

Simplified Transmitter Functional Test proposal.

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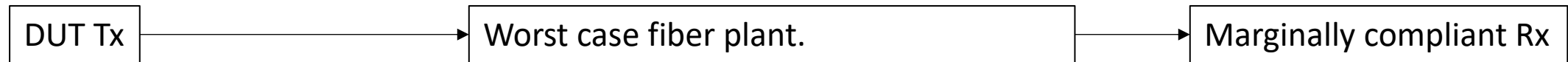
In support of 802.3dj comments 448 and 450 against draft D2.1

Introduction

- A Transmitter Functional test was incorporated in draft 2.1 of 802.3dj
- Further work has progressed on this resulting in the presentation Cole_3dj_01_adhoc_250908 which also proposes over fiber tests.
- This presentation takes a step back and proposes a simplified test. It leverages work and nomenclature from Cole_3dj_01_adhoc_250908
- It is in support of comments 448 and 450 against draft 2.1

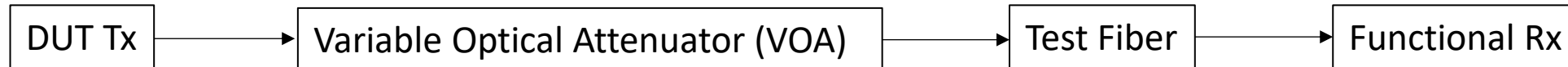
Purpose of test and Test block diagram

- The purpose of the test is to demonstrate that a Tx will be inter-operable with a worst case fiber plant and Rx.
- What we would really like



Worst case chromatic dispersion
Worst case MPI
Worst case DGD.
Maximum attenuation

- What we can have



Comments on Worst case Fiber plant and functional receiver.

- The worst case chromatic dispersion depends on the center wavelength of the DUT, and its chirp and other characteristics. To cover all the possibilities 3 test cases should be used. A fiber with maximum positive dispersion, a fiber with minimum negative dispersion and no fiber (just the same test cases as are used for the combination of TDECQ and TECQ). (Note that if dispersion is known not to be an issue (i.e. TDECQ=TECQ) then only the no-fiber test is needed.)
- MPI and DGD are best handled the same way they are in the link power budget by assuming they are equivalent to additional loss in the system.
 - Note the MPI of the link will depend on the functional receiver return loss as well as the fiber performance (as well as the DUT return loss). If any attempt were made to calibrate for this as is suggested in Cole_3dj_01_adhoc_250908 it would have to be done for the combination of fiber and functional receiver.
 - DGD of the test fiber is very difficult to measure.
- The functional receiver is as is described in D2.1 and Cole_3dj_01_adhoc_250908.
- The pass/fail criterion is as described in Cole_3dj_01_adhoc_250908

Variable Optical Attenuator attenuation value.

- The attenuation of the variable optical attenuator (VOA) is given by the same equation for all clauses
$$VOA_level = Test_SMF_correction + RxS_TECQ_correction - Test_margin$$

Where

- $Test_SMF_correction = Channel_insertion_loss \text{ (from spec)}$
 $+ MPI+DGD_penalty_allocation \text{ (from spec)}$
 $- Loss \text{ of test fiber used in the test.}$
- $RxS_TECQ_correction = RxS_OMA(max) \text{ (@DUT_TECQ) (from spec) - } ORx_RxS \text{ (@DUT_TECQ).}$ (which I think is what is intended in Cole_3dj_01_adhoc_250908)
- *Test Margin is as described in Cole_3dj_01_adhoc_250908*

Advantages of this simplified test.

- No changes to the test set-up are required based on the DUT's TDECQ, ER, OMA etc.
- The Test description is much simpler.
- The DUT gets credit if it has higher than the minimum required OMA. (which it will get in the real system).
- It guarantees system inter-operability with any compliant receiver that has equalization capabilities equivalent to the functional receiver. (same restriction as in Cole_3dj_01_adhoc_250908)
- Any Tx that passes the other Tx tests should pass this test unless it has correlated error problems.

Additional possible simplification.

- The only VOA setting dependency on the DUT performance is in the *RxS_TECQ_correction* where the correction is determined at the DUT-TECQ value. If the sensitivity versus TECQ slope = 1 this correction would be a number based on the functional Rx sensitivity but independent of DUT-TECQ.
- This sensitivity versus TECQ slope is expected to vary depending on what degradations are creating higher TECQ.
 - Additional noise is expected to have a slope of 1
 - Non-equalizable ISI and distortion is expected to have a slope of 1
 - Bandwidth restriction had a lower slope than 1 before the DFE was added in the reference equalizer (because real receivers included the DFE), but [Benefit of Adding DFE to TDECQ](#) (ghiasi_3dj_04c_2507.pdf) shows that the slope is now closer to 1.

• Proposal

Change to

$RxS_TECQ_correction = RxS_OMA(max) (@1.2dB\ TECQ) (from\ spec) - ORx_RxS (@1.2dB\ TECQ).$