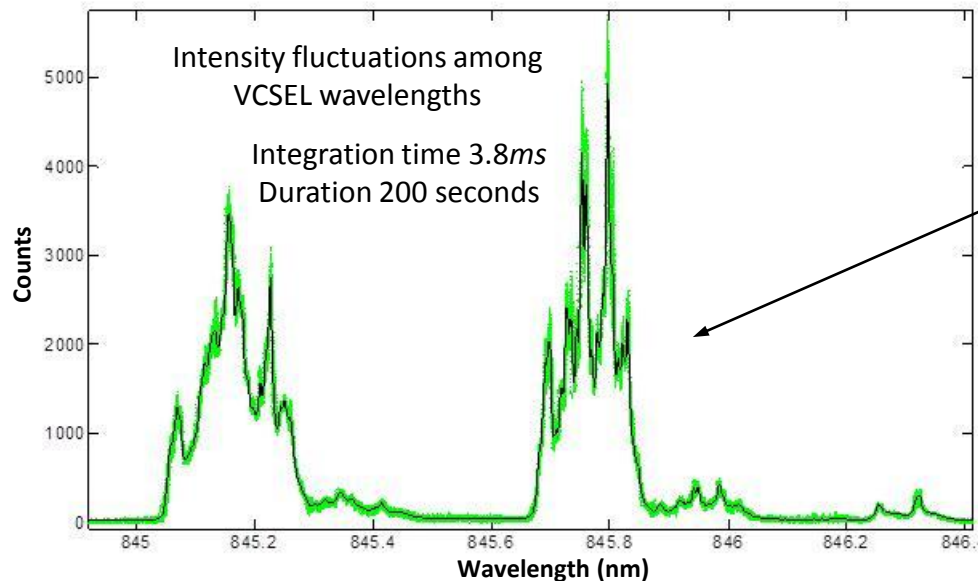
- When modes (different wavelengths) travel at the same speed their fluctuations remain anti-correlated and the resultant pulse-to-pulse noise is zero.
- When modes travel in a dispersive medium the modes undergo different delays resulting in pulse distortions and a noise penalty.

- **Example:** Two VCSEL modes transmitted in a SMF undergoing chromatic dispersion:



Example of Intensity Fluctuation among VCSEL modes

- MPN can be observed using an Optical Spectrum Analyzer (OSA).
- Measurements require a detector with high sensitivity and high bandwidth, and a means of isolating other noise components.
- The Figure below shows the optical spectrum of a 16GFC transceiver
 - Green traces are 100 VCSEL spectral measurements at ~2 second intervals
 - Black trace is the average spectrum
 - Noise can be observed but a slow detector does not provide a means of estimating the magnitude



- High Resolution OSA (0.005nm)
- Low Sensitivity
- Linear amplitude
- 3.8ms integration time (min)
- Two VCSEL "Mode Sets"

Measurement Methods

● **Two methods used to measure k :**

1. *Monochromator and APD measurements (equivalent to OSA)*

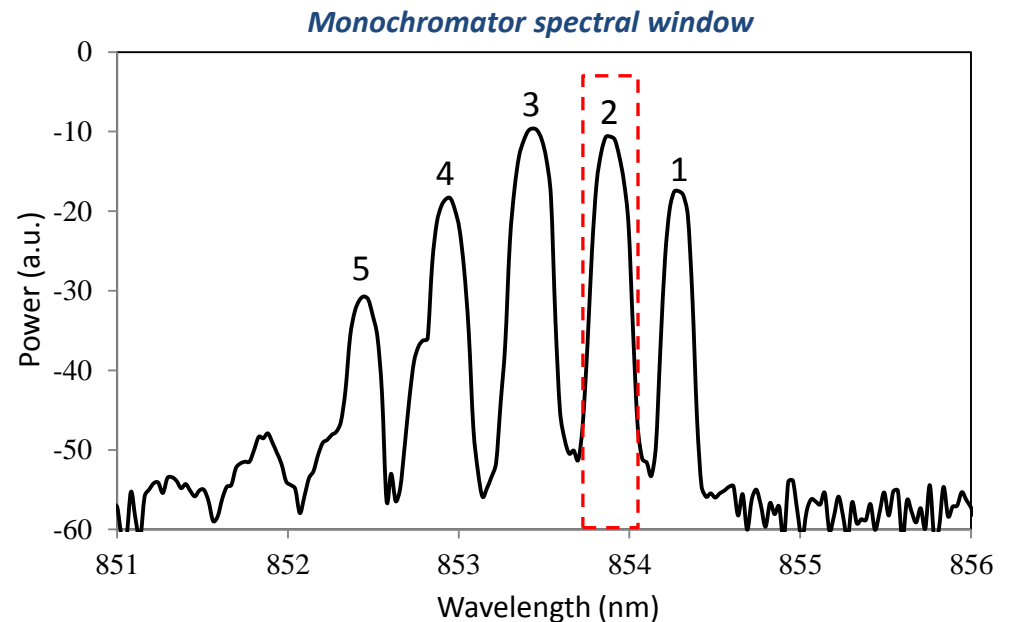
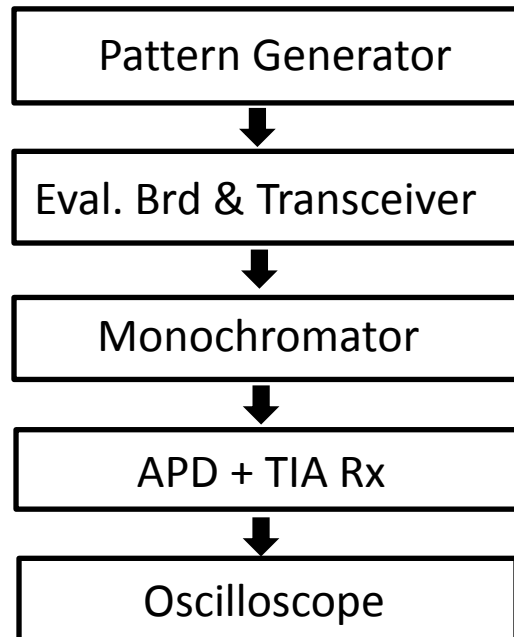
- *High sensitivity*
- *Bandwidth limited by APD*
- *Fast transceivers were modulated at lower rates*
- *Could not measure MPN for response rates $>2.5\text{Gbps}$*
- *Short length used (5m) to avoid dispersion effects*

2. *Temporal measurements in the spectral domain – specific data patterns measured at 16G data rates*

- *Useful for evaluating noise dependence on transmitted pattern [4,5]*
- *Fast detector – enables measurements at high bit rates (i.e. 14.025Gbps for 16GFC)*
- *Short lengths used (5m) to avoid dispersion effects*
- *Lower sensitivity must be compensated by increasing measurement time i.e., sample size*
- *Need to estimate the noise introduced by other noise components*

Method 1: Monochromator–APD measurement

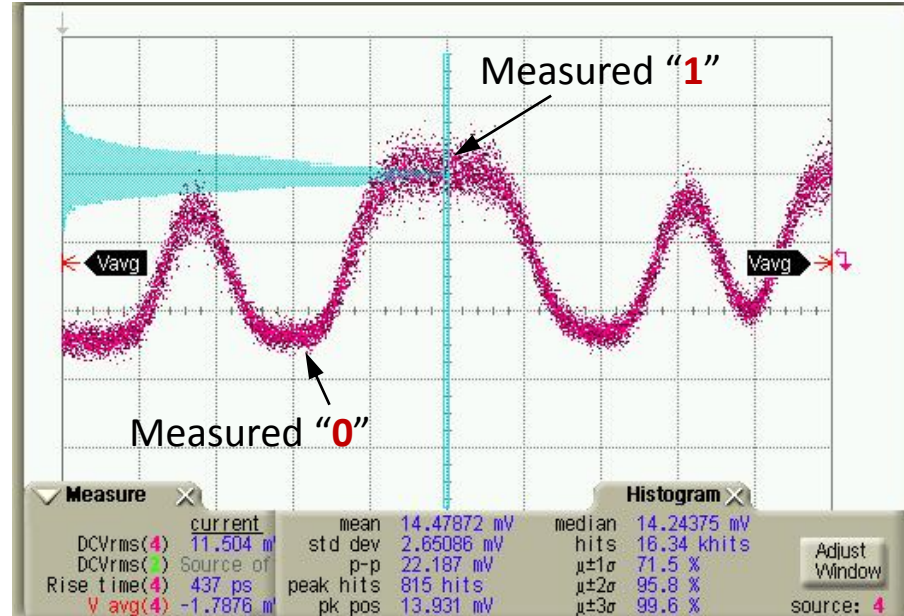
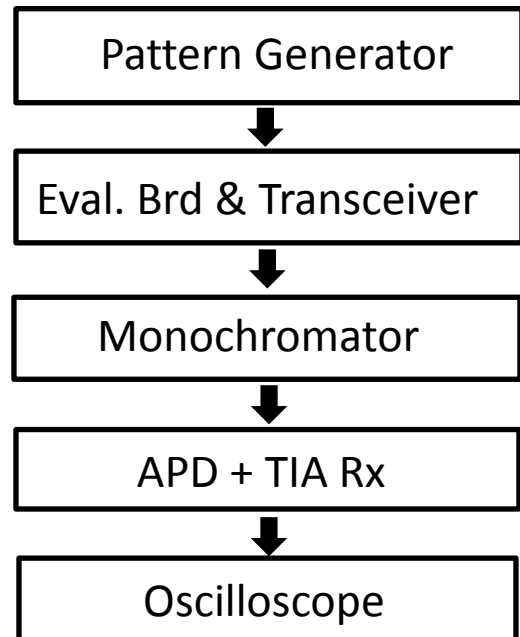
- Signal measured using an APD ($M > 40$).
- Modulation rate limited to $< 2.5\text{Gbps}$ due to APD bandwidth (180ps rise time).
- VCSEL spectra separated into VCSEL Mode Sets (MS's). In practice only 4 MS's could be measured due to low power levels
- Light from the transceiver was filtered using a tunable monochromator with a spectral resolution between 0.2nm – 0.5nm
- Oscilloscope used to obtain the signal histogram for specific bits in the sequence



Method 1: Monochromator–APD measurement

- Used PRBS 2^7-1 bit pattern
- For consistency only the zero and one bits shown in red in the following sequence were measured. "...10**0**1**1**1001..."

➔ Measured signal level histogram away from pulse edges



Time scale: 500ps/div

Y-axis in mV

Method 1: Monochromator–APD Calculation

- Computation using [2]:

$$k = \sqrt{\frac{\overline{a_i^2} - (\overline{a_i})^2}{\overline{a_i} - (\overline{a_i})^2}}$$

for any mode set i

- Where a_i and $\overline{a_i^2}$ are the normalized mean powers of each peak (measured as rms voltage) and the rms variation respectively, after subtracting the background noise SD (0.89mV).
- All OMA measurements limited to <2.5Gbps due to APD bandwidth limitations

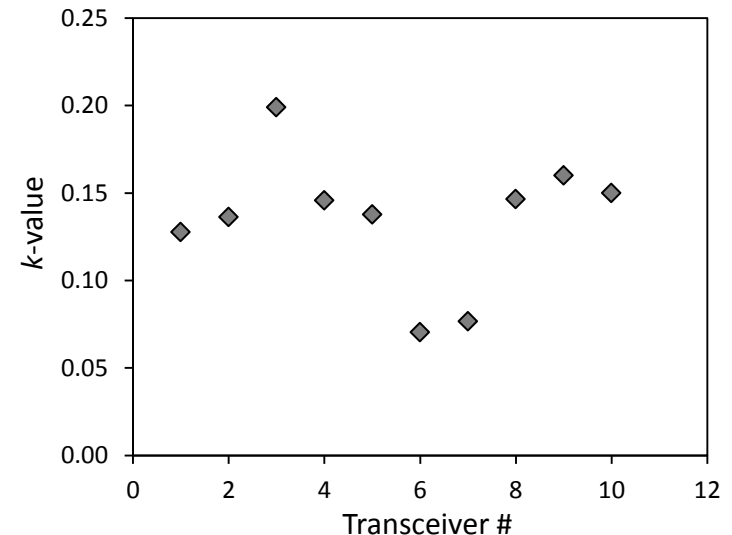
Computation Example

MS	MEAN (mV)	SD (mV)	a_i	SD a_i	k
1	~0.000	0.850	~0.000	~0.000	---
2	26.017	2.500	0.419	0.038	0.077
3	26.910	3.200	0.433	0.050	0.100
4	9.214	1.570	0.148	0.021	0.060

Total Power (V_{rms}) = 62.14mV

Max. k = 0.1

Maximum k for each transceiver



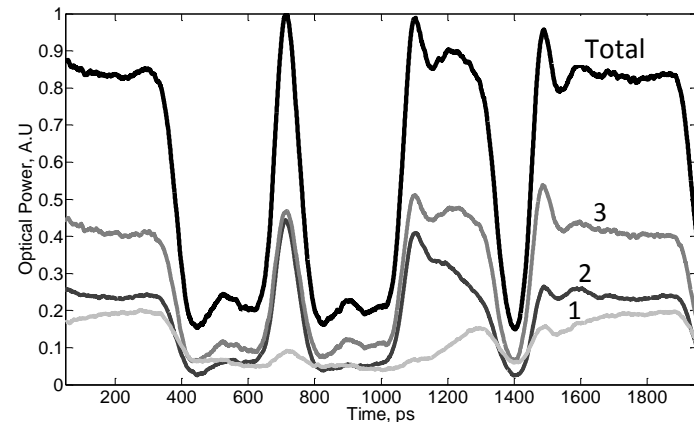
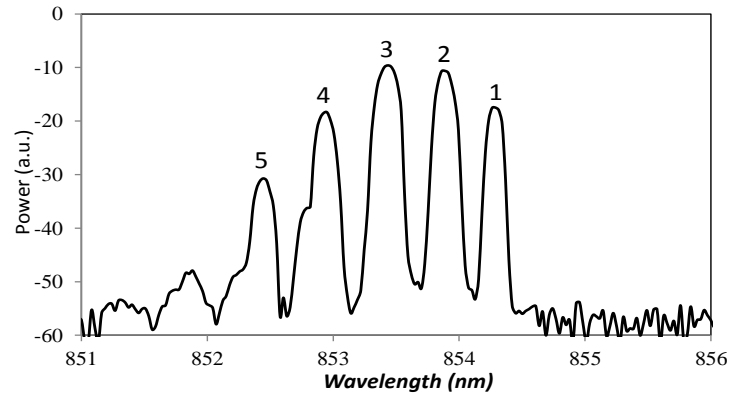
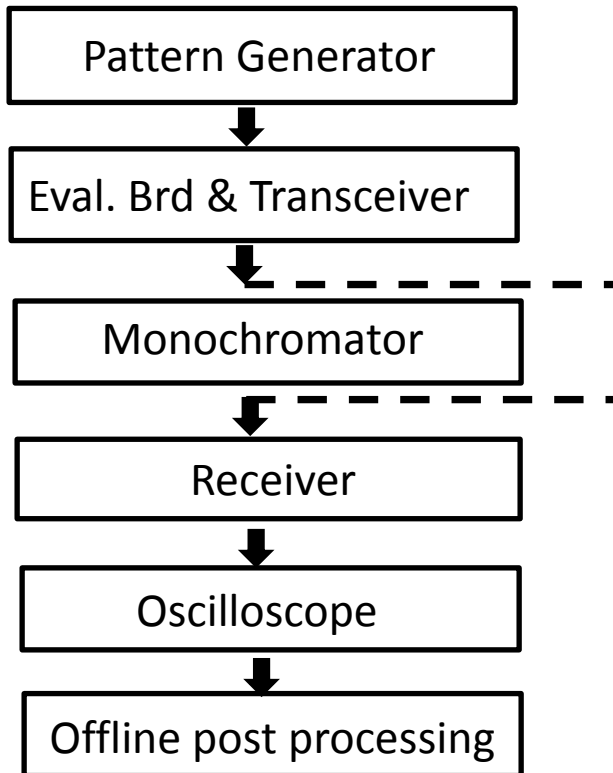
Method 1: Measurement Issues

- *Limited APD bandwidth (2.5Gbps) might result in a lower value for k (filters high frequency noise).*
- *Are the 16G transceivers operating properly at 2.5Gbps, or are we introducing additional noise?*
- *Is a correction required to extrapolate to 14Gbps?*
 - *Based on theory [2] the noise variance should be scaled.*
 - *However, in order to apply scaling, we must assume how the MPN spectrum behaves above the cutoff frequency.*
 - *It is challenging to use the laser rate equations to predict the noise spectrum above cutoff for the individual transceivers measured.*
- *All these questions indicate an alternative method in which the transceivers operate at the specified line rate is required.*

Method 2: Temporal-Spectral characterization using a fast detector and post processing

● Procedure

- The transceiver is modulated with a specific bit pattern
- Resultant waveforms measured for 5m to 1km lengths with and without monochromator
- The measurements reported here are for 5m
- Sampling Oscilloscope with high bandwidth optical plug-in
- The oscilloscope acquired the waveforms and sent them to a computer for processing



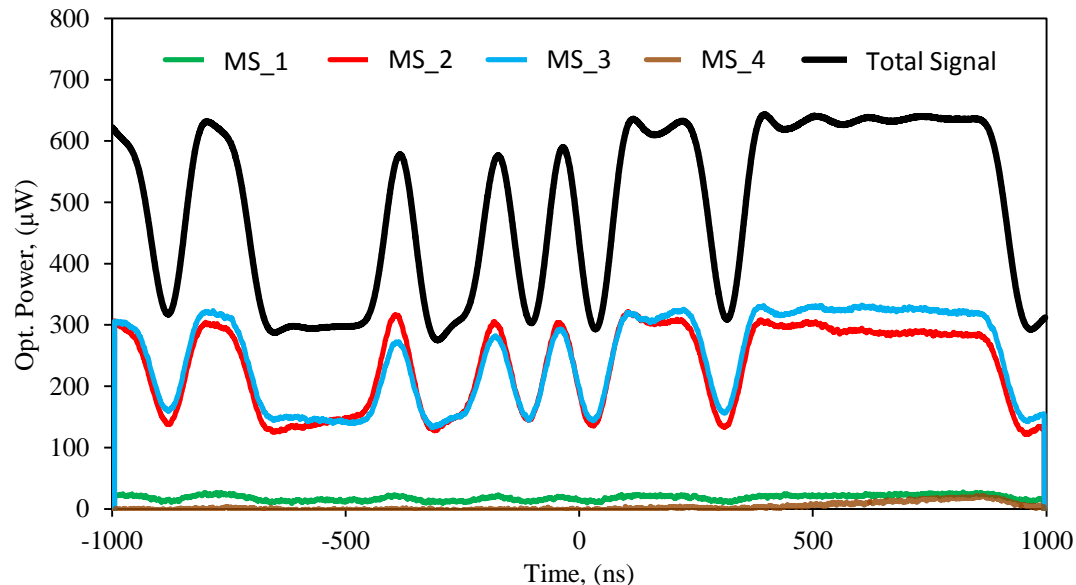
Method 2: Signal acquisition

● Test Equipment Characteristics

- Sources: 16GFC Transceivers (clock 14.025GHz)
- Linear Receiver: DCA plug-in, 12GHz BW
- Sampling Oscilloscope DCA 861000, temporal resolution = 0.5ps

● Acquisition Procedure

- The chromatic unfiltered signal (black trace) was measured
- The signals for 4 VCSEL mode sets were acquired using the monochromator (colored traces)
- Signals were compensated for measurement noise and monochromator loss



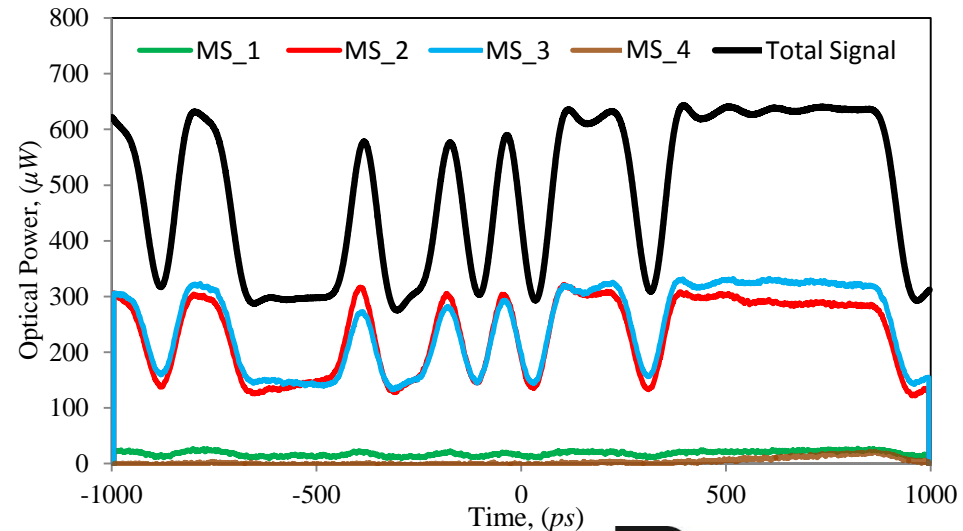
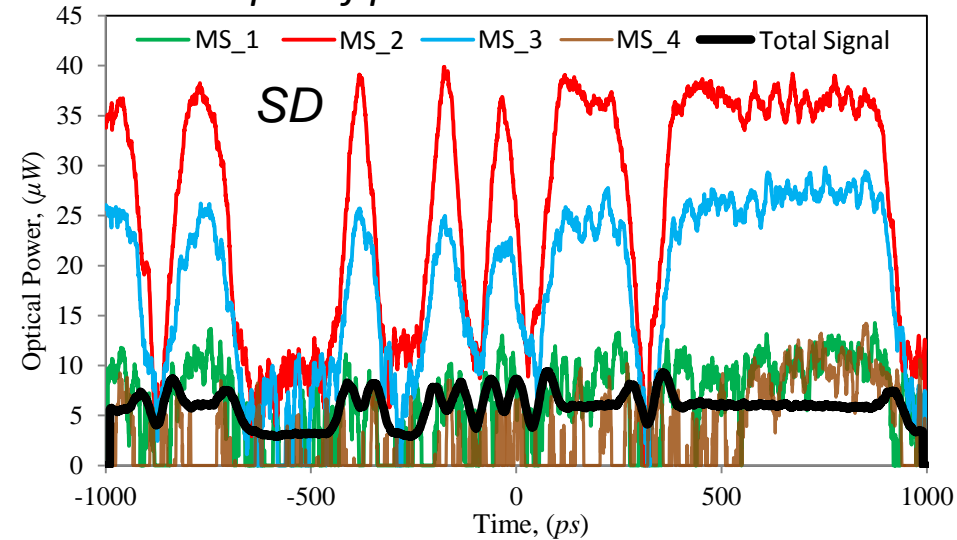
Method 2: Procedure

● Noise Computation Procedure

- >500 signal waveforms were captured for each MS
- The standard deviation (SD) for each MS signal was computed every 0.5ps
- The SD of the total signal (black trace in Top Fig.) is less than the noise in any one VCSEL MS signal
- This is attributed to the high degree of anti-correlation among VCSEL modes [2]
- There are other noise components in the total noise including thermal, jitter-intensity fluctuations, RIN, ...
- Using this measurement method the maximum k is ~ 0.22

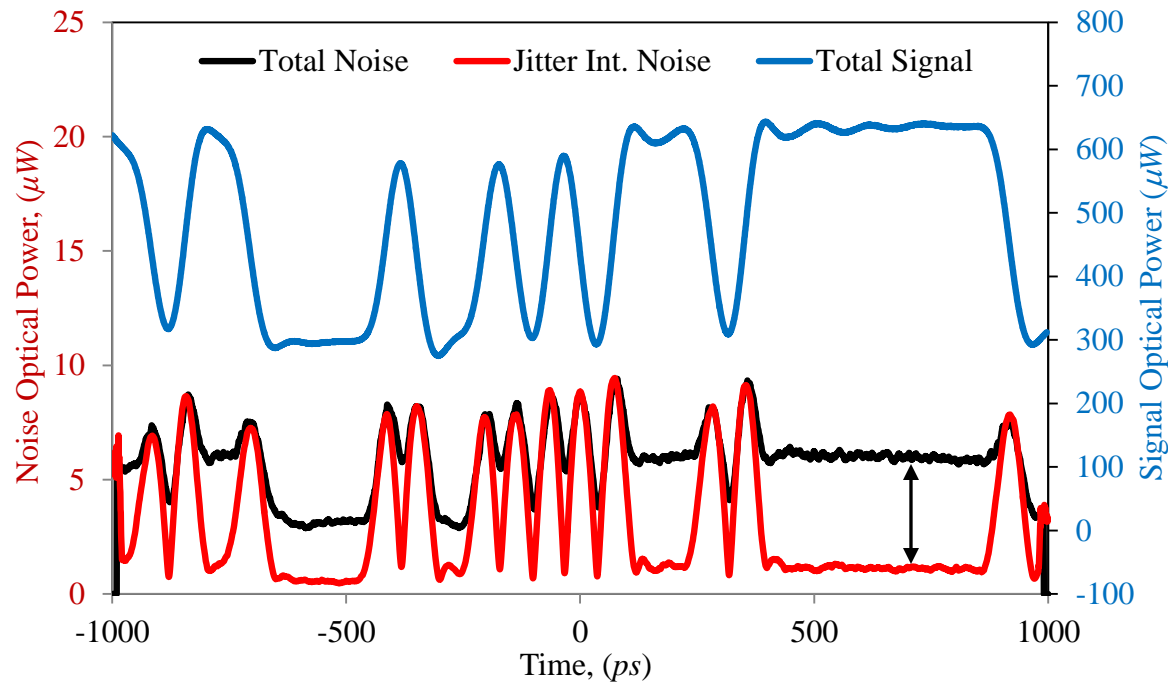
$$k = \sqrt{\frac{\overline{a_i^2} - (\overline{a_i})^2}{\overline{a_i} - (\overline{a_i})^2}}$$

Example of processed Measurements



Method 2: Noise considerations

- The Random and Deterministic Jitter was measured, used RJ for noise calculations.
- The signal waveform and measured jitter was used to calculate the jitter-intensity noise (red trace). Method to be published.
- It can be observed that the jitter-intensity noise matches the total noise at the pulse edges.
- The magnitude of the noise contributions due to RIN and other noise components can be obtained by subtracting the jitter-intensity noise (red trace) from the total noise (black trace). The difference is indicated by the double arrow.
- Close inspection of the jitter-intensity noise and the total noise suggests the remainder of noise is proportional to signal intensity.



Conclusions

- **Two methods were used to measure k :**
 - *Measurements made at 2.5Gbps and 14Gbps*
 - *Both methods yield similar values for k*
 - *Method 1, monochromator and APD:*
 - *The maximum value for k was measured to be 0.20*
 - *Method 2, Temporal-Spectral characterization:*
 - *The maximum value for k was measured to be 0.22*
- **The current value for k (0.3) is reasonable, but might be conservative**
 - *A value 0.25 could be more accurate*
 - *Additional work underway*
 - *Larger transceiver sample set*
 - *MPN over long lengths*
 - *Effect of modal-chromatic dispersion and spectral mode coupling [6]*

References

- [1] K. Ogawa, “Analysis of Mode Partition Noise in Laser Transmission Systems, *IEEE J. Quantum Electron.*, vol. QE-18, no. 5, May 1982.
- [2] K. Ogawa and R.S. Vodhanel, “Measurements of Mode Partition Noise of Laser Diodes,” *IEEE J. Quantum Electron.*, vol. QE-18, No. 7, July 1982.
- [3] G. Agrawal, P. Anthony, and T. Shen, “Dispersion Penalty for 1.3- μ m Lightwave Systems with Multimode Semiconductor Lasers,” *J. Lightwave Technol.*, vol. 6, no. 5, May 1988.
- [4] P. Pepeljugoski, “Dynamic Behavior of Mode Partition Noise in Multimode Fiber Links,” *IEEE J. Lightwave Technol.*, vol. 30, no. 15, August 2012.
- [5] J. Castro, R. Pimpinella, B. Kose, and B. Lane, “The Interaction of Modal and Chromatic Dispersion in VCSEL based Multimode Fiber Channel Links and its Effect on Mode Partition Noise,” *Proceedings of the 61 IWCS 2012*.
- [6] J. Castro, R. Pimpinella, B. Kose, and B. Lane, “Investigation of the Interaction of Modal and Chromatic Dispersion in VCSEL-MMF Channels,” *J. Lightwave Technol.*, vol. 30, no. 15, August 2012