



# TDFOM simplification proposal

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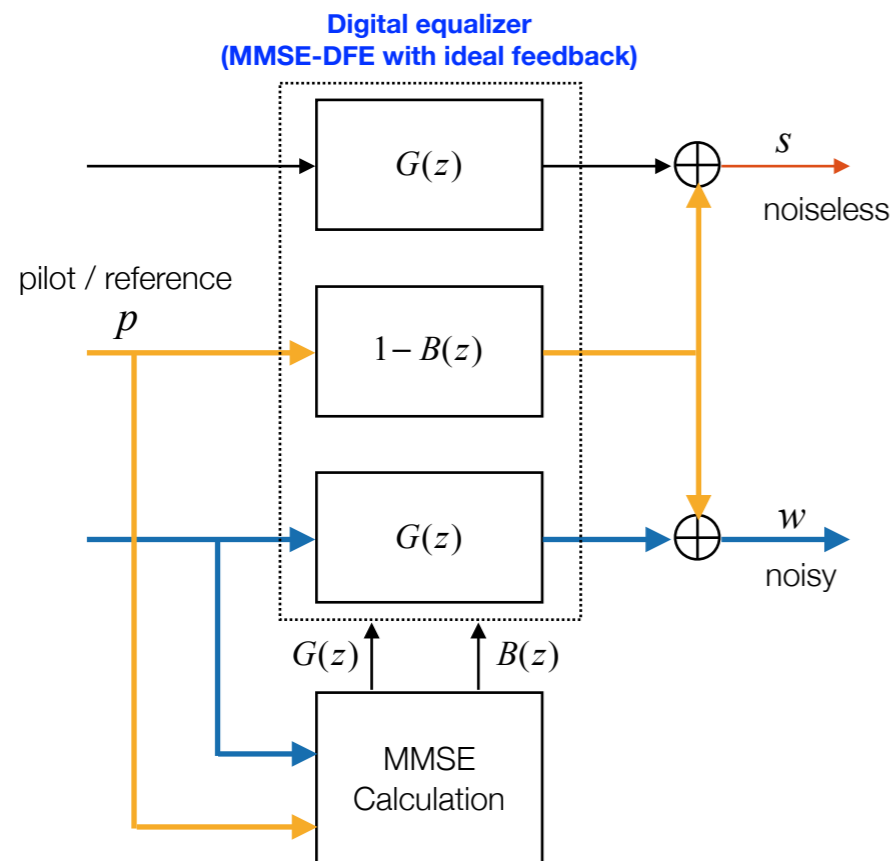
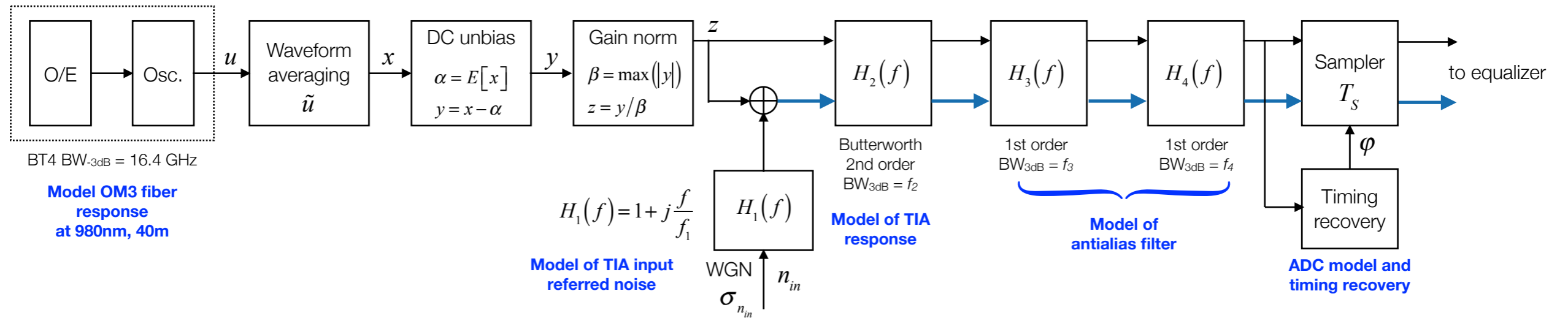
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# Objective

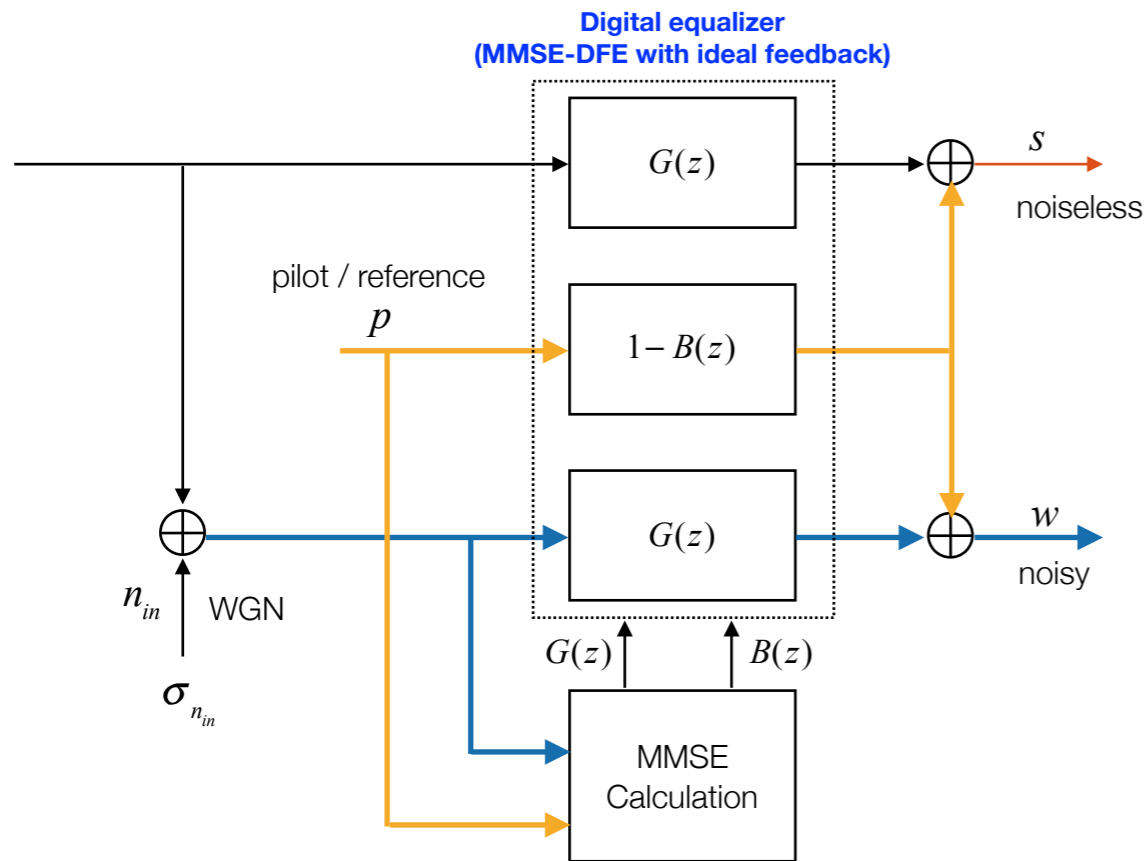
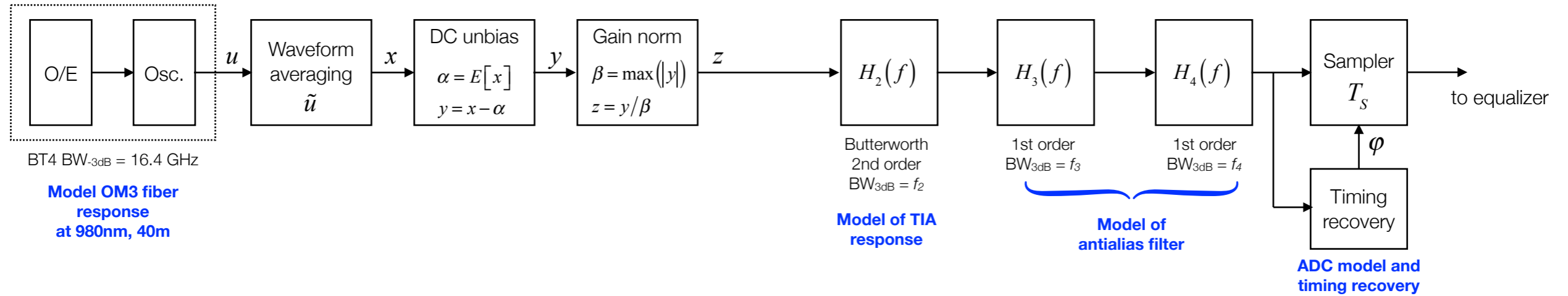
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- This contribution proposes a simplification of the TDFOM reference receiver and figure of merit of [1]
- Simplification is addressed in several ways:
  - Added noise is white, so noise filter is removed
  - Noise is added at the sampler output, so analytical calculation of standard deviation after equalizer is direct (noise variance measurement is removed)
  - Because noise is added at sampler output, the dependency with oversample factor (samples per UI) is also removed
- Improvement in OMA calculation for PAM4 is also proposed
  - CID length and pre/post cursors lengths is updated according to SSPR-PAM4 pattern
- New TDFOM proposal has been validated vs OMA receiver sensitivity

# Original TDFOM from [1]



# New TDFOM



# H1 is removed

## BASE-AU 980nm/OM3 reference receiver and analysis



- The input low pass filter shall be 4<sup>th</sup> order Bessel-Thomson with  $BW_{-3dB} = 16.4$  GHz
- Acquisition oversampling (samples per unit interval) shall be,  $O_v > 15$
- Waveform averaging shall be enabled to eliminate noise; averaging factor shall be selected high enough to avoid noise affecting the TDFOM analysis (error below 0.05 dB)
- Filters shall be scaled according to symbol period and modulation format as:

$$f_1 = \frac{1}{10 \cdot T_s} + 5 \cdot 10^8 \quad (\text{Hz});$$

$$f_3 = \frac{1}{2 \cdot T_s};$$

$$f_2 = \begin{cases} \frac{1}{5 \cdot T_s}, & \text{NRZ} \\ \frac{1}{3 \cdot T_s}, & \text{PAM4} \end{cases};$$
$$f_4 = \begin{cases} \infty, & \text{NRZ} \\ \frac{1}{2 \cdot T_s}, & \text{PAM4} \end{cases};$$

# Standard deviation

## BASE-AU 980nm/OM3 reference receiver and analysis



- BER calculation:

- Calculate the noise sequence in the output of equaliser as  $n = w - s$
- Calculate the standard deviation  $\sigma_n$
- Define the thresholds vector  $THv = [0]$  for NRZ, and  $THv = [-2/3, 0, +2/3]$  for PAM4
  - Define  $N_{th} = 1$  for NRZ, and  $N_{th} = 3$  for PAM4
- Calculate the histogram of signal  $s$ , where the value of each bin  $h(i)$  is normalised to relative probability, such that  $h(i) = c(i)/N_h$ , where  $c(i)$  is the number of elements in the bin centred in  $e(i)$  with width  $\Delta e$ , and  $N_h$  is the number of elements of signal  $s$ 
  - $\Delta e = (max(s) - min(s))/N_h$
  - $N_h$  shall be  $\geq 500$
- For each  $THv(k)$ :
  - Calculate  $ih_p$  as the bins that meet  $e(i) > THv(k)$
  - Calculate  $ih_n$  as the bins that meet  $e(i) \leq THv(k)$
  - Calculate  $SER_{th}(k)$  as:

$$SER_{th}(k) = \frac{1}{2} \sum_{i=\min(ih_n)}^{\max(ih_n)} h(i) \cdot \operatorname{erfc}\left(\frac{THv(k) - e(i)}{\sigma_n \sqrt{2}}\right) + \frac{1}{2} \sum_{i=\min(ih_p)}^{\max(ih_p)} h(i) \cdot \operatorname{erfc}\left(\frac{e(i) - THv(k)}{\sigma_n \sqrt{2}}\right)$$

where  $\operatorname{erfc}(x)$  is the complementary error function defined as:

$$\operatorname{erfc}(x) = \frac{2}{\sqrt{\pi}} \int_x^{\infty} e^{-t^2} dt$$

$$\sigma_n = \sigma_{n_{in}} \cdot \sqrt{\sum_{i=0}^{N_G-1} g_i^2}$$

# OMA calculation for PAM4

## BASE-AU 980nm/OM3 reference receiver and analysis



- OMA calculation at EQ output:
  - Define  $OMA_{eq}$  as the OMA of signal  $s$
  - OMA shall be measured using continuous identical digits (CID)
  - Search for positive CID as continuous samples of signal  $s$  with value  $> 0$ , for NRZ, or with value  $> 2/3$ , for PAM4
  - Search for negative CID as continuous samples of signal  $s$  with value  $< 0$ , for NRZ, or with value  $< -2/3$ , for PAM4
  - CID sequence length shall be  $\geq 14$  for NRZ,  $\geq 7$  for PAM4
  - For all the CID sequences that meet length constraint, remove:
    - For NRZ: first 6 and last 6 samples
    - For PAM4: first 3 and last 2 samples
  - For the remaining symbols of all the CID sequences calculate the average value
    - For positive CID sequences, we obtain  $OMA_p$
    - For negative CID sequences, we obtain  $OMA_n$
  - $OMA_{eq} = OMA_p - OMA_n$
- OMA calculation at EQ input
  - Calculate:

$$OMA_{in} = \frac{OMA_{eq}}{G_{eq}}$$

# TDFOM calculation

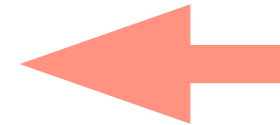
## BASE-AU 980nm/OM3 reference receiver and analysis



- TDFOM calculation

- Define reference Q-factor  $Q_0$  as:
  - $Q_0 = 3.5741$  for NRZ, consistent with  $BER = 1.757 \cdot 10^{-4}$
  - $Q_0 = 3.4981$  for PAM4, consistent with  $BER = 1.757 \cdot 10^{-4}$
- Calculate transmitter and distortion figure of merit (TDFOM) as:

$$TDFOM = 10 \cdot \log_{10} \left( \frac{OMA_{in} \sqrt{Ov}}{2(M-1)\sigma_{n_{in}} Q_0} \right) - TDFOM_0$$



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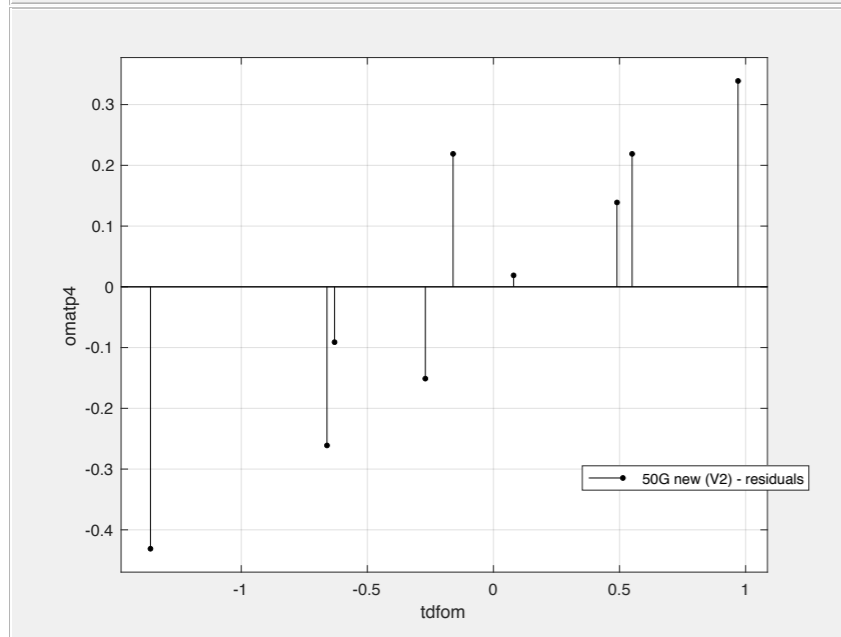
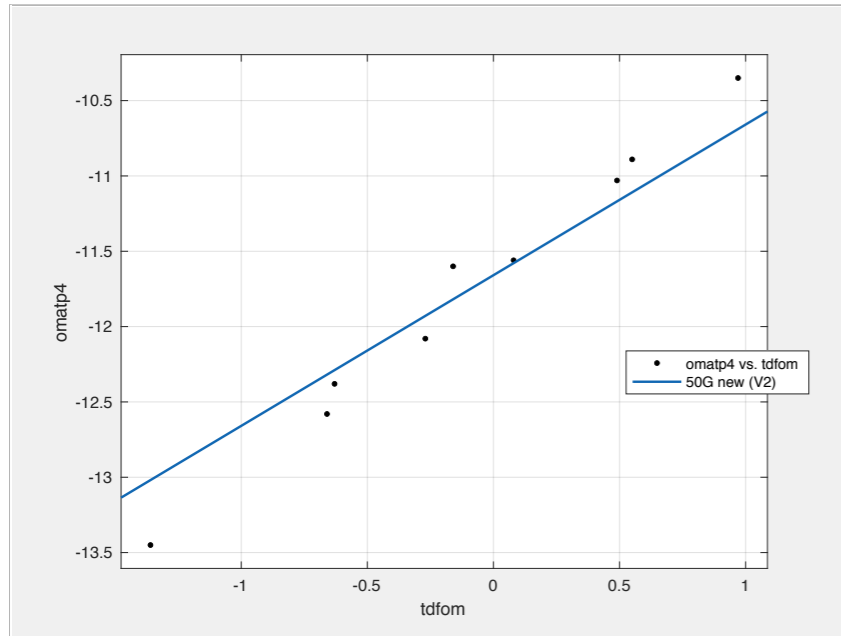
where  $M = 2$  for NRZ, and  $M = 4$  for PAM4.

- $TDFOM_0$  is calculated to get  $TDFOM = 0$  dB when an ideal transmitter (square pulse) is connected to the reference receiver
- It depends on bit-rate:
  - For 50 Gb/s:  $TDFOM_0 = 4.47$  dB    **2.83113**
  - For 25 Gb/s:  $TDFOM_0 = 4.27$  dB    **3.92395**
  - For 10 Gb/s:  $TDFOM_0 = 3.29$  dB    **3.63153**
  - For 5 Gb/s:  $TDFOM_0 = 2.59$  dB    **3.60715**
  - For 2.5 Gb/s:  $TDFOM_0 = 1.84$  dB    **3.59469**
- $TDFOM_0$  values are obtained by simulation connecting a square pulse transmitter to the reference receiver input

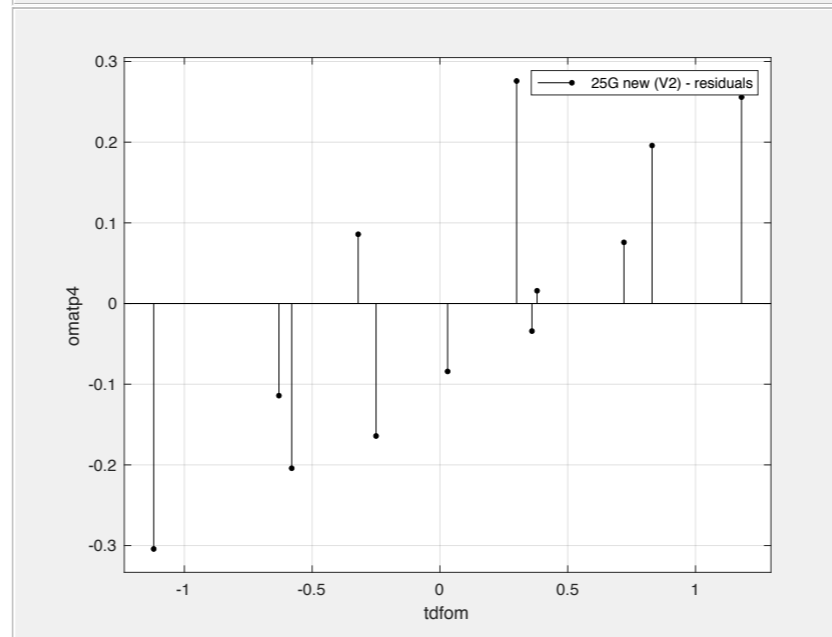
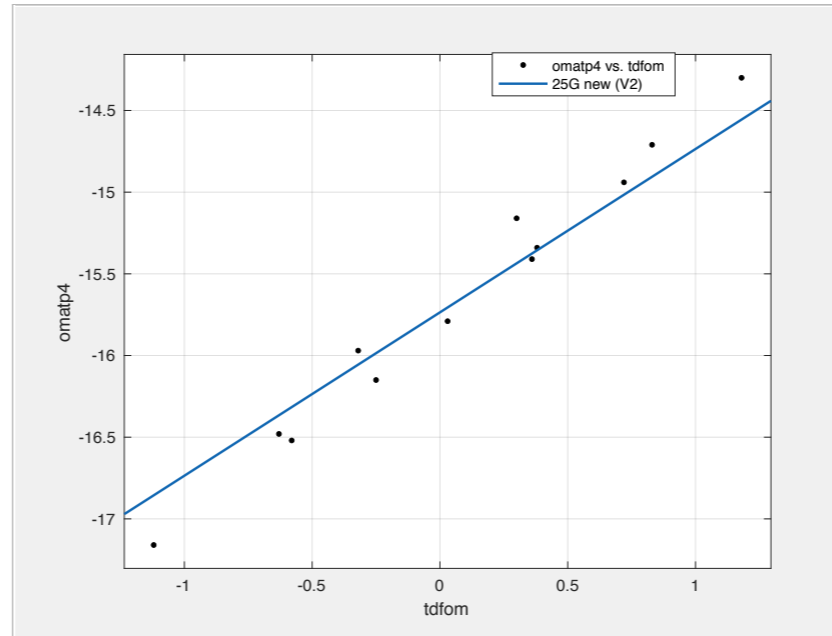


# New TDFOM vs. RX sensitivity

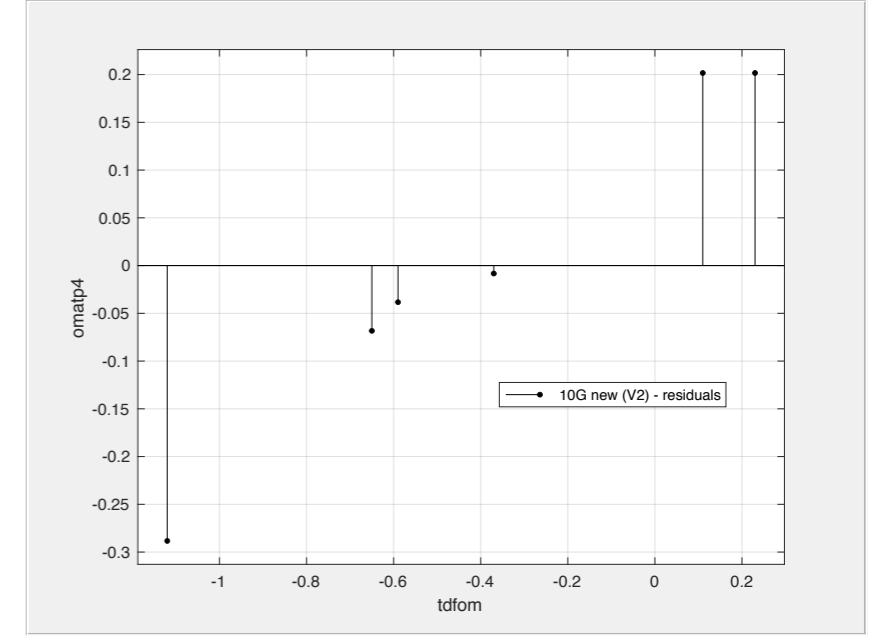
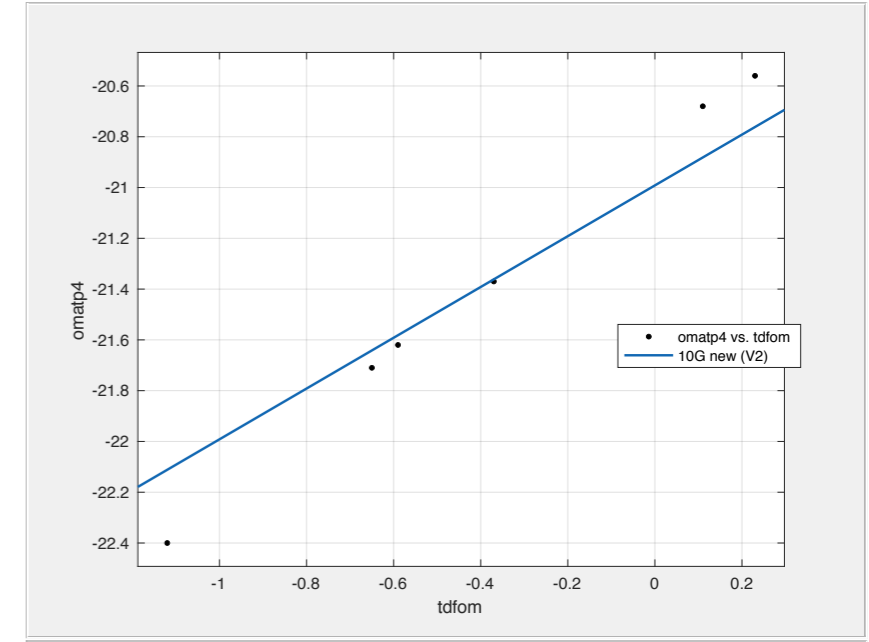
Fitting:  $OMA_{TP4} = TDFOM + K$



**50 Gb/s**  
**3 VCSEL driver designs**  
**Tbs = -40, 25 and 125 °C**  
**1 RX design at 125°C**



**25 Gb/s**  
**4 VCSEL driver designs**  
**Tbs = -40, 25 and 125 °C**  
**1 RX design at 125°C**



**10 Gb/s**  
**2 VCSEL driver designs**  
**Tbs = -40, 25 and 125 °C**  
**1 RX design at 125°C**

# References

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- [1] R. Pérez-Aranda, “BASE-AU 980nm/OM3 baseline. Reference receiver and transmitter and distortion figure of merit,” February 2022, [Online], Available: [https://www.ieee802.org/3/cz/public/8\\_feb\\_2022/perezaranda\\_3cz\\_01c\\_080222\\_TDFOM.pdf](https://www.ieee802.org/3/cz/public/8_feb_2022/perezaranda_3cz_01c_080222_TDFOM.pdf)

Thank you