

# **Practical Device Test Fixtures for 100G KR ... or Not and the Impact on ERL and $P_{\max}/V_f$ (ref: comment 19, 20, 21, 25)**

Richard Mellitz, Samtec

Mike Li, Masashi Shimanouchi, Hsinho Wu, Intel

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# Agenda

- ❑ Test fixture background
- ❑ Impact of small perturbations on hypothetical test fixtures
- ❑ Measurement variability due to a few simple UUT (package) impedance variations across the hypothetical fixtures
- ❑ Realistic device variations suggest  $ERL_{\min}$  and  $P_{\max}/V_f$  specs
- ❑ Summary/Recommendation

# The Test Fixture Reference was Basically a Transmission Line

Clause 93

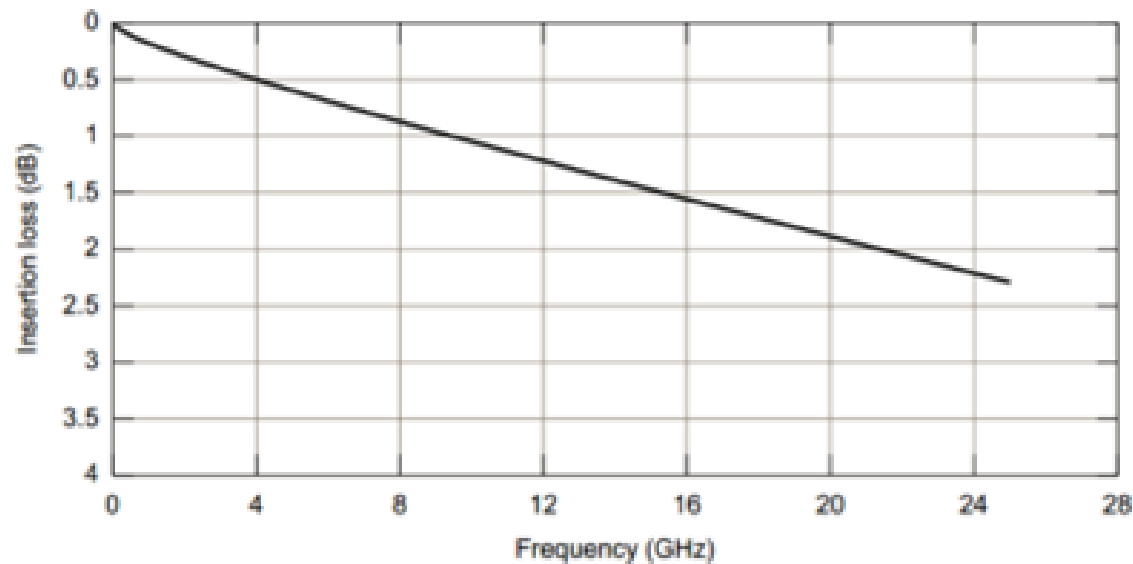


Figure 93-3—Test fixture reference insertion loss

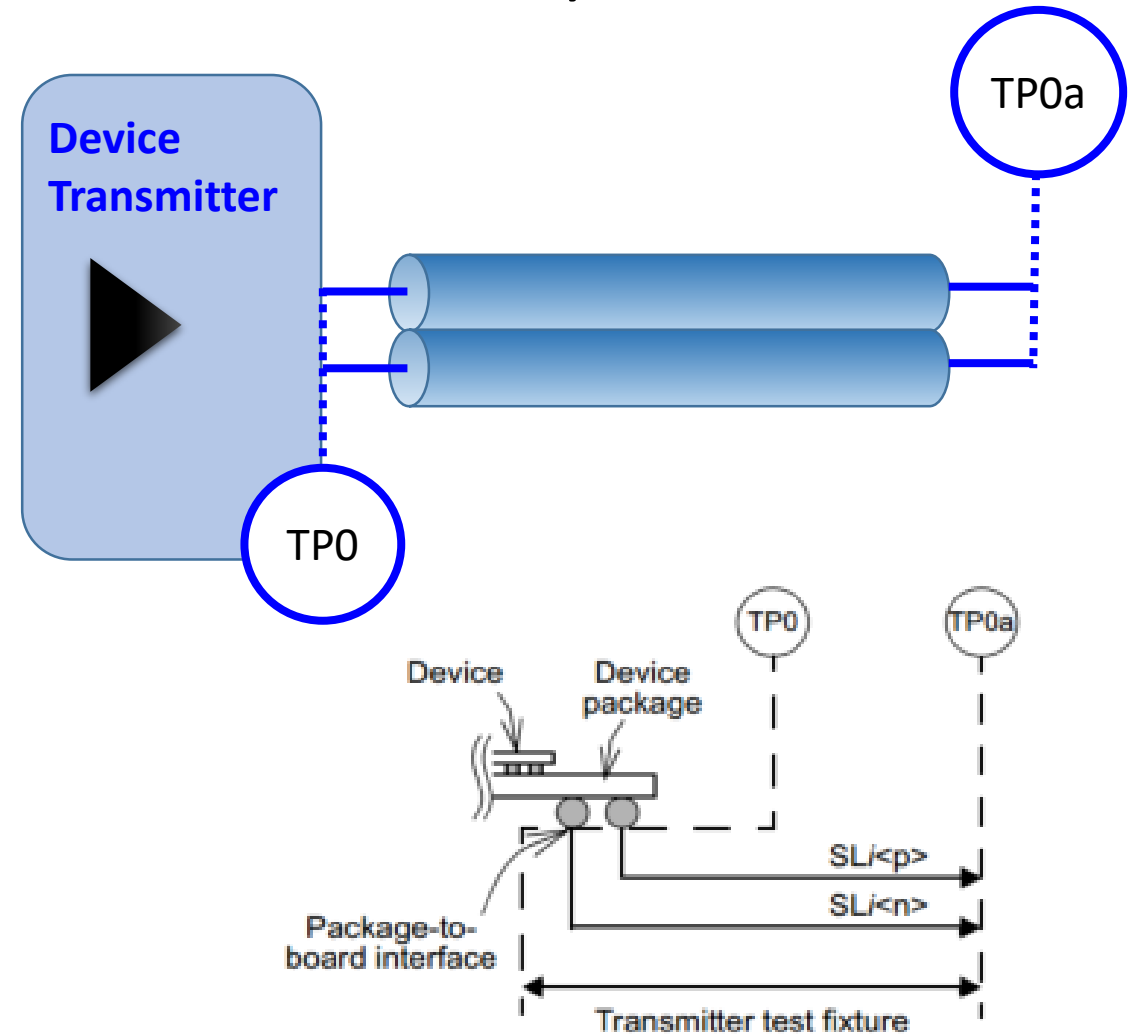
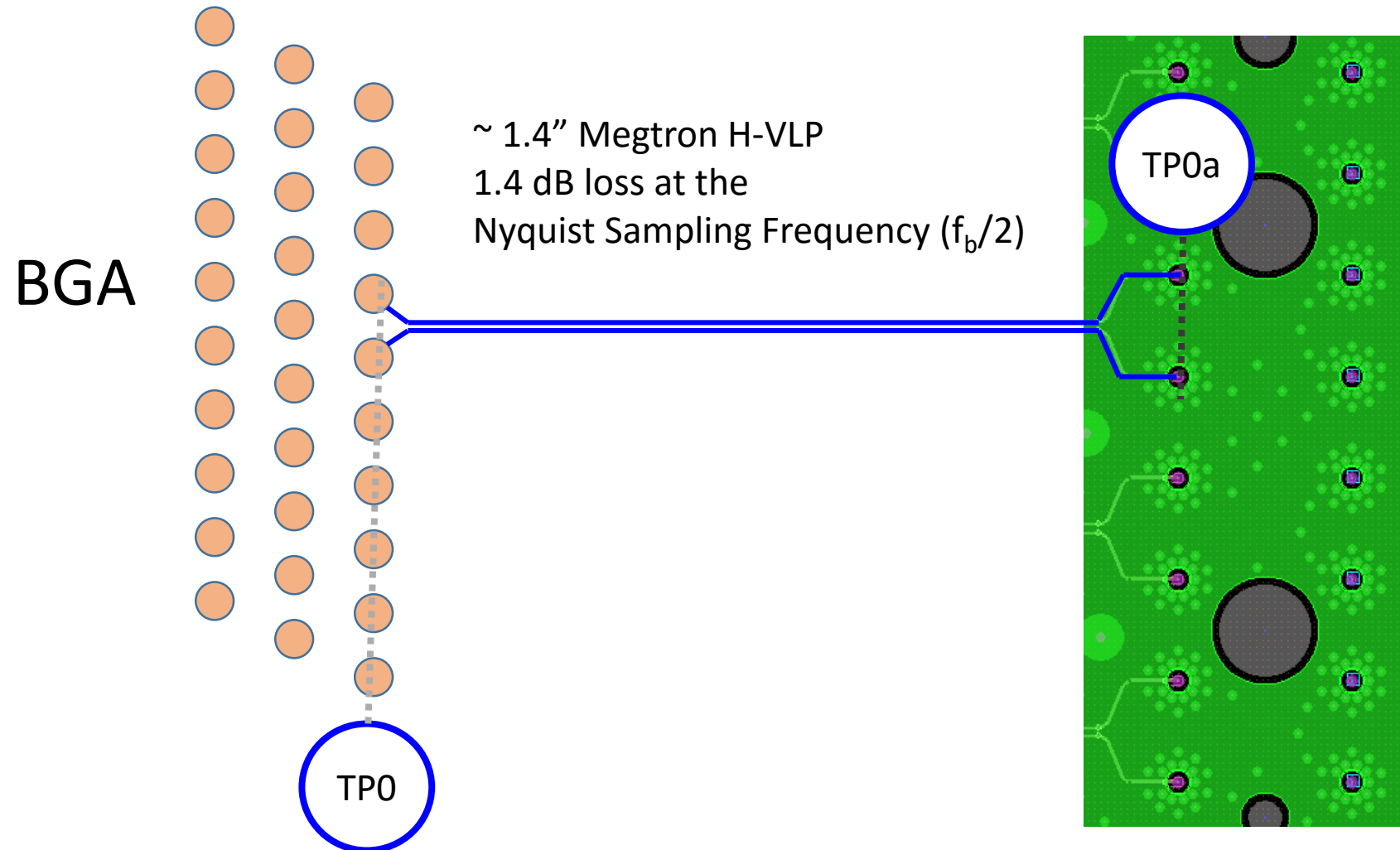
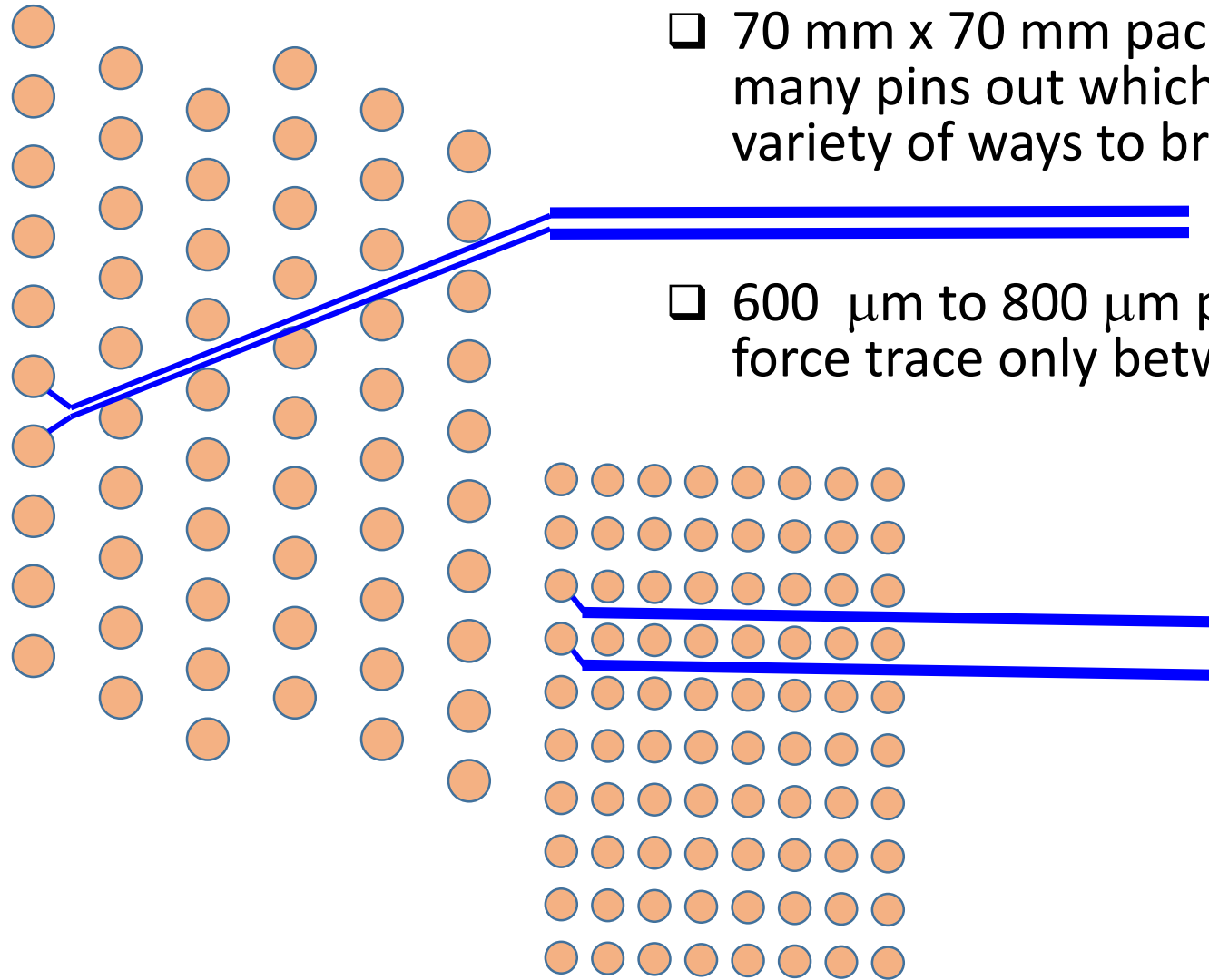


Figure 93-5—Transmitter test fixture and test points

# Ideally a Test Fixture Layout Might Look Like This



# Variability does exist



## Thoughts for practical fixtures

- ❑ Limit loss at  $(f_b/2)$  to be between 1.2 and 1.6 dB
- ❑ Limit return loss
- ❑ Limit IL ripple to 0.1 dB
  - Called  $\text{FOM}_{\text{ILD}}$

# Variability is allowed ... BUT

Clause 93

$$IL_{ref}(f) = -0.0015 + 0.144\sqrt{f} + 0.069f \text{ dB} \quad 0.05 \leq f \leq 25 \quad (93-1)$$

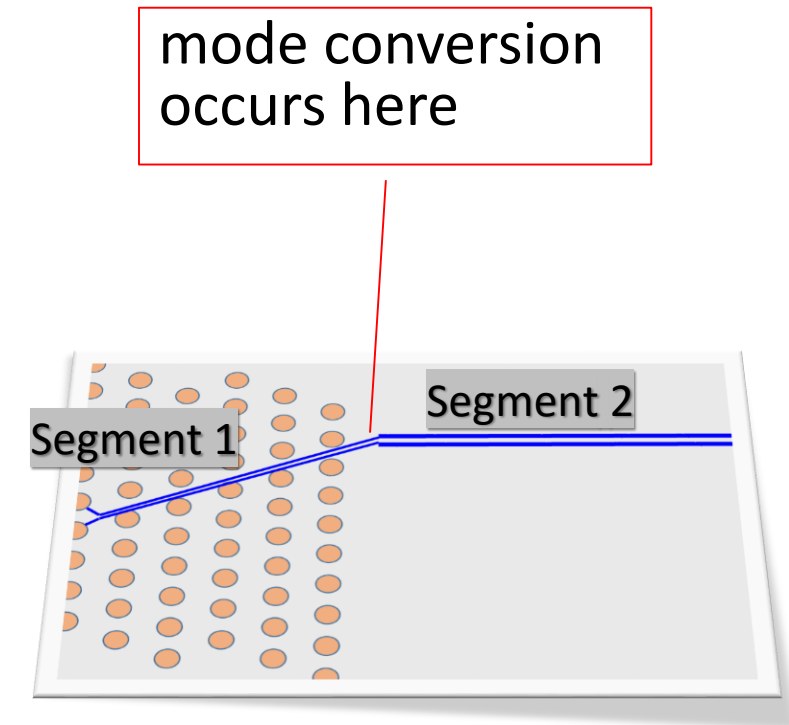
The effects of differences between the insertion loss of an actual test fixture and the reference insertion loss are to be accounted for in the measurements. The reference insertion loss is illustrated in Figure 93-3.

- ❑ The standard allows variability but specs are for the **exact** reference fixture.
- ❑ It's the implementer responsibility to adjust
  - “The bridge doesn't care that the truck height has variability”
- ❑ Question:
  - How much margin does a perfect fixture cost?



# Hypothetical Fixture Models Used To Investigate Examples Of Variability

- ❑ 1.4 dB at 100 ohm (differential) Megtron 7 H-VLP (idea for a reference fixture)
- ❑ 1.2 dB fixture consisting of 2 segments
  - 105 ohm section (~0.4") and 95 ohm section (~0.8")
  - 30 fF between sections representing mode conversion
- ❑ 1.6 dB fixture consisting of 2 segments
  - 105 ohm section (~0.4") and 95 ohm section (~1.2")
  - 30 fF between sections representing mode conversion



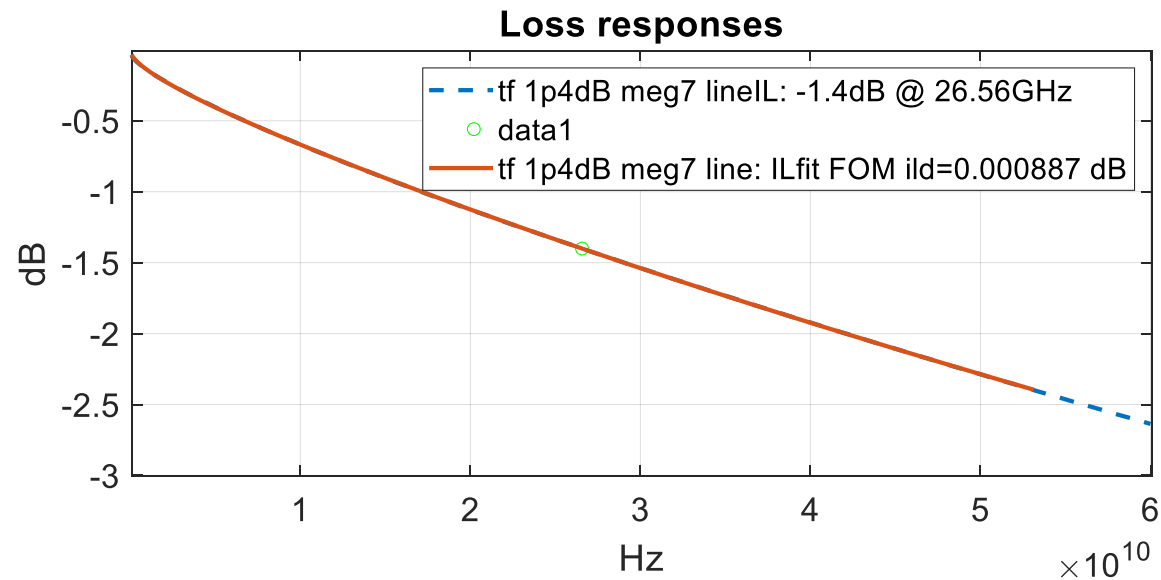
# Idea: 1.4 dB (@ 26.56 GHz) Fixture Strawman

❑ For this experiment replace equation 93-1

$$IL_{ref}(f) = -0.0015 + 0.144\sqrt{f} + 0.069f \text{ dB} \quad 0.05 \leq f \leq 25 \quad (93-1)$$

❑ With

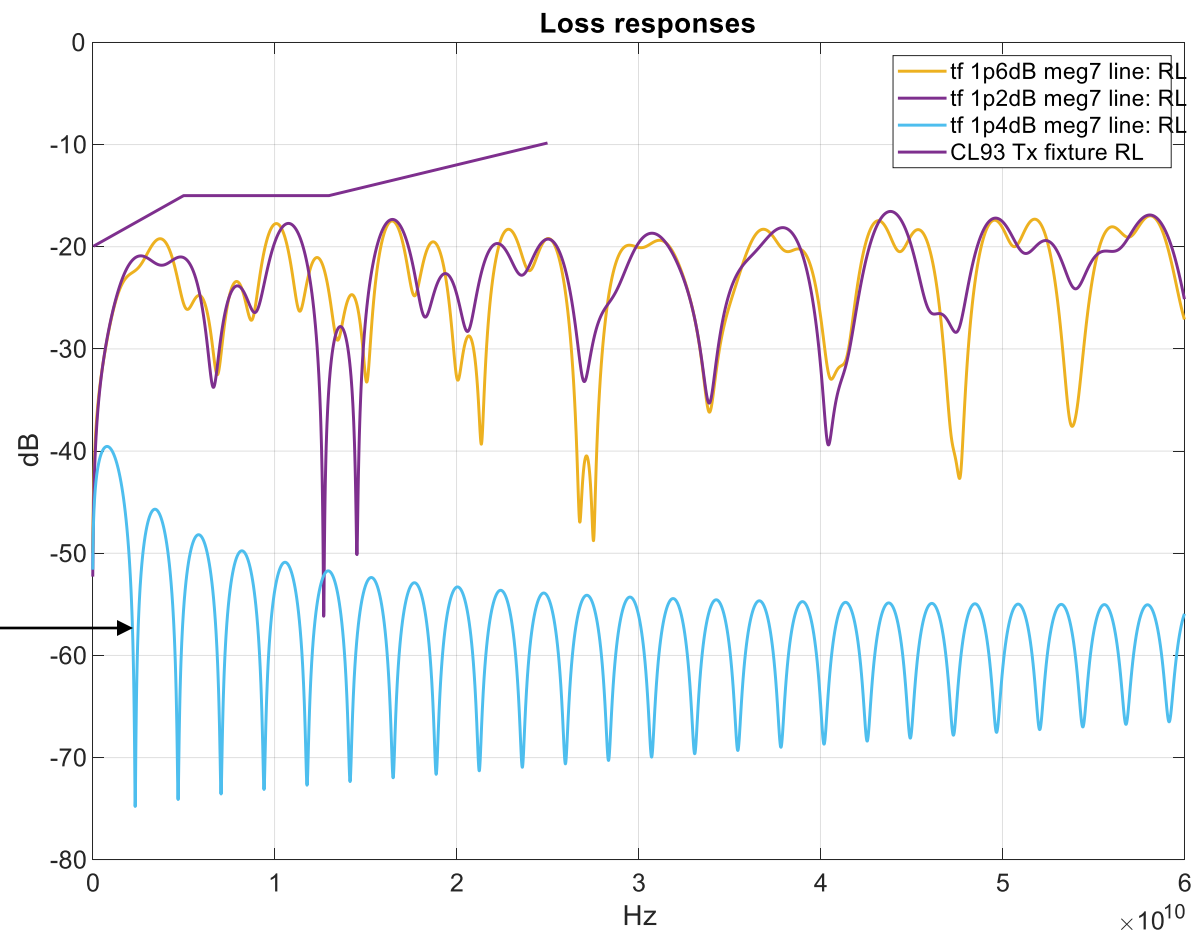
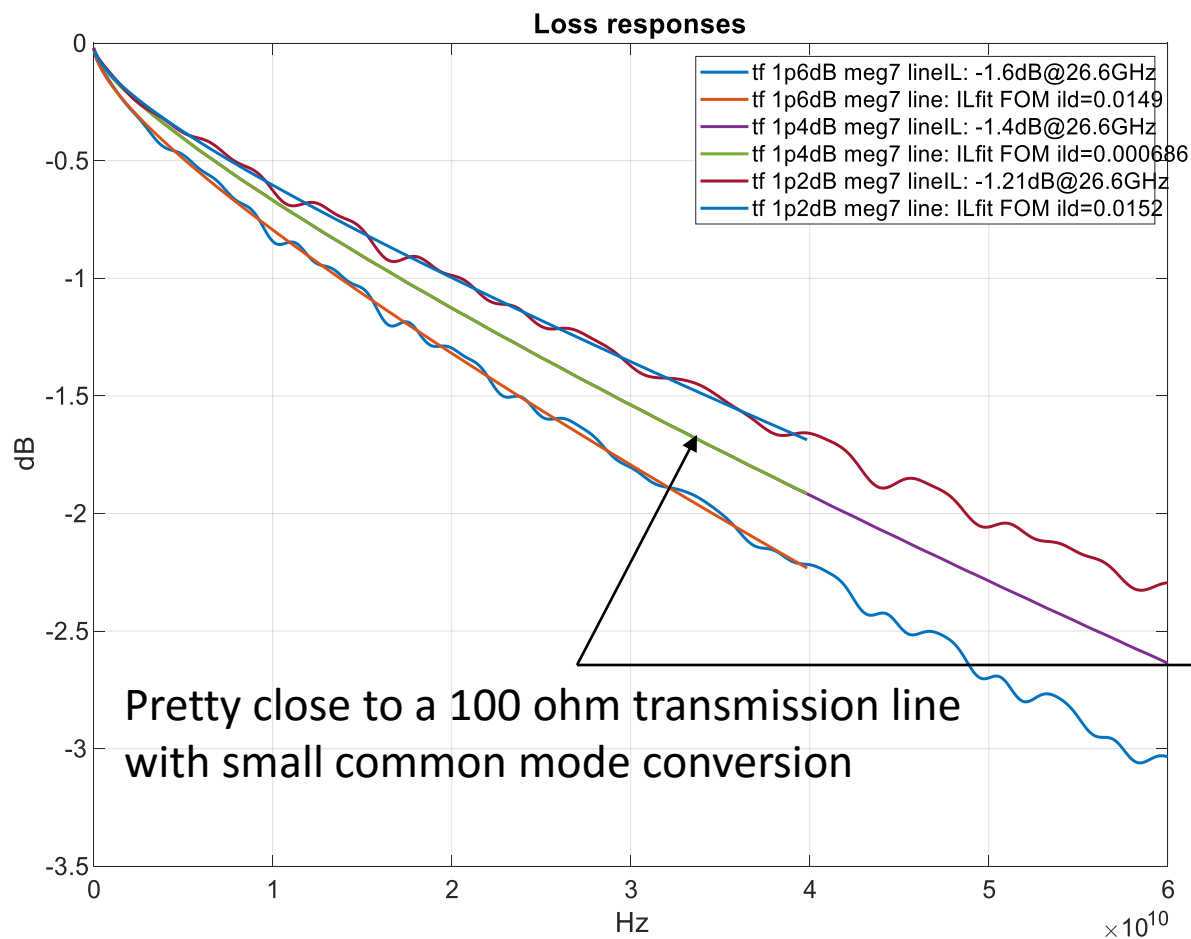
- $IL_{ref} = 0.0037 + 0.1052\sqrt{f} + 0.0337f$



- 1.4 dB at 100 ohm (differential) Megtron 7 H-VLP (strawman for reference fixture)
- Dotted blue line is the actual measurement
- Red line is the fit with above coefficients



# Even the 2 test fixtures don't look too bad



❑ So how much variability do they cause?

# First Set of Data to Illustrate Variability Experiment

- ❑ For each of test fixture, measure (TP0a)
  - ERL
  - $V_f$
  - $P_{\max}/V_f$
- ❑ Also measure ERL,  $V_f$ ,  $P_{\max}/V_f$  at TP0
- ❑ Sweep Package length and perform a DOE for package impedances
  - That's only 3 variables in this limited experiment
    - $z_p$ : 8 mm to 32 mm in 0.25 mm steps
    - $z_c$ :  $87.5 \Omega$  +/- 10%
    - $z_{c1}$ :  $92.5 \Omega$  +/- 10%
    - More variable added later to determine specification
- ❑ Goal is to determine spec impact for the above 3 parameters for each of the test fixtures

# Recommended Parameters for Computing ERL, $V_f$ , $P_{\max}/V_f$

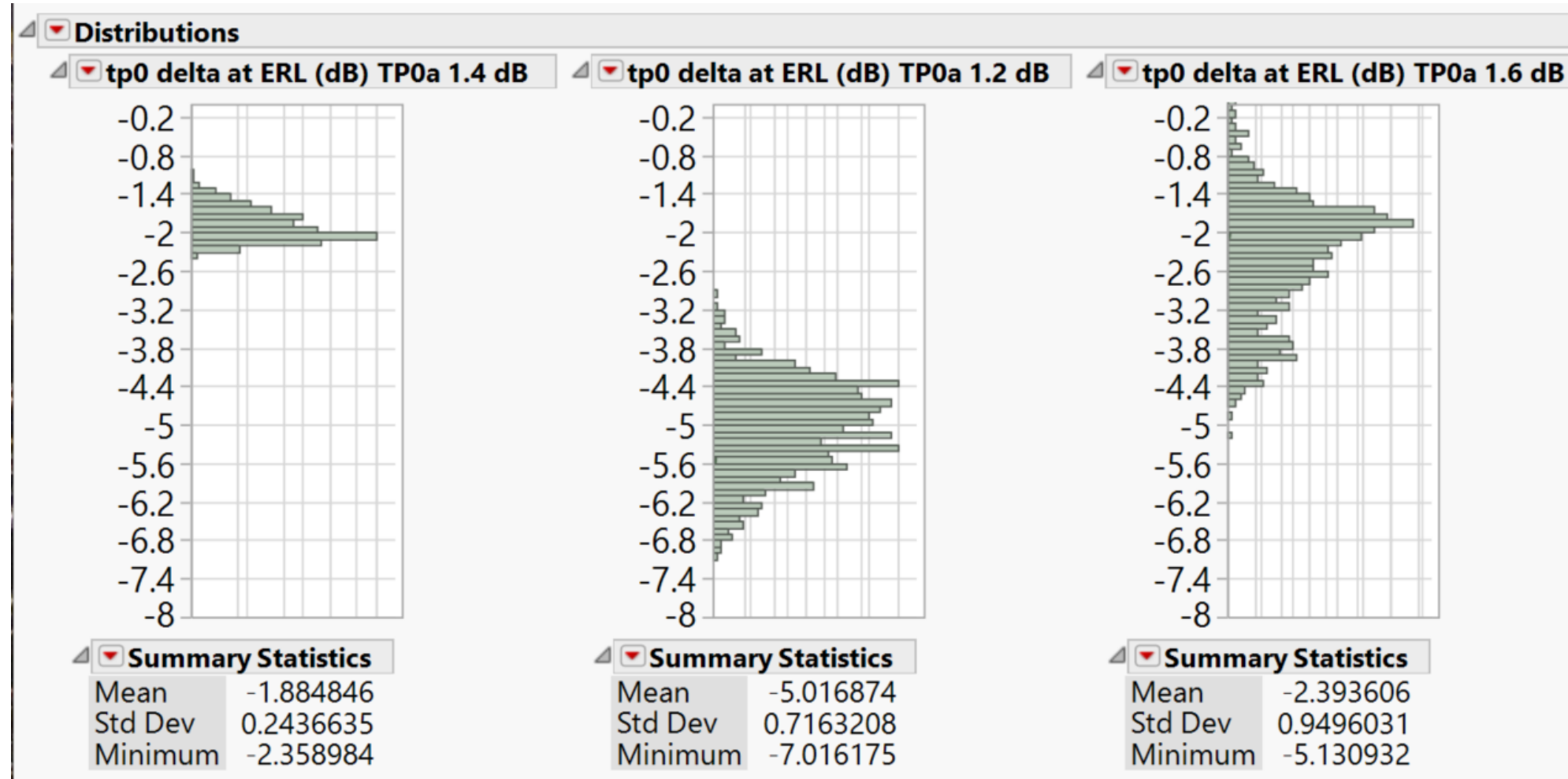
## □ ERL parameters

- $N_{bx} = 21$  (comment 22 modified)
  - Seems to be consensus here:  $21 = N_b + N_f * N_g$
- $\beta_x = 2.4$  GHz (comment 21)
- $\rho_x = 0.32$  (comment 21 modified)
  - Seems to be consensus to keep same as .3cd
- $N = 200$

## □ $V_f$ parameters (comment 25, see mellitz\_3ck\_01b\_0919)

- $N_v = 200$ 
  - In practice when computing from s-parameters and a computed step response this value may need to lower because of some data may not have sufficient low frequency data.
  - Produces a  $V_f$  more like a real steady state voltage
- $k = -3$  to  $1$
- $D_p = 4$

# Point by point case differences between ERL at TP0 and TP0a for discussion in next slide



# The Fixtures Introduce an Offset and Variability

- ❑ The reference fixture has the least amount of variability.
- ❑ Even the very good 100 ohm test fixture has variability
- ❑ Accounting for practical test fixture variability test dwarfs the limit we would want set
- ❑ Recommend:
  - Specify transmitter at a TP0 and receiver ERL at TP5
  - Remove test fixture references
  - Modified remedy for comment 19

$P_{\max}/V_f$  is impacted when tp0 is the test point

Draft Amendment to IEEE Std 802.3-2018  
IEEE P802.3ck Task Force name Task Force

IEEE Draft P802.3ck/D1.0  
12th December 2019

**Table 163–5—Summary of transmitter specifications at TP0a (continued)**

Parameter	Reference	Value	Units
AC common-mode RMS voltage (max.) <sup>1</sup>	93.8.1.3	30	mV
Effective return loss (ERL) (min.)	163.9.2.1	TBD	dB
Common-mode return loss (min.)	93.8.1.4	TBD	dB
Transmitter steady-state voltage, $v_f$ (min.) Transmitter steady-state voltage, $v_f$ (max.)	162.9.3.1.2	0.4 0.6	V
Linear fit pulse peak (min.) $P_{\max}$	162.9.3.1.2	TBD $\times v_f$	V
Level separation mismatch ratio $R_{LM}$ (min.)	120D.3.1.2	0.95	—

# Add a few more parameter to determine spec's

□ Use 5 variables in to determine ERL and  $P_{\max}/V_f$  variability,

- $z_p$ : 8 mm to 32
- $z_c$ :  $87.5 \Omega \pm 10\%$
- $z_{c1}$ :  $92.5 \Omega \pm 10\%$
- $R_d$ :  $50 \Omega \pm 10\%$
- $C_d$ : 126 ff  $\pm 10\%$
- $L_s$ : 126 pH  $\pm 10\%$

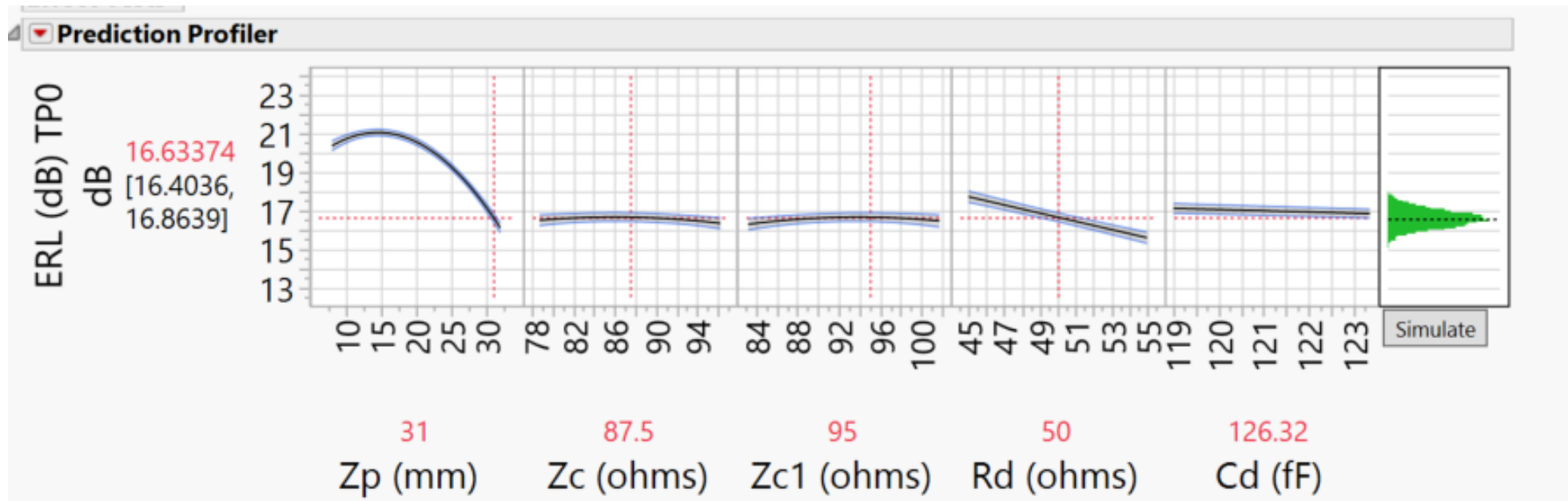
ERL fit to parameter is pretty good and  $P_{\max}/V_f$  fits are excellent.

- ❑ Lock the  $Z_p$  to 31 as in the COM reference
  - This is the max loss package
- ❑ Use manufacturing variability and fit uncertainty to determine ERL and  $P_{\max}/V_f$  specifications



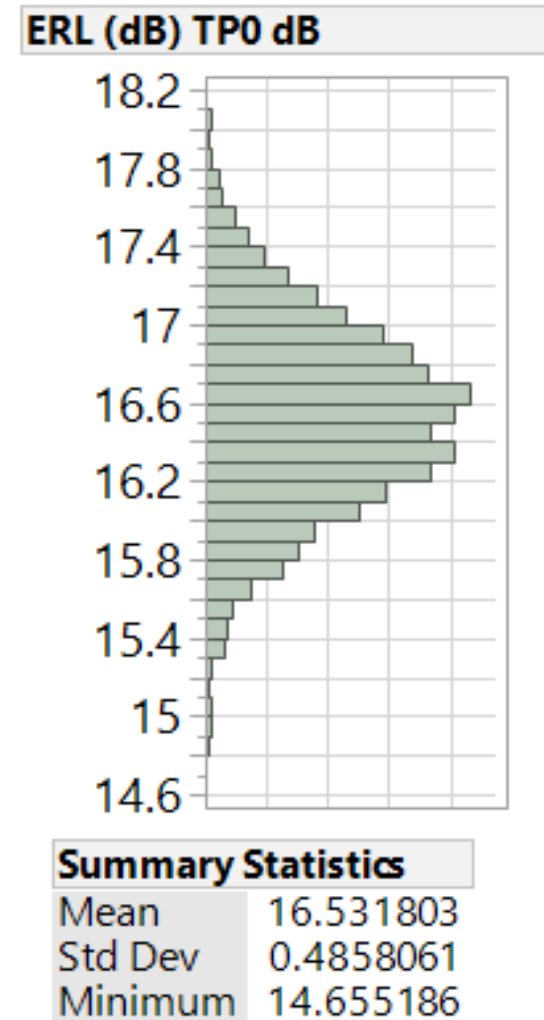
# ERL Fit is pretty good

- ❑ the RMS fits error at  $Z_p=31\text{mm}$  is  $< 0.2\text{ dB}$
- ❑ This RMS uncertainty is used to lower the spec.



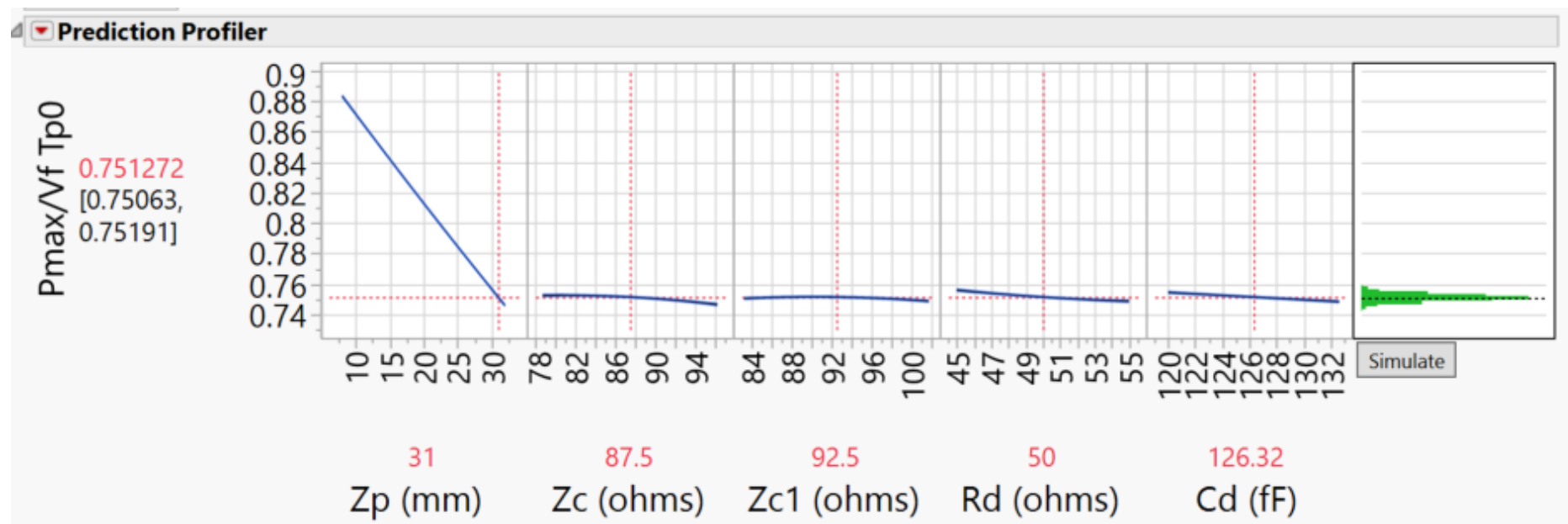
# ERL<sub>min</sub> Recommendation

- ❑ For 50000 cases manufacturing cases the minimum ERL is 14.65 dB
- ❑ Subtract 0.2 dB for fit uncertainty
- ❑ Recommend ERL<sub>min</sub> = 14.45 dB
  - Measured at tp0 (and TP5)



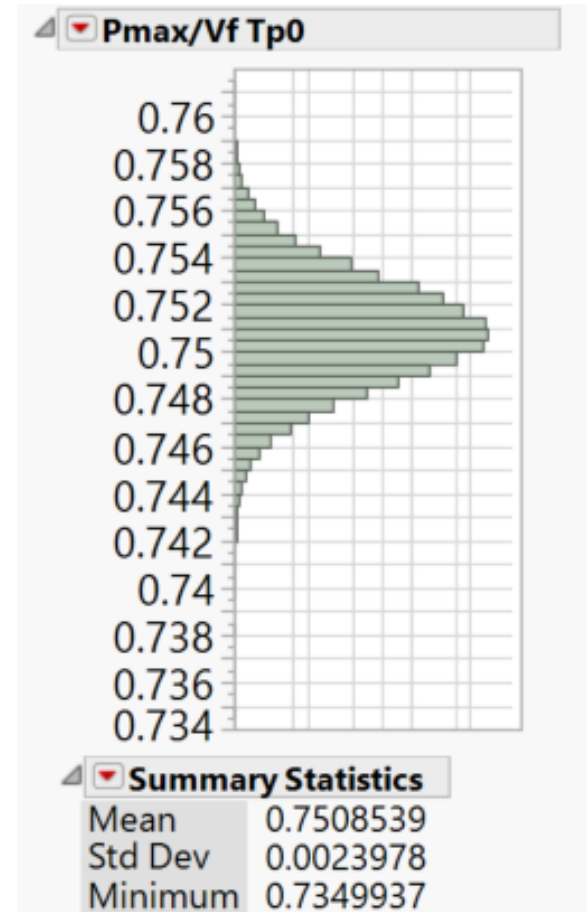
# $P_{\max}/V_f$ Fit is excellent

- ❑ To put another way it is a good measure of package and termination insertion loss.
- ❑ The RMS fits error at  $Z_p=31\text{mm}$  is  $< 0.002$  dB
- ❑ This RMS uncertainty used to lower the spec



# $P_{\max}/V_f$ Recommendation

- ❑ For 50000 cases manufacturing cases the minimum  $V_{\text{peak}}/V_f$  is 0.734
- ❑ Subtract 0.002 dB for fit uncertainty
- ❑ Recommend  $P_{\max}/V_f \text{ min} = 0.73$ 
  - Measured at TP0 (and TP5)



# Summary/Recommendation

- ❑ Specify ERL,  $V_f$ , and  $P_{\max}$  at  $tp_0$
- ❑ Specify  $P_{\max}/V_f \min = 0.73$
- ❑ Specify  $ERL_{\min} = 14.45$  dB for Tx and Rx
- ❑ Remove reference to  $tp_{0a}$  and  $tp_{5a}$  test fixtures for transmitter testing and receiver ERL.

# Backup

# COM template configuration used to compute ERL, $V_f$ , $P_{\max}/V_f$

$Z_p$  and  $Z_c$  are set by experiment control

Channel s parameters are an ideal thru (No RL and no IL)

$A_v$  becomes the  $V_f$  spec at TP0.

Table 93A-1 parameters			
Parameter	Setting	Units	Information
f_b	53.125	GBd	
f_min	0.05	GHz	
Delta_f	0.01	GHz	
C_d	[1.2e-4 0]	nF	[TX RX]
L_s	[0.12, 0]	nH	[TX RX]
C_b	[0.3e-4 0]	nF	[TX RX]
z_p select	1		[test cases to run]
z_p (TX)	[11; 1.8]	mm	[test cases]
z_p (NEXT)	[0; 0]	mm	[test cases]
z_p (FEXT)	[0; 0]	mm	[test cases]
z_p (RX)	[0; 0]	mm	[test cases]
C_p	[0.87e-4 0]	nF	[TX RX]
R_0	50	Ohm	
R_d	[ 50 50]	Ohm	[TX RX]
A_v	0.415	V	vp/vf=.694
A_fe	0.415	V	vp/vf=.694
A_ne	0.608	V	
L	4		
M	32		
filter and Eq			
f_r	0.75	*fb	
c(0)	0.54		min
c(-1)	0		[min:step:max]
c(-2)	0		[min:step:max]
c(-3)	0		[min:step:max]
c(1)	0		[min:step:max]
N_b	0	UI	
b_max(1)	0.85		
b_max(2..N_b)	0.2		
g_DC	0	dB	[min:step:max]
f_z	200	GHz	
f_p1	200	GHz	
f_p2	400	GHz	
g_DC_HP	0		[min:step:max]
f_HP_PZ	0.0001	GHz	

I/O control		
DIAGNOSTICS	0	logical
DISPLAY_WINDOW	0	logical
CSV_REPORT	0	logical
RESULT_DIR	.\results\100GEL_CR_{date}\	
SAVE_FIGURES	0	logical
Port Order	[1 3 2 4]	
RUNTAG	CR_eval_	
COM_CONTRIBUTION	0	logical
Operational		
COM Pass threshold	3	dB
ERL Pass threshold	10	dB
DER_0	1.00E-04	
T_r	6.16E-03	ns
FORCE_TR	1	logical
TDR and ERL options		
TDR	1	logical
ERL	1	logical
ERL_ONLY	1	logical
TR_TDR	0.01	ns
N	200	
beta_x	2.4000E+09	
rho_x	0.32	
fixture delay time	[ 0 0 ]	[ port1 port2 ]
TDR_W_TXPKG	1	
N_bx	21	UI
N_v	200	UI
Receiver testing		
RX_CALIBRATION	0	logical
Sigma BBN step	5.00E-03	V
Noise, jitter		
sigma_RJ	0.01	UI
A_DD	0.02	UI
eta_0	8.2E-09	V^2/GHz
SNR_TX	33	dB
R_LM	0.95	

Table 93A-3 parameters		
Parameter	Setting	Units
package_tl_gamma0_a1_a2	[0 0.0009909 0.0002772]	
package_tl_tau	6.141E-03	ns/mm
package_Z_c	[87.5 87.5 ; 92.5 92.5 ]	Ohm
benartsi_3ck_01_0119 & mellitz_3ck_01_0119		
Table 92-12 parameters		
Parameter	Setting	
board_tl_gamma0_a1_a2	[0 3.8206e-04 9.5909e-05]	
board_tl_tau	5.790E-03	ns/mm
board_Z_c	100	Ohm
z_bp (TX)	110.3	mm
z_bp (NEXT)	110.3	mm
z_bp (FEXT)	110.3	mm
z_bp (RX)	110.3	mm
C_0	[0.29e-4]	nF
C_1	[0.19e-4]	nF
Include PCB	0	logical
Floating Tap Control		
N_bg	0	0 1 2 or 3 groups
N_bf	3	taps per group
N_f	40	UI span for floating taps
bmaxg	0.2	max DFE value for floating taps
cable assemblies require this for each HCB		
ICN parameters (v2.73)		
f_f	12.919	
f_n	12.919	
f_2	39.844	
A_ft	0.600	
A_nt	0.600	
heck_3ck_03b_0319	Adopted Mar 2019	COM V2.77 but can do same on COM 2.76 by setting N_b to 200
walker_3ck_01a_0719	Adopted July 2019	
result of R_d=50		
benartsi_3ck_01a_0719	no used for KR	
mellitz_3ck_03_0919		