

**Experimental Characterization** 

IEEE P802.3cz Multi-Gigabit Optical Automotive Ethernet Task Force, Jun. 2021.

#### Presented by:

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### 1. Objective

☐ Demonstrate the relationship between insertion loss in multi-mode connectors and modal noise.

## 2. Agenda

- Modal Noise Estimation from RIN<sub>OMA</sub> Measurements
  - Definition of Modal Noise Estimation
- Launching Setup: VCSEL to Fiber Coupling
  - Modal Noise due to VCSEL to Lens Radial Misalignment
- Modal Noise in Butt-Coupling (BC) Connections
  - Effects of Radial Misalignment
  - > Effects of Axial Misalignment
  - > Effects of Tilt Misalignment
- Modal Noise in Expanded Beam Optics (EBO) Connections
  - Effects of Tilt Misalignment
    - Relation between Tilt Misalignment in EBO and Radial Misalignment in BC.
  - Analysis of Radial Offset in EBO
    - Relation between Radial Misalignment in EBO and Tilt Misalignment in BC.
- □ Conclusions



Modal Noise Estimation from RIN<sub>OMA</sub> Measurement

## 1. Modal Noise Estimation from RIN<sub>OMA</sub> Measurement



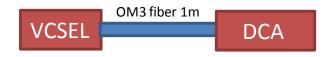
## 1. RIN<sub>OMA</sub>

Test method for RIN<sub>OMA</sub> has been defined by [1] as:

$$RIN_{OMA} = 10 \times log_{10} \left( \frac{RN_{one} + RN_{zero}}{OMA^2 \times BW_N} \right)$$

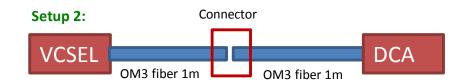
where  $RN_{one/zero}$  is standard deviation of noise measured in level 1/0 (in Watts); OMA is the optical modulation amplitude (in Watts) and  $BW_N$  is the noise equivalent bandwidth (in Hz).

VCSEL's RIN can be considered to be the main source of noise in the following setup (setup 1):



- ➤ If the VCSEL is directly connected to the DCA with a short section of fiber and there is no mode selective loss in the VCSEL coupling.
- Scope (DCA) background noise is compensated.

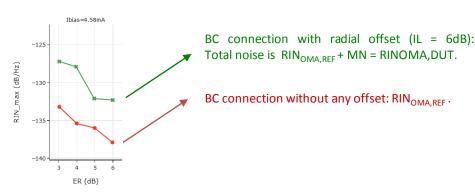
## 2. Estimation of Modal Noise (MN)



If we consider a link with in-line connectors (setup 2), the  $RIN_{OMA}$  measurements in the DCA will be effected by the Modal Noise (MN) that may be produced due misalignments in the connectors.

The difference of variances between the **Total Noise** ( $RIN_{OMA,DUT}$  from setup 2) and the reference  $RIN_{OMA}$  (from setup 1) will be an acceptable approximation of MN caused by the connectors misalignments. This can be calculated as:

$$\frac{\sigma_{n0,MN} + \sigma_{n1,MN}}{OMA} = \sqrt{\left(10^{\frac{RIN_{OMA,DUT}}{10}} - \left(10^{\frac{RIN_{OMA,REF}}{10}}\right) \times BW_n\right)}$$





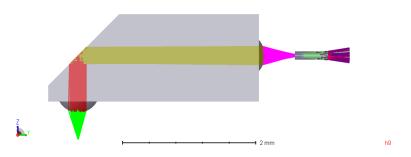
2. Launching Setup: VCSEL to Fiber Coupling

## 2.1. Launching Setup

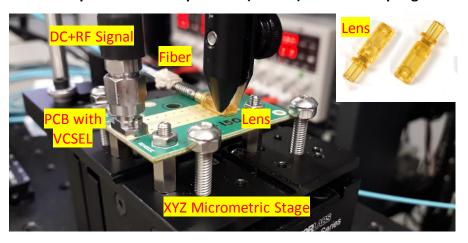


### 1. COB Type Lens (ULTEM)

- □ Coupling Efficiency > 78% | IL < 1.1dB.
  - Losses are mainly due to material attenuation and Fresnel. No mode selective loss.

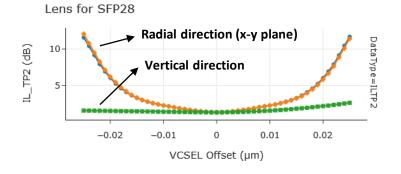


☐ Experimental Setup: VCSEL (850nm) to Fiber Coupling.



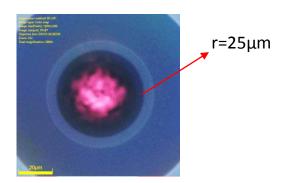
### 2. Alignment for the lowest RIN

☐ IL vs VCSEL Offset (**Simulation**).



#### NFP at TP2 (1m of fiber). Underfilled launch!

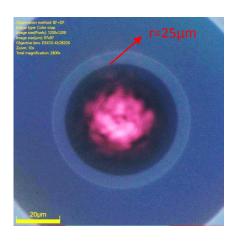
➤ To avoid selective losses at the VCSEL-to-Fiber coupling in order to evaluate the modal noise in the intermediate connectors.



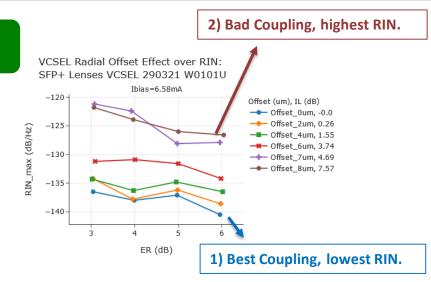
## 2.2. Effects of VCSEL-to-Lens Radial Misalignment



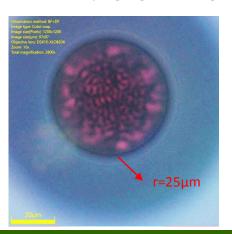
1. Reference RIN (RIN<sub>OMA,REF</sub>) Best Coupling, No misalignment.



- 1. Degradation of RIN<sub>OMA</sub>
  Measurements
- ➤ Losses due to VCSEL-to-Lens Misalignment generates Noise.
- ➤ Mode Selective Loss



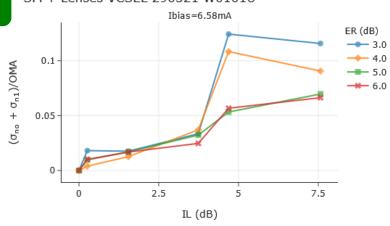
2) Worst RIN<sub>OMA,DUT</sub>
Worst Coupling, highest misalignment



#### 2. Estimation of Modal Noise

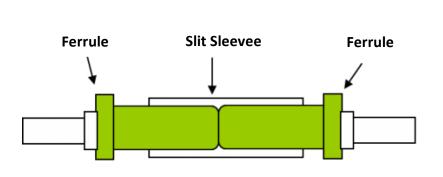
- ➤ Modal Noise is estimated from RIN<sub>OMA DUT</sub>.
- There is a direct relationship between ILs due to VCSEL-to-Lens radial misalignment and Modal Noise

VCSEL Radial Offset Effect over Modal Noise: SFP+ Lenses VCSEL 290321 W0101U





## 3. Modal Noise in Butt-Coupling Connections





## 3.1. Modal Noise in Butt-Coupling

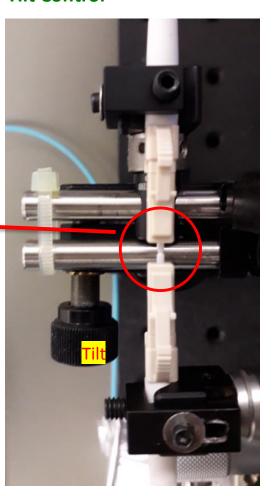


## 1. Experimental Setup

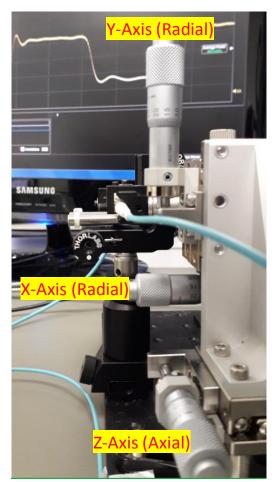
- ➤ IL < 0.55dB</p>
- No spring-loaded
- > 2 x LC fibers of 2m with PC termination
- No mandrel wrapping



#### **Tilt Control**



#### **XYZ Control**



## 3.2. Modal Noise in Butt-Coupling: Effects of Radial Misalignments



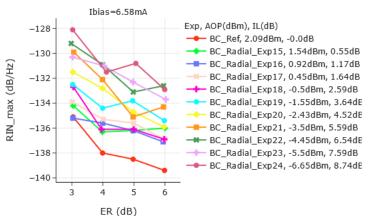
#### BC: Radial Misalignment

- ➤ IL with no offset = 0.55dB.
  - A small gap is needed between the fibers to allow radial displacement.
- High sensitivity to Radial Misalignment.
- Direct dependence between MN and ILs.

# (QD) 1 -2.5 -5.0 OM3 Fibers -7.5 0 10 20 30 BC Radial Offset (um)

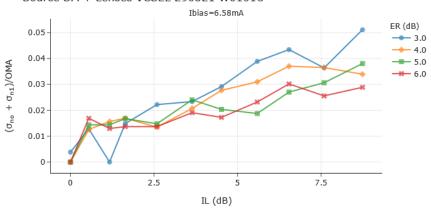
#### 1. RIN<sub>OMA</sub> Measurements

Ref RIN<sub>OMA</sub> measurement has been taken with a LC-to-LC connector. Radial Offset Effect over RIN in BC connection of OM3 Fibers: Source SFP+ Lenses VCSEL 290321 W0101U



#### 2. Estimation of Modal Noise

Radial Offset Effect over Modal Noise in a BC connection of OM3 Fibers: Source SFP+ Lenses VCSEL 290321 W0101U

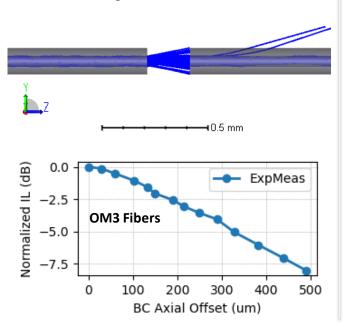


## 3.3. Modal Noise in Butt-Coupling: Effects of Axial Misalignments



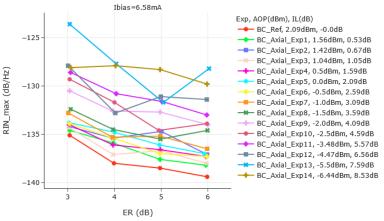
#### BC: Axial Misalignment (Gap)

- > IL with no offset = 0.53dB
- ➤ IL has **low dependence with the gap**, especially if manufacturing tolerances are taken into account. However, any gap generates reflections.
- > Direct dependence between MN and ILs.
  - Quite similar to the case of radial misalignment



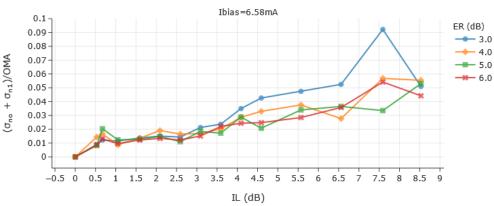
#### 1. RIN<sub>OMA</sub> Measurements

Ref RIN<sub>OMA</sub> measurement has been taken with a LC-to-LC connector. Axial Offset Effect over RIN in a BC connection of OM3 Fibers: Source SFP+ Lenses VCSEL 290321 W0101U



#### 2. Estimation of Modal Noise

Axial Offset Effect over Modal Noise in a BC connection of OM3 Fibers: Source SFP+ Lenses VCSEL 290321 W0101U



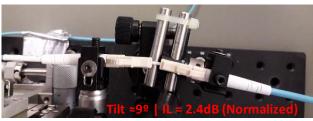
## 3.4. Modal Noise in Butt-Coupling: Effects of Tilt Misalignments

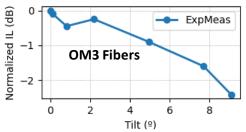


#### **BC**: Tilt Misalignment

- $\Box$  IL with no offset = 0.55dB
- ☐ BC has Very low sensitivity to tilt.
  - However, it is not a realistic case.
  - It is not possible to have very high tilt values in a connector.
- ☐ There is a direct relationship between MN and IL from IL> 1dB.

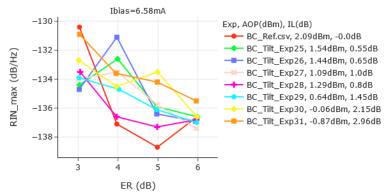






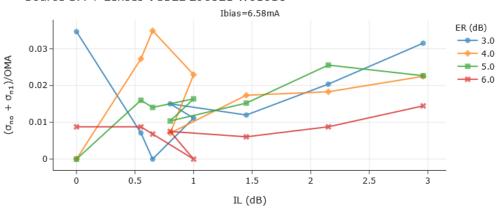
#### 1. RIN<sub>OMA</sub> Measurements

Ref RIN<sub>OMA</sub> measurement has been taken with a LC-to-LC connector. Tilt Offset Effect over RIN in a BC connection of OM3 Fibers: Source SFP+ Lenses VCSEL 290321 W0101U



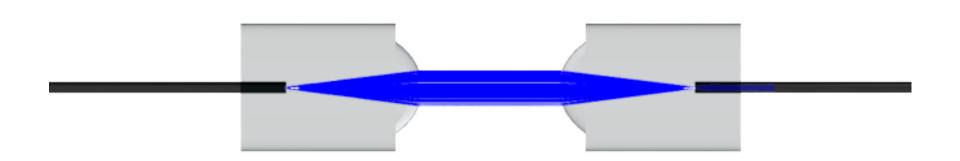
#### 2. Estimation of Modal Noise

Tilt Offset Effect over Modal Noise in a BC connection of OM3 Fibers: Source SFP+ Lenses VCSEL 290321 W0101U





Modal Noise in Expanded BeamOptics (EBO) Connections



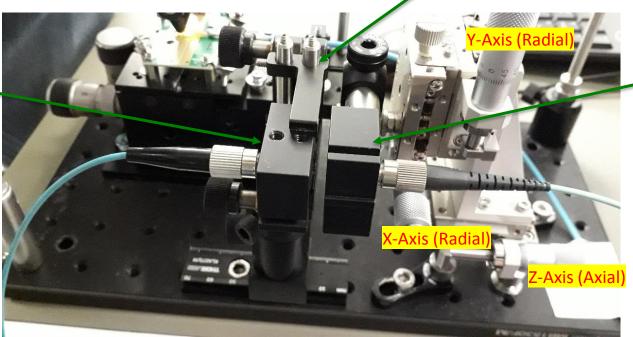
## 4. Modal Noise in Expanded Beam Optics (EBO)



## 1. Experimental Setup

- > Two 2m OM3 fibers. No mandrel wrapping.
- **EBO** connector with two collimators: F220FC-850
  - Beam diameter: 2.5mm
  - Focal distance: 11.12mm
- Kinematic stage for tilt control: KM100C
  - 8mrad Tilt per turn (from datasheet)
- xyz stage form alignment
- ➤ Min IL = 0.45dB







## 4. Modal Noise in EBO: Experimental Tilt Measurements



#### Tilt Measurements

- AOP Measurements
  - ➤ OPTOKON 820
    - 1mm diameter detector
  - Micrometer Head
    - Tilt = 0.46º (8mrad) per turn (from datasheet)

Image	Tilt_Deg	AOP_dBm	IL_dB
1	0	-1.46	0
2	0.0336125	-2	0.54
3	0.0503942	-2.5	1.04
4	0.0641543	-3	1.54
5	0.0790596	-3.61	2.15
6	0.0956225	-4.5	3.04
7	0.1113365	-5.6	4.14
8	0.1407354	-7.6	6.14
9	0.1565097	-9.5	8.04
10	0.1742315	-11.31	9.85



















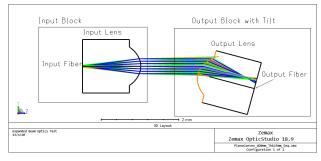


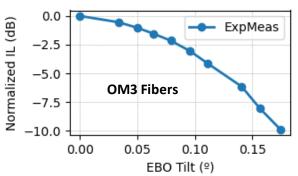
### 4. Modal Noise in EBO: Effects of Tilt Misalignment



### EBO: Tilt Misalignment

- $\Box$  IL with no offset = 0.56dB.
- ☐ Fibers and collimators move as a single element .
- ☐ High sensitivity to tilt.
- ☐ There is a direct relationship between ILs due to tilt and the modal noise.
- ☐ Tilt in EBO is equivalent to Radial Misalignment in BC.

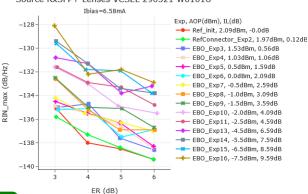




#### 1. RIN<sub>OMA</sub> Measurements

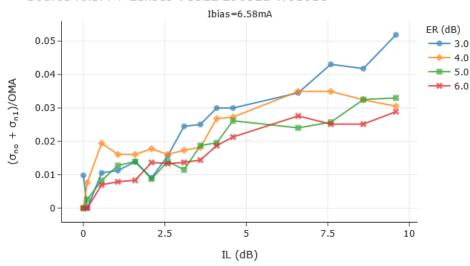
Ref RIN<sub>OMA</sub> measurement has been taken with a LC-to-LC connector.





#### 2. Estimation of Modal Noise

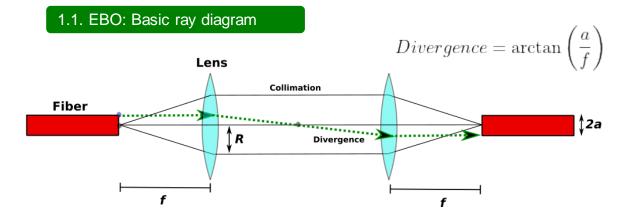
## Tilt Offset Effect over Modal Noise in a EBO conection of OM3 Fibers: Source RxSFP+ Lenses VCSEL 290321 W0101U



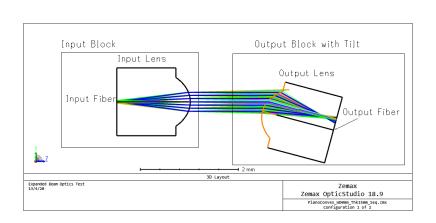
## 4. Modal Noise in EBO: Analysis of Tilt Misalignment



### 1. Tilt in EBO is equivalent to Radial Misalignment in BC



#### 1.2. Divergence can be considered as tilt in EBO



$$Tilt = \arctan\left(\frac{\Delta r}{f}\right)$$
$$\Delta r : Radial M is a lignment$$
$$\Delta r = f \times \tan\left(Tilt\right)$$

#### 1.3. Verification

#### ☐ Slide 16:

- ➤ In EBO the IL = 3.1dB when Tilt = 0.096º.
- In an EBO system with f = 11.12mm, a tilt of 0.096<sup>o</sup> generates an equivalent
   Δr = 19μm at the fiber input (Theoretical value).

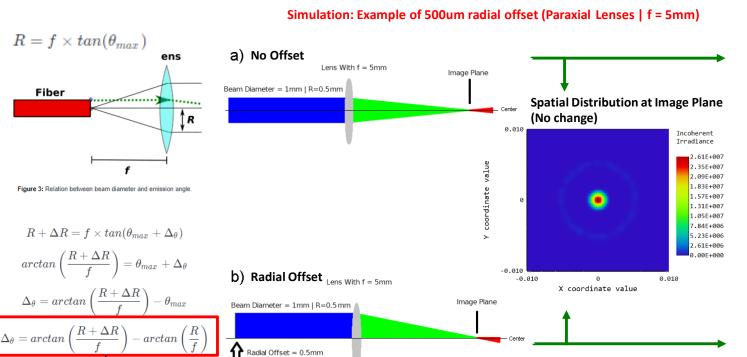
#### Slide 10:

ightharpoonup In BC IL = 3.1dB when Δr=20μm (Experimental value).

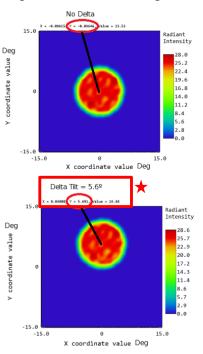
## 4. Modal Noise in EBO: Analysis of Radial Misalignment



#### Radial Misalignment in EBO is equivalent to Tilt in BC



#### **Angular Distribution at Image Plane**



**Angular Distribution at Image Plane** 

An approximation! GI Profile has to be taken in to account.

## In this example: $\Delta_{\theta} = \arctan\left(\frac{0.5mm + 0.5mm}{5mm}\right) - \arctan\left(\frac{0.5mm}{5mm}\right) = 5.6^{\circ}$

- ☐ EBO has very low sensitivity to radial misalignment.
  - Values are far from a practical case (real connector).
- ☐ This is because radial misalignment in EBO is equivalent to Tilt in BC.



## 5. Conclusions:

### 5. Conclusions: Modal Noise vs Misalignment Losses in MMFs Connectors



#### **Conclusions**

It has been shown that there is a direct dependence between Insertion Losses due to Misalignments in BC and EBO connectors with the Modal Noise. Therefore, it is very important to take into account that the losses in the connectors not only reduce the power in the Rx but may also increase the noise. On the other hand, it is important to remember that those losses that affect all modes equally (for example, material attenuation, Fresnel, NDFs) do not generate MSL and therefore do not generate modal noise. It has been shown that tilt misalignment in an EBO connector produces an effect equivalent to radial displacement in BC. > BC is very sensitive to radial misalignment. **EBO** is very sensitive to tilt misalignment. > Both effects can be related with a simple expression. It also has been shown that radial misalignment in EBO produces an effect equivalent to a tilt misalignment in BC. > BC is very robust to tilt misalignment. **EBO** is very robust to radial misalignment. > Both effects can be easily related. Therefore, the manufacturing tolerances EBO and BC connectors will be very similar.

However, it is important to remember that EBO is much more resistant to contamination than BC.

## 5. Conclusions: Modal Noise vs Misalignment Losses in MMFs Connectors



## **Future work**

Measure modal noise due to misalignment on multiple connectors.
<b>Improve</b> modal noise <b>measurements</b> by directly using the standard deviation components for high and low levels reported by the DCA.
Determine the <b>relationship</b> between the <b>spectral width of</b> the VCSEL and the <b>modal noise</b> at the connectors.
Determine the influence of reflections in multimode connectors over the modal noise.
Repeat the measurements with a VCSELs at 980nm.



6. References:

1. R. Aranda and P.J. Pinzón, "Test methods for VCSEL characterization", IEEE P802.3cz Multi-Gigabit Optical Automotive Ethernet Task Force, Jul. 2020. [Online]. Available:

https://www.ieee802.org/3/cz/public/jul\_2020/perezaranda\_OMEGA\_01b\_0720\_VCSEL\_test\_methods.pdf. [Accessed May. 25, 2021].